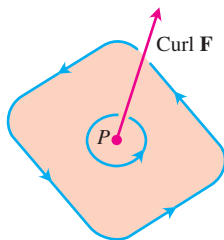


## 16.7

## Stokes' Theorem



**FIGURE 16.59** The circulation vector at a point  $P$  in a plane in a three-dimensional fluid flow. Notice its right-hand relation to the circulation line.

As we saw in Section 16.4, the circulation density or curl component of a two-dimensional field  $\mathbf{F} = M\mathbf{i} + N\mathbf{j}$  at a point  $(x, y)$  is described by the scalar quantity  $(\partial N/\partial x - \partial M/\partial y)$ . In three dimensions, the circulation around a point  $P$  in a plane is described with a vector. This vector is normal to the plane of the circulation (Figure 16.59) and points in the direction that gives it a right-hand relation to the circulation line. The length of the vector gives the rate of the fluid's rotation, which usually varies as the circulation plane is tilted about  $P$ . It turns out that the vector of greatest circulation in a flow with velocity field  $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$  is the **curl vector**

$$\operatorname{curl} \mathbf{F} = \left( \frac{\partial P}{\partial y} - \frac{\partial N}{\partial z} \right) \mathbf{i} + \left( \frac{\partial M}{\partial z} - \frac{\partial P}{\partial x} \right) \mathbf{j} + \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) \mathbf{k}. \quad (1)$$

We get this information from Stokes' Theorem, the generalization of the circulation-curl form of Green's Theorem to space.

Notice that  $(\operatorname{curl} \mathbf{F}) \cdot \mathbf{k} = (\partial N/\partial x - \partial M/\partial y)$  is consistent with our definition in Section 16.4 when  $\mathbf{F} = M(x, y)\mathbf{i} + N(x, y)\mathbf{j}$ . The formula for  $\operatorname{curl} \mathbf{F}$  in Equation (1) is often written using the symbolic operator

$$\nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z}. \quad (2)$$

(The symbol  $\nabla$  is pronounced “del.”) The curl of  $\mathbf{F}$  is  $\nabla \times \mathbf{F}$ :

$$\begin{aligned}\nabla \times \mathbf{F} &= \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ M & N & P \end{vmatrix} \\ &= \left( \frac{\partial P}{\partial y} - \frac{\partial N}{\partial z} \right) \mathbf{i} + \left( \frac{\partial M}{\partial z} - \frac{\partial P}{\partial x} \right) \mathbf{j} + \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) \mathbf{k} \\ &= \text{curl } \mathbf{F}.\end{aligned}$$

$$\text{curl } \mathbf{F} = \nabla \times \mathbf{F} \quad (3)$$

### EXAMPLE 1 Finding Curl $\mathbf{F}$

Find the curl of  $\mathbf{F} = (x^2 - y)\mathbf{i} + 4z\mathbf{j} + x^2\mathbf{k}$ .

**Solution**

$$\text{curl } \mathbf{F} = \nabla \times \mathbf{F} \quad \text{Equation (3)}$$

$$\begin{aligned}&= \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x^2 - y & 4z & x^2 \end{vmatrix} \\ &= \left( \frac{\partial}{\partial y}(x^2) - \frac{\partial}{\partial z}(4z) \right) \mathbf{i} - \left( \frac{\partial}{\partial x}(x^2) - \frac{\partial}{\partial z}(x^2 - y) \right) \mathbf{j} \\ &\quad + \left( \frac{\partial}{\partial x}(4z) - \frac{\partial}{\partial y}(x^2 - y) \right) \mathbf{k} \\ &= (0 - 4)\mathbf{i} - (2x - 0)\mathbf{j} + (0 + 1)\mathbf{k} \\ &= -4\mathbf{i} - 2x\mathbf{j} + \mathbf{k} \quad \blacksquare\end{aligned}$$

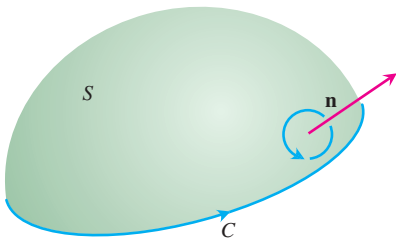
As we will see, the operator  $\nabla$  has a number of other applications. For instance, when applied to a scalar function  $f(x, y, z)$ , it gives the gradient of  $f$ :

$$\nabla f = \frac{\partial f}{\partial x} \mathbf{i} + \frac{\partial f}{\partial y} \mathbf{j} + \frac{\partial f}{\partial z} \mathbf{k}.$$

This may now be read as “del  $f$ ” as well as “grad  $f$ .”

### Stokes' Theorem

Stokes' Theorem says that, under conditions normally met in practice, the circulation of a vector field around the boundary of an oriented surface in space in the direction counterclockwise with respect to the surface's unit normal vector field  $\mathbf{n}$  (Figure 16.60) equals the integral of the normal component of the curl of the field over the surface.



**FIGURE 16.60** The orientation of the bounding curve  $C$  gives it a right-handed relation to the normal field  $\mathbf{n}$ .

**THEOREM 5** Stokes' Theorem

The circulation of a vector field  $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$  around the boundary  $C$  of an oriented surface  $S$  in the direction counterclockwise with respect to the surface's unit normal vector  $\mathbf{n}$  equals the integral of  $\nabla \times \mathbf{F} \cdot \mathbf{n}$  over  $S$ .

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma \quad (4)$$

Counterclockwise  
circulation      Curl integral

Notice from Equation (4) that if two different oriented surfaces  $S_1$  and  $S_2$  have the same boundary  $C$ , their curl integrals are equal:

$$\iint_{S_1} \nabla \times \mathbf{F} \cdot \mathbf{n}_1 \, d\sigma = \iint_{S_2} \nabla \times \mathbf{F} \cdot \mathbf{n}_2 \, d\sigma.$$

Both curl integrals equal the counterclockwise circulation integral on the left side of Equation (4) as long as the unit normal vectors  $\mathbf{n}_1$  and  $\mathbf{n}_2$  correctly orient the surfaces.

Naturally, we need some mathematical restrictions on  $\mathbf{F}$ ,  $C$ , and  $S$  to ensure the existence of the integrals in Stokes' equation. The usual restrictions are that all functions, vector fields, and their derivatives be continuous.

If  $C$  is a curve in the  $xy$ -plane, oriented counterclockwise, and  $R$  is the region in the  $xy$ -plane bounded by  $C$ , then  $d\sigma = dx \, dy$  and

$$(\nabla \times \mathbf{F}) \cdot \mathbf{n} = (\nabla \times \mathbf{F}) \cdot \mathbf{k} = \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right).$$

Under these conditions, Stokes' equation becomes

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_R \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx \, dy,$$

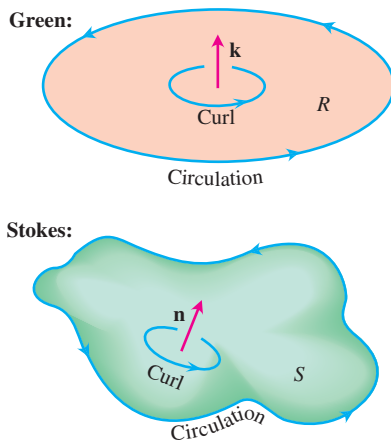
which is the circulation-curl form of the equation in Green's Theorem. Conversely, by reversing these steps we can rewrite the circulation-curl form of Green's Theorem for two-dimensional fields in del notation as

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_R \nabla \times \mathbf{F} \cdot \mathbf{k} \, dA. \quad (5)$$

See Figure 16.61.

**EXAMPLE 2** Verifying Stokes' Equation for a Hemisphere

Evaluate Equation (4) for the hemisphere  $S: x^2 + y^2 + z^2 = 9, z \geq 0$ , its bounding circle  $C: x^2 + y^2 = 9, z = 0$ , and the field  $\mathbf{F} = y\mathbf{i} - x\mathbf{j}$ .



**FIGURE 16.61** Comparison of Green's Theorem and Stokes' Theorem.

**Solution** We calculate the counterclockwise circulation around  $C$  (as viewed from above) using the parametrization  $\mathbf{r}(\theta) = (3 \cos \theta)\mathbf{i} + (3 \sin \theta)\mathbf{j}$ ,  $0 \leq \theta \leq 2\pi$ :

$$d\mathbf{r} = (-3 \sin \theta \, d\theta)\mathbf{i} + (3 \cos \theta \, d\theta)\mathbf{j}$$

$$\mathbf{F} = y\mathbf{i} - x\mathbf{j} = (3 \sin \theta)\mathbf{i} - (3 \cos \theta)\mathbf{j}$$

$$\mathbf{F} \cdot d\mathbf{r} = -9 \sin^2 \theta \, d\theta - 9 \cos^2 \theta \, d\theta = -9 \, d\theta$$

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \int_0^{2\pi} -9 \, d\theta = -18\pi.$$

For the curl integral of  $\mathbf{F}$ , we have

$$\nabla \times \mathbf{F} = \left( \frac{\partial P}{\partial y} - \frac{\partial N}{\partial z} \right)\mathbf{i} + \left( \frac{\partial M}{\partial z} - \frac{\partial P}{\partial x} \right)\mathbf{j} + \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right)\mathbf{k}$$

$$= (0 - 0)\mathbf{i} + (0 - 0)\mathbf{j} + (-1 - 1)\mathbf{k} = -2\mathbf{k}$$

$$\mathbf{n} = \frac{x\mathbf{i} + y\mathbf{j} + z\mathbf{k}}{\sqrt{x^2 + y^2 + z^2}} = \frac{x\mathbf{i} + y\mathbf{j} + z\mathbf{k}}{3} \quad \text{Outer unit normal}$$

$$d\sigma = \frac{3}{z} dA$$

Section 16.5, Example 5,  
with  $a = 3$

$$\nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma = -\frac{2z}{3} \frac{3}{z} dA = -2 \, dA$$

and

$$\iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma = \iint_{x^2+y^2 \leq 9} -2 \, dA = -18\pi.$$

The circulation around the circle equals the integral of the curl over the hemisphere, as it should. ■

### EXAMPLE 3 Finding Circulation

Find the circulation of the field  $\mathbf{F} = (x^2 - y)\mathbf{i} + 4z\mathbf{j} + x^2\mathbf{k}$  around the curve  $C$  in which the plane  $z = 2$  meets the cone  $z = \sqrt{x^2 + y^2}$ , counterclockwise as viewed from above (Figure 16.62).

**Solution** Stokes' Theorem enables us to find the circulation by integrating over the surface of the cone. Traversing  $C$  in the counterclockwise direction viewed from above corresponds to taking the *inner* normal  $\mathbf{n}$  to the cone, the normal with a positive  $z$ -component.

We parametrize the cone as

$$\mathbf{r}(r, \theta) = (r \cos \theta)\mathbf{i} + (r \sin \theta)\mathbf{j} + r\mathbf{k}, \quad 0 \leq r \leq 2, \quad 0 \leq \theta \leq 2\pi.$$

We then have

$$\begin{aligned} \mathbf{n} &= \frac{\mathbf{r}_r \times \mathbf{r}_\theta}{|\mathbf{r}_r \times \mathbf{r}_\theta|} = \frac{-(r \cos \theta)\mathbf{i} - (r \sin \theta)\mathbf{j} + r\mathbf{k}}{r\sqrt{2}} \\ &= \frac{1}{\sqrt{2}} \left( -(\cos \theta)\mathbf{i} - (\sin \theta)\mathbf{j} + \mathbf{k} \right) \end{aligned} \quad \begin{array}{l} \text{Section 16.6,} \\ \text{Example 4} \end{array}$$

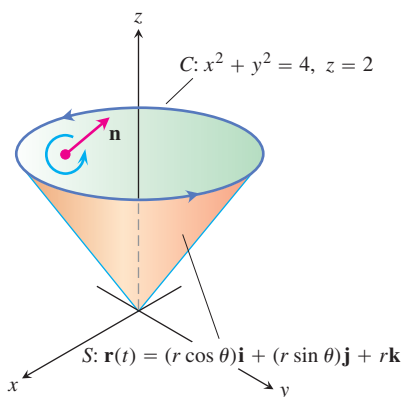


FIGURE 16.62 The curve  $C$  and cone  $S$  in Example 3.

$$\begin{aligned}
 d\sigma &= r\sqrt{2} \, dr \, d\theta && \text{Section 16.6, Example 4} \\
 \nabla \times \mathbf{F} &= -4\mathbf{i} - 2x\mathbf{j} + \mathbf{k} && \text{Example 1} \\
 &= -4\mathbf{i} - 2r \cos \theta \mathbf{j} + \mathbf{k}. && x = r \cos \theta
 \end{aligned}$$

Accordingly,

$$\begin{aligned}
 \nabla \times \mathbf{F} \cdot \mathbf{n} &= \frac{1}{\sqrt{2}} \left( 4 \cos \theta + 2r \cos \theta \sin \theta + 1 \right) \\
 &= \frac{1}{\sqrt{2}} \left( 4 \cos \theta + r \sin 2\theta + 1 \right)
 \end{aligned}$$

and the circulation is

$$\begin{aligned}
 \oint_C \mathbf{F} \cdot d\mathbf{r} &= \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma && \text{Stokes' Theorem, Equation (4)} \\
 &= \int_0^{2\pi} \int_0^2 \frac{1}{\sqrt{2}} \left( 4 \cos \theta + r \sin 2\theta + 1 \right) (r\sqrt{2} \, dr \, d\theta) = 4\pi. && \blacksquare
 \end{aligned}$$

### Paddle Wheel Interpretation of $\nabla \times \mathbf{F}$

Suppose that  $\mathbf{v}(x, y, z)$  is the velocity of a moving fluid whose density at  $(x, y, z)$  is  $\delta(x, y, z)$  and let  $\mathbf{F} = \delta \mathbf{v}$ . Then

$$\oint_C \mathbf{F} \cdot d\mathbf{r}$$

is the circulation of the fluid around the closed curve  $C$ . By Stokes' Theorem, the circulation is equal to the flux of  $\nabla \times \mathbf{F}$  through a surface  $S$  spanning  $C$ :

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma.$$

Suppose we fix a point  $Q$  in the domain of  $\mathbf{F}$  and a direction  $\mathbf{u}$  at  $Q$ . Let  $C$  be a circle of radius  $\rho$ , with center at  $Q$ , whose plane is normal to  $\mathbf{u}$ . If  $\nabla \times \mathbf{F}$  is continuous at  $Q$ , the average value of the  $\mathbf{u}$ -component of  $\nabla \times \mathbf{F}$  over the circular disk  $S$  bounded by  $C$  approaches the  $\mathbf{u}$ -component of  $\nabla \times \mathbf{F}$  at  $Q$  as  $\rho \rightarrow 0$ :

$$(\nabla \times \mathbf{F} \cdot \mathbf{u})_Q = \lim_{\rho \rightarrow 0} \frac{1}{\pi\rho^2} \iint_S \nabla \times \mathbf{F} \cdot \mathbf{u} \, d\sigma.$$

If we replace the surface integral in this last equation by the circulation, we get

$$(\nabla \times \mathbf{F} \cdot \mathbf{u})_Q = \lim_{\rho \rightarrow 0} \frac{1}{\pi\rho^2} \oint_C \mathbf{F} \cdot d\mathbf{r}. \quad (6)$$

The left-hand side of Equation (6) has its maximum value when  $\mathbf{u}$  is the direction of  $\nabla \times \mathbf{F}$ . When  $\rho$  is small, the limit on the right-hand side of Equation (6) is approximately

$$\frac{1}{\pi\rho^2} \oint_C \mathbf{F} \cdot d\mathbf{r},$$

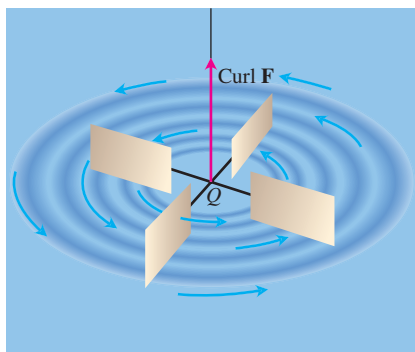


FIGURE 16.63 The paddle wheel interpretation of curl  $\mathbf{F}$ .

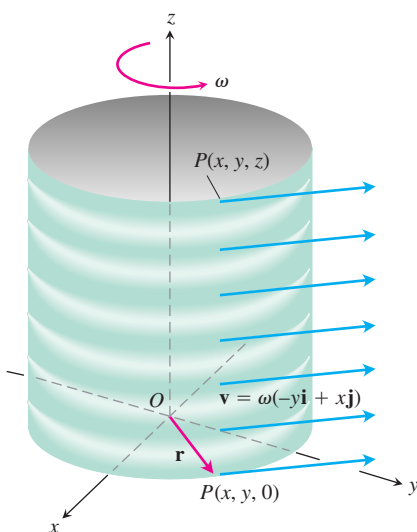


FIGURE 16.64 A steady rotational flow parallel to the  $xy$ -plane, with constant angular velocity  $\omega$  in the positive (counterclockwise) direction (Example 4).

which is the circulation around  $C$  divided by the area of the disk (circulation density). Suppose that a small paddle wheel of radius  $\rho$  is introduced into the fluid at  $Q$ , with its axle directed along  $\mathbf{u}$ . The circulation of the fluid around  $C$  will affect the rate of spin of the paddle wheel. The wheel will spin fastest when the circulation integral is maximized; therefore it will spin fastest when the axle of the paddle wheel points in the direction of  $\nabla \times \mathbf{F}$  (Figure 16.63).

#### EXAMPLE 4 Relating $\nabla \times \mathbf{F}$ to Circulation Density

A fluid of constant density rotates around the  $z$ -axis with velocity  $\mathbf{v} = \omega(-y\mathbf{i} + x\mathbf{j})$ , where  $\omega$  is a positive constant called the *angular velocity* of the rotation (Figure 16.64). If  $\mathbf{F} = \mathbf{v}$ , find  $\nabla \times \mathbf{F}$  and relate it to the circulation density.

**Solution** With  $\mathbf{F} = \mathbf{v} = -\omega y\mathbf{i} + \omega x\mathbf{j}$ ,

$$\begin{aligned}\nabla \times \mathbf{F} &= \left( \frac{\partial P}{\partial y} - \frac{\partial N}{\partial z} \right) \mathbf{i} + \left( \frac{\partial M}{\partial z} - \frac{\partial P}{\partial x} \right) \mathbf{j} + \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) \mathbf{k} \\ &= (0 - 0)\mathbf{i} + (0 - 0)\mathbf{j} + (\omega - (-\omega))\mathbf{k} = 2\omega\mathbf{k}.\end{aligned}$$

By Stokes' Theorem, the circulation of  $\mathbf{F}$  around a circle  $C$  of radius  $\rho$  bounding a disk  $S$  in a plane normal to  $\nabla \times \mathbf{F}$ , say the  $xy$ -plane, is

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma = \iint_S 2\omega\mathbf{k} \cdot \mathbf{k} \, dx \, dy = (2\omega)(\pi\rho^2).$$

Thus,

$$(\nabla \times \mathbf{F}) \cdot \mathbf{k} = 2\omega = \frac{1}{\pi\rho^2} \oint_C \mathbf{F} \cdot d\mathbf{r},$$

consistent with Equation (6) when  $\mathbf{u} = \mathbf{k}$ . ■

#### EXAMPLE 5 Applying Stokes' Theorem

Use Stokes' Theorem to evaluate  $\int_C \mathbf{F} \cdot d\mathbf{r}$ , if  $\mathbf{F} = xz\mathbf{i} + xy\mathbf{j} + 3xz\mathbf{k}$  and  $C$  is the boundary of the portion of the plane  $2x + y + z = 2$  in the first octant, traversed counterclockwise as viewed from above (Figure 16.65).

**Solution** The plane is the level surface  $f(x, y, z) = 2$  of the function  $f(x, y, z) = 2x + y + z$ . The unit normal vector

$$\mathbf{n} = \frac{\nabla f}{|\nabla f|} = \frac{(2\mathbf{i} + \mathbf{j} + \mathbf{k})}{|2\mathbf{i} + \mathbf{j} + \mathbf{k}|} = \frac{1}{\sqrt{6}}(2\mathbf{i} + \mathbf{j} + \mathbf{k})$$

is consistent with the counterclockwise motion around  $C$ . To apply Stokes' Theorem, we find

$$\text{curl } \mathbf{F} = \nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xz & xy & 3xz \end{vmatrix} = (x - 3z)\mathbf{j} + y\mathbf{k}.$$

On the plane,  $z$  equals  $2 - 2x - y$ , so

$$\nabla \times \mathbf{F} = (x - 3(2 - 2x - y))\mathbf{j} + y\mathbf{k} = (7x + 3y - 6)\mathbf{j} + y\mathbf{k}$$

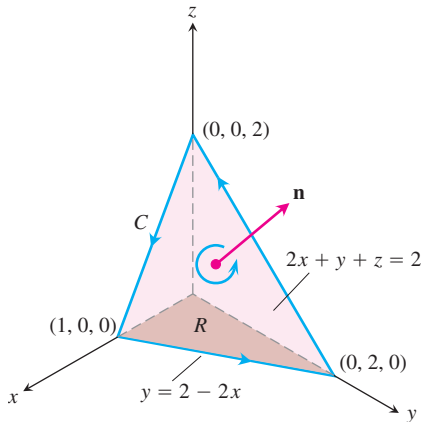


FIGURE 16.65 The planar surface in Example 5.

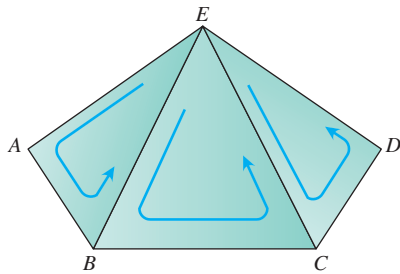


FIGURE 16.66 Part of a polyhedral surface.

and

$$\nabla \times \mathbf{F} \cdot \mathbf{n} = \frac{1}{\sqrt{6}} (7x + 3y - 6 + y) = \frac{1}{\sqrt{6}} (7x + 4y - 6).$$

The surface area element is

$$d\sigma = \frac{|\nabla f|}{|\nabla f \cdot \mathbf{k}|} dA = \frac{\sqrt{6}}{1} dx dy.$$

The circulation is

$$\begin{aligned} \oint_C \mathbf{F} \cdot d\mathbf{r} &= \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma && \text{Stokes' Theorem, Equation (4)} \\ &= \int_0^1 \int_0^{2-2x} \frac{1}{\sqrt{6}} (7x + 4y - 6) \sqrt{6} dy dx \\ &= \int_0^1 \int_0^{2-2x} (7x + 4y - 6) dy dx = -1. \end{aligned}$$

### Proof of Stokes' Theorem for Polyhedral Surfaces

Let  $S$  be a polyhedral surface consisting of a finite number of plane regions. (See Figure 16.66 for an example.) We apply Green's Theorem to each separate panel of  $S$ . There are two types of panels:

1. Those that are surrounded on all sides by other panels
2. Those that have one or more edges that are not adjacent to other panels.

The boundary  $\Delta$  of  $S$  consists of those edges of the type 2 panels that are not adjacent to other panels. In Figure 16.66, the triangles  $EAB$ ,  $BCE$ , and  $CDE$  represent a part of  $S$ , with  $ABCDE$  part of the boundary  $\Delta$ . Applying Green's Theorem to the three triangles in turn and adding the results, we get

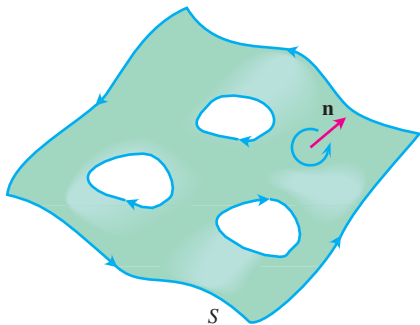
$$\left( \oint_{EAB} + \oint_{BCE} + \oint_{CDE} \right) \mathbf{F} \cdot d\mathbf{r} = \left( \iint_{EAB} + \iint_{BCE} + \iint_{CDE} \right) \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma. \quad (7)$$

The three line integrals on the left-hand side of Equation (7) combine into a single line integral taken around the periphery  $ABCDE$  because the integrals along interior segments cancel in pairs. For example, the integral along segment  $BE$  in triangle  $ABE$  is opposite in sign to the integral along the same segment in triangle  $EBC$ . The same holds for segment  $CE$ . Hence, Equation (7) reduces to

$$\oint_{ABCDE} \mathbf{F} \cdot d\mathbf{r} = \iint_{ABCDE} \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma.$$

When we apply Green's Theorem to all the panels and add the results, we get

$$\oint_{\Delta} \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma.$$



**FIGURE 16.67** Stokes' Theorem also holds for oriented surfaces with holes.

This is Stokes' Theorem for a polyhedral surface  $S$ . You can find proofs for more general surfaces in advanced calculus texts.

### Stokes' Theorem for Surfaces with Holes

Stokes' Theorem can be extended to an oriented surface  $S$  that has one or more holes (Figure 16.67), in a way analogous to the extension of Green's Theorem: The surface integral over  $S$  of the normal component of  $\nabla \times \mathbf{F}$  equals the sum of the line integrals around all the boundary curves of the tangential component of  $\mathbf{F}$ , where the curves are to be traced in the direction induced by the orientation of  $S$ .

### An Important Identity

The following identity arises frequently in mathematics and the physical sciences.

$$\text{curl grad } f = \mathbf{0} \quad \text{or} \quad \nabla \times \nabla f = \mathbf{0} \quad (8)$$

This identity holds for any function  $f(x, y, z)$  whose second partial derivatives are continuous. The proof goes like this:

$$\nabla \times \nabla f = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial f}{\partial x} & \frac{\partial f}{\partial y} & \frac{\partial f}{\partial z} \end{vmatrix} = (f_{zy} - f_{yz})\mathbf{i} - (f_{zx} - f_{xz})\mathbf{j} + (f_{yx} - f_{xy})\mathbf{k}.$$

If the second partial derivatives are continuous, the mixed second derivatives in parentheses are equal (Theorem 2, Section 14.3) and the vector is zero.

### Conservative Fields and Stokes' Theorem

In Section 16.3, we found that a field  $\mathbf{F}$  is conservative in an open region  $D$  in space is equivalent to the integral of  $\mathbf{F}$  around every closed loop in  $D$  being zero. This, in turn, is equivalent in *simply connected* open regions to saying that  $\nabla \times \mathbf{F} = \mathbf{0}$ .

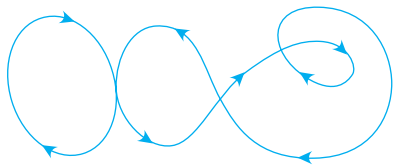
#### **THEOREM 6** Curl $\mathbf{F} = \mathbf{0}$ Related to the Closed-Loop Property

If  $\nabla \times \mathbf{F} = \mathbf{0}$  at every point of a simply connected open region  $D$  in space, then on any piecewise-smooth closed path  $C$  in  $D$ ,

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = 0.$$

**Sketch of a Proof** Theorem 6 is usually proved in two steps. The first step is for simple closed curves. A theorem from topology, a branch of advanced mathematics, states that





**FIGURE 16.68** In a simply connected open region in space, differentiable curves that cross themselves can be divided into loops to which Stokes' Theorem applies.

every differentiable simple closed curve  $C$  in a simply connected open region  $D$  is the boundary of a smooth two-sided surface  $S$  that also lies in  $D$ . Hence, by Stokes' Theorem,

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma = 0.$$

The second step is for curves that cross themselves, like the one in Figure 16.68. The idea is to break these into simple loops spanned by orientable surfaces, apply Stokes' Theorem one loop at a time, and add the results. ■

The following diagram summarizes the results for conservative fields defined on connected, simply connected open regions.

