



Introduction to Aerospace Propulsion

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Lecture No - 34



In this lecture ...

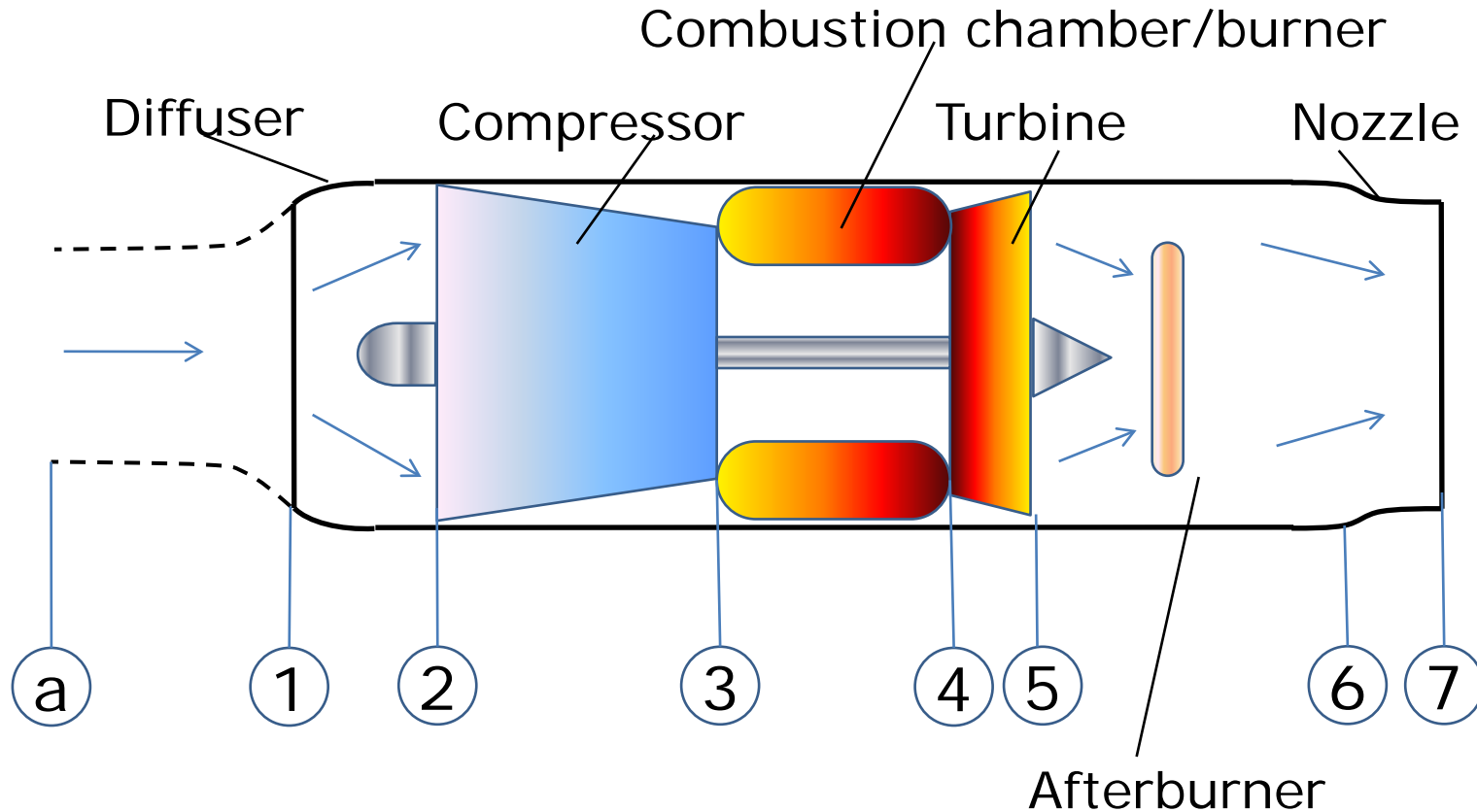
- Solve problems
 - Ideal cycle analysis of air breathing engines

Problem # 1

- The following data apply to a turbojet flying at an altitude where the ambient conditions are 0.458 bar and 248 K.
- Speed of the aircraft: 805 km/h
- Compressor pressure ratio: 4:1
- Turbine inlet temperature: 1100 K
- Nozzle outlet area 0.0935 m²
- Heat of reaction of the fuel: 43 MJ/kg

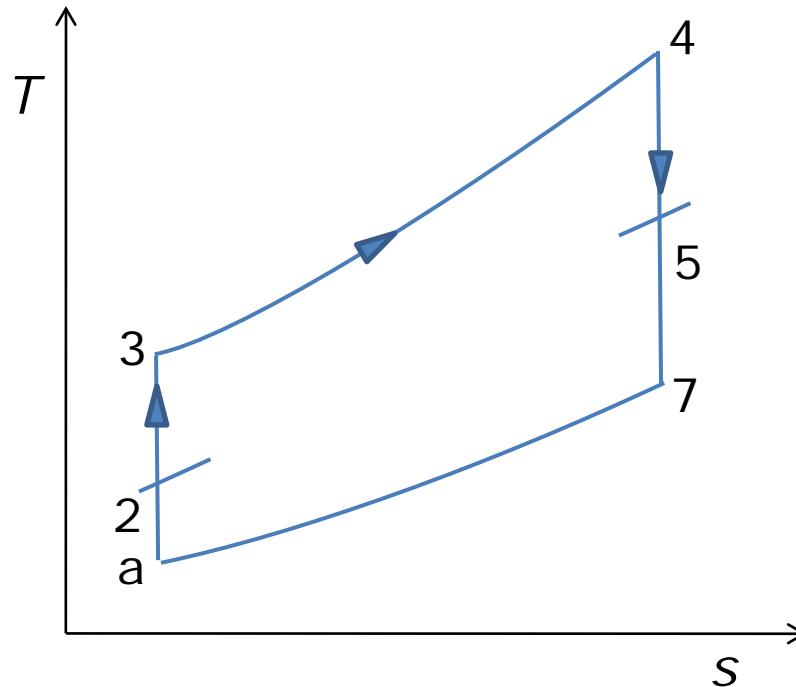
Find the thrust and TSFC assuming c_p as 1.005 kJ/kgK and γ as 1.4

Ideal cycle for jet engines



Schematic of a turbojet engine and station numbering scheme

Ideal cycle for jet engines



Ideal turbojet cycle (without afterburning)
on a T-s diagram

Solution: Problem # 1

- Speed of the aircraft =
 $805 \times 1000 / 3600 = 223.6 \text{ m/s}$
- Mach number = $223.6 / \sqrt{(\gamma RT)}$
 $= 223.6 / \sqrt{(1.4 \times 287 \times 248)}$
 $= 0.708$

- Intake:

$$T_{02} = T_a \left(1 + \frac{\gamma - 1}{2} M^2 \right) = 248 \left(1 + \frac{1.4 - 1}{2} 0.708^2 \right) = 272.86 \text{ K}$$

$$P_{02} = P_a \left(\frac{T_{02}}{T_a} \right)^{\gamma / (\gamma - 1)} = 0.458 (272.86 / 248)^{1.4 / (1.4 - 1)} = 0.639 \text{ bar}$$

Solution: Problem # 1

- Compressor:

$$P_{03} = \pi_c P_{02} = 4 \times 0.639 = 2.556 \text{ bar}$$

$$T_{03} = T_{02} (\pi_c)^{(\gamma-1)/\gamma} = 272.86(4)^{(1.4-1)/1.4} = 405.63 \text{ K}$$

- Combustion chamber: From energy balance,

$$h_{04} = h_{03} + fQ_R$$

$$\text{or, } f = \frac{T_{04}/T_{03} - 1}{Q_R / c_p T_{03} - T_{04}/T_{03}}$$

$$= \frac{1100/405.63 - 1}{(43 \times 10^6 / 1005 \times 405.63) - 1100/405.63} = 0.017$$

Solution: Problem # 1

- Turbine: Since the turbine produces work to drive the compressor, $W_{turbine} = W_{compressor}$

$$\dot{m}_t c_p (T_{04} - T_{05}) = \dot{m}_a c_p (T_{03} - T_{02})$$

$$T_{05} = T_{04} - (T_{03} - T_{02}) / (1 + f)$$

$$= 1100 - (405.63 - 272.86) / (1 + 0.017) = 969.45 \text{ K}$$

$$\text{Hence, } P_{05} = P_{04} \left(\frac{T_{05}}{T_{04}} \right)^{\gamma / (\gamma - 1)} = 2.556 (969.45 / 1100)^{1.4 / (1.4 - 1)}$$

$$= 1.642 \text{ bar}$$

Solution: Problem # 1

- Nozzle: we first check for choking of the nozzle.
- The nozzle pressure ratio is $P_{05}/P_a = 1.642/0.458 = 3.58$
- The critical pressure ratio is

$$\frac{P_{05}}{P^*} = \left[\frac{\gamma + 1}{2} \right]^{\gamma/(\gamma-1)} = \left(\frac{1.4 + 1}{2} \right)^{1.4/(1.4-1)} = 1.893$$

- Therefore the nozzle is choking.
- The nozzle exit conditions will be determined by the critical properties.

Solution: Problem # 1

$$T_7 = T^* = \left(\frac{2}{\gamma + 1} \right) T_{05} = \frac{2}{1.4 + 1} 969.5 = 807.92 \text{ K}$$

$$P_7 = P^* = P_{05} \left(\frac{1}{P_{04} / P^*} \right) = \frac{1.642}{1.893} = 0.867$$

$$\rho_7 = P_7 / RT_7 = 0.867 \times 10^5 / (287 \times 807.92) = 0.374 \text{ kg/m}^3$$

Therefore, $u_e = \sqrt{\gamma RT_7} = \sqrt{1.4 \times 287 \times 807.92} = 569.75 \text{ m/s}$

The mass flow rate is, $\dot{m} = \rho_7 A_7 u_e = 19.92 \text{ kg/s}$

Solution: Problem # 1

The thrust developed is $\mathfrak{T} = \dot{m}[(1+f)u_e - u] + A_7(P^* - P_a)$

$$= 19.92[(1+0.017)569.75 - 223.6]$$
$$+ 0.0935(0.867 - 0.458) \times 10^5$$
$$= 10.912 \text{ kN}$$

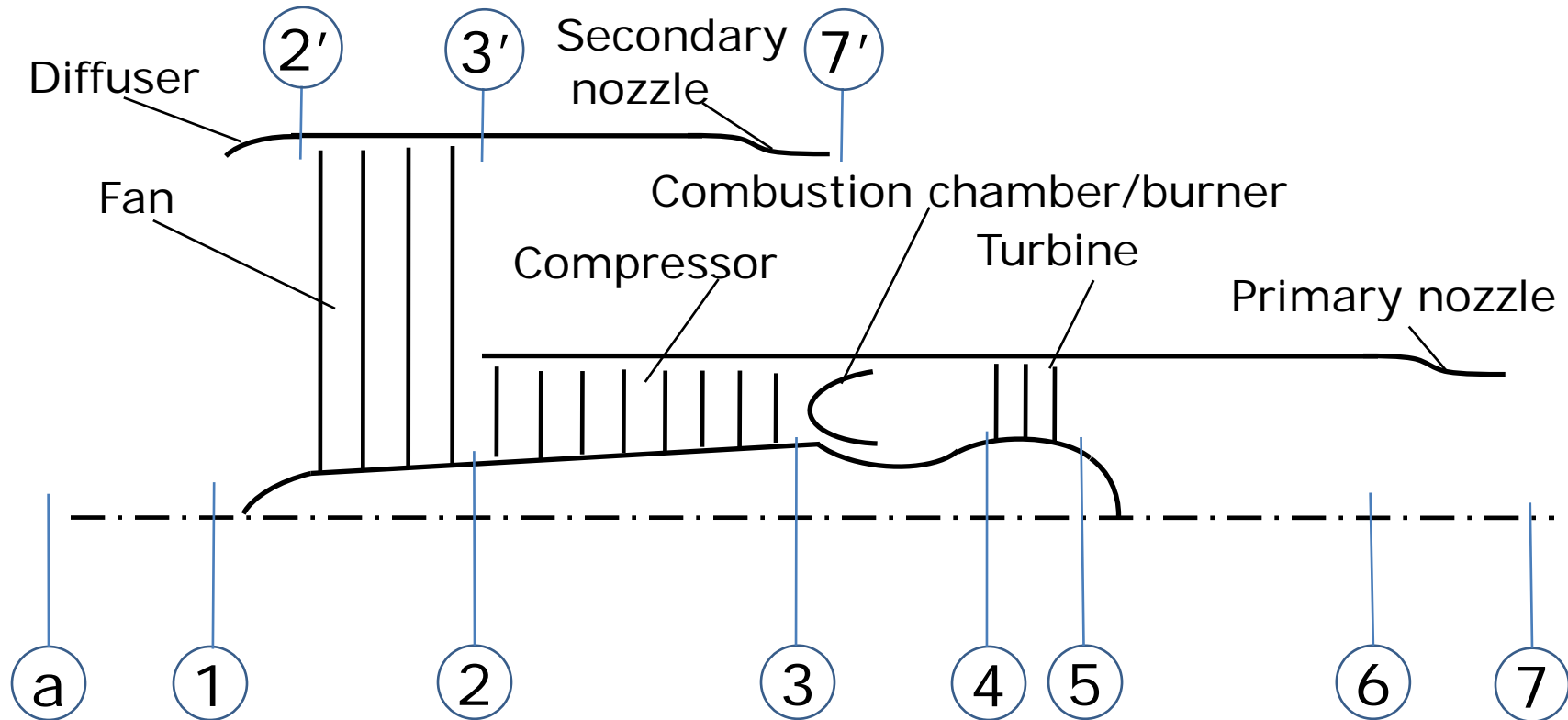
Fuel flow rate, $\dot{m}_f = f \times \dot{m}_a = 0.017 \times 19.92 = 0.3387 \text{ kg/s}$

Therefore, TSFC = $\dot{m}_f / \mathfrak{T} = 3.1 \times 10^{-5} \text{ kg/Ns} = 0.111 \text{ kg/N h}$

Problem # 2

- The following data apply to a twin spool turbofan engine, with the fan driven by the LP turbine and the compressor by the HP turbine. Separate hot and cold nozzles are used.
- Overall pressure ratio: 19.0
- Fan pressure ratio: 1.65
- Bypass ratio: 3.0
- Turbine inlet temperature: 1300 K
- Air mass flow: 115 kg/s
- Find the sea level static thrust and TSFC if the ambient pressure and temperature are 1 bar and 288 K. Heat of reaction of the fuel: 43 MJ/kg

Ideal turbofan engine



Schematic of an unmixed turbofan engine and station numbering scheme

Solution: Problem # 2

- Since we are required to find the static thrust, the Mach number is zero.

- Intake:

$$T_{02'} = T_a \left(1 + \frac{\gamma - 1}{2} M^2 \right) = 288 \text{ K}$$

$$P_{02'} = P_a \left(\frac{T_{02'}}{T_a} \right)^{\gamma/(\gamma-1)} = 1 \text{ bar}$$

- Fan: Fan pressure ratio is known: $\pi_f = P_{03'} / P_{02'}$

$$P_{03'} = \pi_f P_{02'} = 1.65 \text{ bar}$$

$$T_{03'} = T_{02'} (\pi_f)^{(\gamma-1)/\gamma} = 288(1.65)^{(1.4-1)/1.4} = 332.35 \text{ K}$$

Solution: Problem # 2

- Compressor:

$$\pi_c = \text{Overall pressure ratio} / 1.65 = 19 / 1.65 = 11.515$$

$$P_{03} = \pi_c P_{02} = 11.5151 \times 1.65 = 19.0 \text{ bar}$$

$$T_{03} = T_{02} (\pi_c)^{(\gamma-1)/\gamma} = 332.35 \times (11.515)^{(1.4-1)/1.4} = 668.53 \text{ K}$$

- Combustion chamber: From energy balance,

$$f = \frac{T_{04} / T_{03} - 1}{Q_R / c_p T_{03} - T_{04} / T_{03}}$$

$$= \frac{1300 / 668.53 - 1}{(43 \times 10^6 / 1005 \times 668.53) - 1300 / 668.53} = 0.01522$$

Solution: Problem # 2

- High pressure turbine:

$$\dot{m}_t c_p (T_{04} - T_{05'}) = \dot{m}_{aH} c_p (T_{03} - T_{02})$$

Here, $T_{05'}$ is the temperature at the HPT exit.

$$\begin{aligned} \therefore T_{05'} &= T_{04} - (T_{03} - T_{02}) / (1 + f) \\ &= 1300 - (668.53 - 332.53) / (1 + 0.01522) = 969.04 \text{ K} \end{aligned}$$

$$\text{Hence, } P_{05'} = P_{04} \left(\frac{T_{05'}}{T_{04}} \right)^{\gamma/(\gamma-1)} = 19 \left(\frac{969.04}{1300} \right)^{1.4/(1.4-1)} = 6.79 \text{ bar}$$

Solution: Problem # 2

- Low pressure turbine:

$$\dot{m}_t c_p (T_{05'} - T_{05}) = \dot{m}_{aC} c_p (T_{03'} - T_{02'})$$

Here, $T_{05'}$ is the temperature at the HPT exit/LPT inlet.

$$\begin{aligned} \therefore T_{05} &= T_{05'} - B(T_{03'} - T_{02'}) / (1 + f), \text{ where, } B = \frac{\dot{m}_{aC}}{\dot{m}_{aH}} \\ &= 969.04 - 3 \times (332.35 - 288) / (1 + 0.01522) = 837.98 \text{ K} \end{aligned}$$

$$\text{And, } P_{05} = P_{05'} \left(\frac{T_{05}}{T_{05'}} \right)^{\gamma/(\gamma-1)} = 6.79 \left(\frac{837.98}{969.04} \right)^{1.4/(1.4-1)} = 4.08 \text{ bar}$$

Solution: Problem # 2

- Primary nozzle: we first check for choking of the nozzle.
- The nozzle pressure ratio is $P_{05}/P_a = 4.08/1 = 4.08$ bar
- The critical pressure ratio is

$$\frac{P_{05}}{P^*} = \left[\frac{\gamma + 1}{2} \right]^{\gamma/(\gamma-1)} = \left(\frac{1.4 + 1}{2} \right)^{1.4/(1.4-1)} = 1.893$$

- Therefore the nozzle is choking.
- The nozzle exit conditions will be determined by the critical properties.

Solution: Problem # 2

$$T_7 = T^* = \left(\frac{2}{\gamma + 1} \right) T_{05} = \frac{2}{1.4 + 1} 837.98 = 698.32 \text{ K}$$

$$P_7 = P^* = P_{05} \left(\frac{1}{P_{05} / P^*} \right) = \frac{4.08}{1.893} = 2.155 \text{ bar}$$

$$\text{Therefore, } u_e = \sqrt{\gamma R T_7} = \sqrt{1.4 \times 287 \times 698.32} = 529.7 \text{ m/s}$$

Solution: Problem # 2

- Secondary nozzle:
- The nozzle pressure ratio is $P_{03'}/P_a = 1.65/1 = 1.65$ bar
- The critical pressure ratio is

$$\frac{P_{05}}{P^*} = \left[\frac{\gamma + 1}{2} \right]^{\gamma/(\gamma-1)} = \left(\frac{1.4 + 1}{2} \right)^{1.4/(1.4-1)} = 1.893$$

- Therefore the nozzle is not choking.

$$\begin{aligned} \therefore u_{ef} &= \sqrt{2c_p T_{03'} \left[1 - \left(P_a / P_{03'} \right)^{(\gamma-1)/\gamma} \right]} \\ &= \sqrt{2 \times 1005 \times 332.35 \left[1 - (1/1.65)^{(1.4-1)/1.4} \right]} = 298.52 \end{aligned}$$

Solution: Problem # 2

- Thrust,

$$\mathfrak{T} = \dot{m}_{aH} [(1 + f)u_e - u] + B\dot{m}_{aH} (u_{ef} - u)$$

assuming $(P_e - P_a)A_e$ to be negligible.

$$\dot{m}_{aC} / \dot{m}_{aH} = 3.0, \quad \dot{m}_{aH} + \dot{m}_{aC} = 115 \text{ kg/s}$$

$$\therefore \dot{m}_{aH} = 115 / 4 = 28.75 \text{ kg/s}$$

$$\mathfrak{T} = 28.75[(1 + 0.01522) \times 529.7 - 0]$$

$$+ 3 \times 28.75(298.52 - 0)$$

$$= 40.74 \text{ kN}$$

Solution: Problem # 2

- Exercise: calculate the thrust by factoring the pressure thrust term as well. Hint: you can calculate the exit area from mass flow, density and exhaust velocity.
- TSFC,
Fuel flow rate, $\dot{m}_f = f \times \dot{m}_a = 0.01522 \times 28.75 = 0.4376 \text{ kg/s}$
Therefore, $\text{TSFC} = \dot{m}_f / \mathfrak{T} = 1.075 \times 10^{-5} \text{ kg/Ns} = 0.0388 \text{ kg/N h}$

Problem # 3

- A helicopter using a turboshaft engine is flying at 300 km/h at an altitude where the ambient temperature is 5°C . Determine the specific power output and thermal efficiency. The specifications of the engine are: compressor pressure ratio = 9.0 , turbine inlet temperature = 800°C .

Problem # 3

- For a turboshaft engine, there is no nozzle thrust.
- $u = 300 \times 1000 / 3600 = 83.33 \text{ m/s}$
- $T_a = 278 \text{ K}$
- Therefore, Mach number
 $M = 83.33 / \sqrt{(1.4 \times 287 \times 278)} = 0.25$
- Intake:

$$T_{02} = T_a \left(1 + \frac{\gamma - 1}{2} M^2 \right) = 278 \left(1 + \frac{1.4 - 1}{2} 0.25^2 \right) = 281.48 \text{ K}$$

$$P_{02} = P_a \left(\frac{T_{02}}{T_a} \right)^{\gamma / (\gamma - 1)} = 0.8 \left(\frac{281.48}{278} \right)^{1.4 / (1.4 - 1)} = 0.835 \text{ bar}$$

Problem # 3

- Compressor:

$$P_{03} = \pi_c P_{02} = 9.0 \times 0.835 = 7.52 \text{ bar}$$

$$T_{03} = T_{02} (\pi_c)^{(\gamma-1)/\gamma} = 281.48 \times (9.0)^{(1.4-1)/1.4} = 527.67 \text{ K}$$

Specific work required to drive the compressor,

$$W_c = c_p (T_{03} - T_{02}) = 1.005(527.67 - 281.48) = 247.42 \text{ kJ/kg}$$

- Combustor:

$$f = \frac{T_{04}/T_{03} - 1}{Q_R / c_p T_{03} - T_{04}/T_{03}}$$

$$= \frac{1073/527.67 - 1}{(43 \times 10^6 / 1005 \times 527.67) - 1073/527.67} = 0.013$$

Problem # 3

- Turbine:

$$\frac{P_{04}}{P_{05}} = \frac{P_{03}}{P_a} = \frac{P_{03}}{P_{02}} \frac{P_{02}}{P_a} = 9 \times \frac{0.835}{0.8} = 9.394$$

$$\frac{T_{04}}{T_{05}} = \left(\frac{P_{04}}{P_{05}} \right)^{(\gamma-1)/\gamma} = 9.394^{(1.4-1)/1.4} = 1.897$$

$$T_{05} = 565.63K$$

$$\begin{aligned} \text{Work done by the turbine, } W_t &= (1 + f)c_p (T_{04} - T_{05}) \\ &= (1 + 0.013) \times 1.005 \times (1073 - 565.63) \\ &= 516.54 \text{ kJ/kg} \end{aligned}$$

Problem # 3

- Specific work output, $W_{net} = W_t - W_c$
 $= 516.54 - 247.42$
 $= 269.12 \text{ kJ/kg}$
- Thermal efficiency: W_{net}/Q_{in}
- $Q_{in} = c_p(T_{04} - T_{03}) = 1.005(1073 - 527.67)$
 $= 548.05 \text{ kJ/kg}$
- Therefore, thermal efficiency $= 269.12/548.05$
 $= 0.49 \text{ or } 49\%$

Exercise Problem # 1

- A turbojet engine inducts **51 kg** of air per second and propels an aircraft with a uniform flight speed of **912 km/h**. The enthalpy change for the nozzle is **200 kJ/kg**. The fuel-air ratio is **0.0119** and the heating value of the fuel is **42 MJ/kg**. Determine the thermal efficiency, TSFC, propulsive power.
- Ans: **0.34, 0.1034 kg/Nh, 8012 kW**.

Exercise Problem # 2

- A twin spool mixed turbofan engine operates with an overall pressure ratio of 18. The fan operates with a pressure ratio is 1.5 and the bypass ratio is 5.0. The turbine inlet temperature is 1200 K. If the engine is operating at a Mach number of 0.75 at an altitude where the ambient temperature and pressure are 240 K and 0.5 bar.
- Determine the thrust and the SFC.
- Ans: 74 kN, 0.027 kg/N h

Exercise Problem # 3

- An aircraft using a turboprop engine is flying at 800 km/h at an altitude where the ambient conditions are 0.567 bar and -20°C . Compressor pressure ratio is 8.0 and the turbine inlet temperature is 1100 K . Assuming that the turboprop does not generate any nozzle thrust, determine the specific power output and the thermal efficiency.
- Ans: 311 kJ/kg , 0.44