



Introduction to Aerospace Propulsion

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Lecture No - 32



In this lecture ...

- Ideal gas turbine cycles
- Thrust and efficiency
- The thrust equation
- Other engine performance parameters
- Ideal cycle for jet engines
 - Turbojet engine
 - Turbojet engine with afterburning

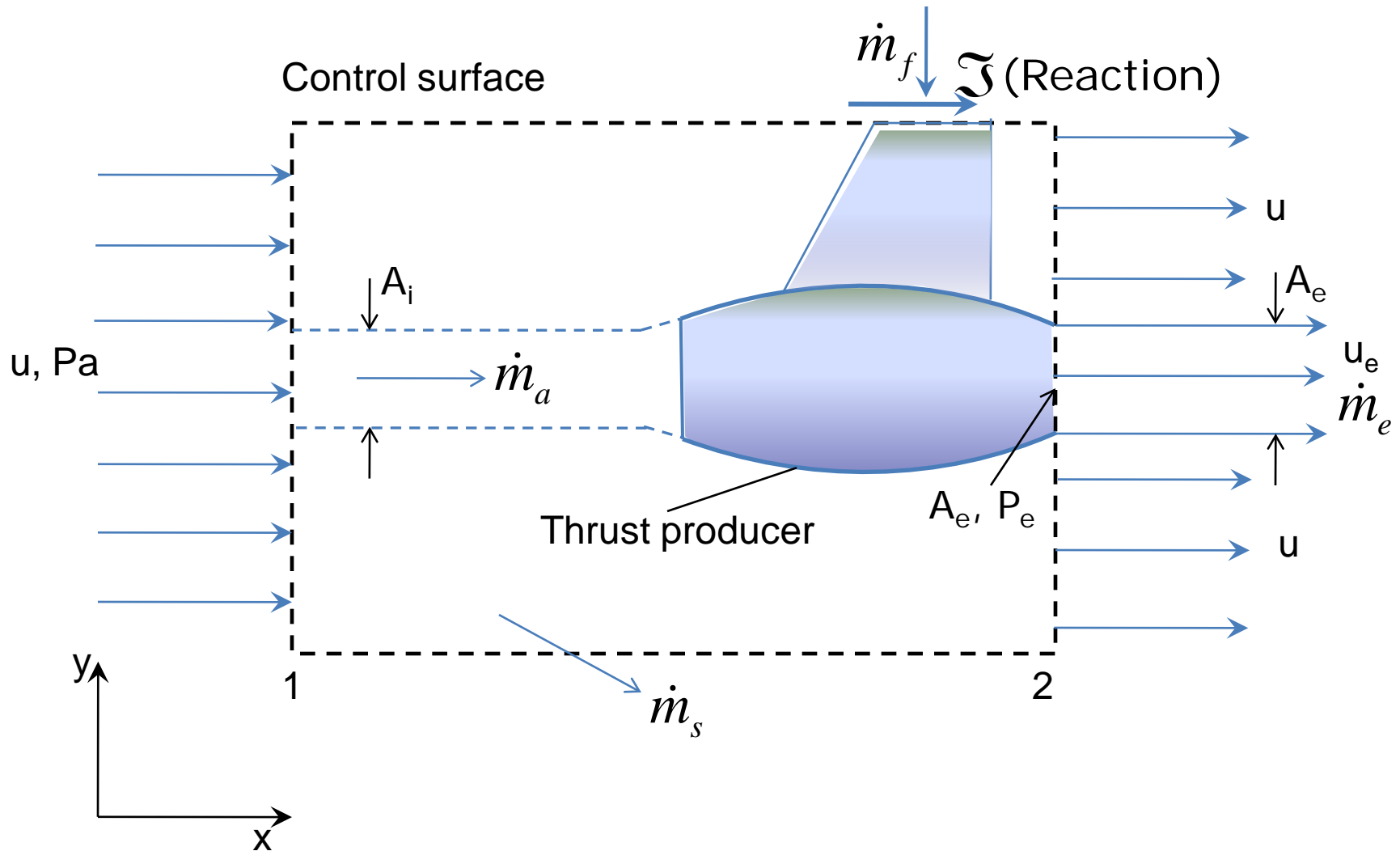
Gas turbine cycles

- Gas turbine engines operate on Brayton cycles.
- Ideal Brayton cycle is a closed cycle, whereas gas turbines operate in the open cycle mode.
- Ideal cycle assumes that there are no irreversibilities in the processes, air behaves like an ideal gas with constant specific heats, and that there are no frictional losses.

Thrust and efficiency

- We will now derive expressions for thrust and efficiency of air-breathing engines from the momentum and energy equations.
- We shall consider a generalized thrust producing device with a single inlet and single exhaust.
- We assume that the thrust and conditions at all points within the control volume do not change with time.

The thrust equation



The thrust equation

- The reaction to the thrust, \mathfrak{T} , is transmitted to the support. The engine thrust is thus the vector summation of all forces on the internal and external surfaces of the engine.

- Therefore,
$$\sum \vec{F} = \int_{CS} \vec{u} \rho(\vec{u} \cdot \vec{n}) dA$$

- Considering the components of force and the momentum flux in the x-direction only,

$$\sum F_x = \int_{CS} u_x \rho(\vec{u} \cdot \vec{n}) dA$$

The thrust equation

- The pressure and velocity can be assumed to be constant over the entire control surface, except over the exhaust area, A_e .
- The net pressure force acting on this control volume is $(P_a - P_e)A_e$.
- The only other force acting on the control volume is the reaction to the thrust, \mathfrak{T} .
- Adding up the forces in the x-direction,

$$\sum F_x = (P_a - P_e)A_e + \mathfrak{T}$$

The thrust equation

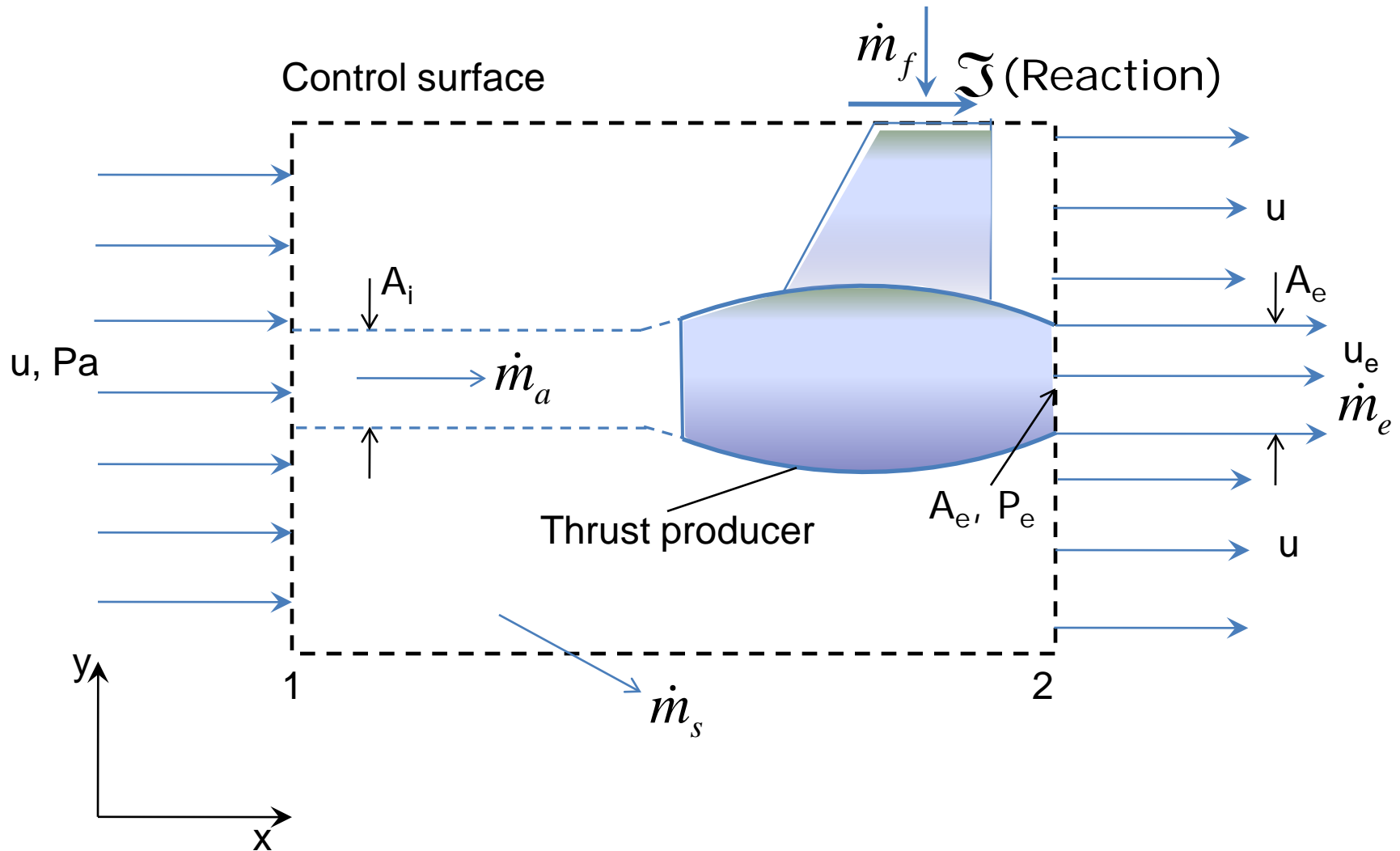
- The mass flow that enters the capture area, A_i , is $\dot{m}_a = \rho u A_i$
- Similarly, the mass flow crossing the exhaust area A_e , is, $\dot{m}_e = \rho_e u_e A_e$
- Also, $\dot{m}_e = \dot{m}_i + \dot{m}_f$
Or, $\dot{m}_f = \rho_e u_e A_e - \rho u A_i$
- Continuity equation for the CV gives,

$$\rho_e u_e A_e + \rho u (A - A_e) + \dot{m}_s - \dot{m}_f - \rho u A = 0$$

$$\text{Rearranging, } \dot{m}_s = \dot{m}_f + \rho u A_e - \rho_e u_e A_e$$

$$\text{Which is, } \dot{m}_s = \rho u (A_e - A_i)$$

The thrust equation



The thrust equation

- From the momentum balance across the CV,

$$\int_{CS} u_x \rho (\vec{u} \cdot \vec{n}) dA = \dot{m}_e u_e + \dot{m}_s u + \rho u (A - A_e) u - \dot{m}_a u - \rho u (A - A_i) u$$

- This is the net outward flux of x-momentum.
- This equation reduces to

$$\int_{CS} u_x \rho (\vec{u} \cdot \vec{n}) dA = \dot{m}_e u_e - \dot{m}_a u$$

- From the force balance equation, we have,

$$\mathcal{T} = \dot{m}_e u_e - \dot{m}_a u + (P_e - P_a) A_e$$

The thrust equation

- If we define fuel-air ratio, $f = \dot{m}_f / \dot{m}_a$

$$\mathcal{T} = \dot{m}_a [(1 + f)u_e - u] + (P_e - P_a)A_e$$

- This is the generalised thrust equation for air-breathing engines.
- The term $(P_e - P_a)A_e$ is not zero only if the exhaust jet is supersonic and the nozzle does not expand the exhaust jet to ambient pressure.
- However if $P_a \ll P_e$, it can be substantial contribution.

Engine performance parameters

- The engine performance is described by different efficiency definitions, thrust and the fuel consumption.
- The efficiency definitions that we shall now be discussing are applicable to an engine with a single propellant stream (turbojets or ramjets).
- For other types of jet engines (turbofan, turboprop) the equations need to be appropriately modified.

Engine performance parameters

- Propulsion efficiency: The ratio of thrust power to the rate of production of propellant kinetic energy.

$$\eta_P = \frac{\mathcal{T}u}{\dot{m}_a \left[(1+f)(u_e^2/2) - u^2/2 \right]}$$

- If we assume that $f \ll 1$ and the pressure thrust term is negligible,

$$\eta_P = \frac{(u_e - u)u}{u_e^2/2 - u^2/2} = \frac{2u/u_e}{1 + u/u_e}$$

Engine performance parameters

- Thermal efficiency: The ratio of the rate of production of propellant kinetic energy to the total energy consumption rate

$$\eta_{th} = \frac{\dot{m}_a \left[(1+f) \left(\frac{u_e^2}{2} \right) - \frac{u^2}{2} \right]}{\dot{m}_f Q_R} = \frac{\left[(1+f) \left(\frac{u_e^2}{2} \right) - \frac{u^2}{2} \right]}{f Q_R}$$

where, Q_R , is the heat of reaction of the fuel.

- For a turboprop or turboshaft engine, the output is largely shaft power. In this case,

$$\eta_{th} = \frac{P_s}{\dot{m}_f Q_R} \text{ where, } P_s, \text{ is the shaft power output of the engine.}$$

Engine performance parameters

- Overall efficiency: The product of thermal efficiency and propulsion efficiency.

$$\eta_o = \eta_p \eta_{th}$$

- In the case of aircraft that generate thrust using propellers,

$$\eta_o = \eta_{pr} \eta_{th}$$

Where, η_{pr} is the propeller efficiency.

Engine performance parameters

- Thrust specific fuel consumption, TSFC

$$TSFC = \frac{\dot{m}_f}{\mathfrak{T}} \approx \frac{\dot{m}_f}{\dot{m}_a [(1+f)u_e - u]}$$

- For turbine engines that produce shaft power, brake specific fuel consumption, BSFC

$$BSFC = \frac{\dot{m}_f}{P_s}$$

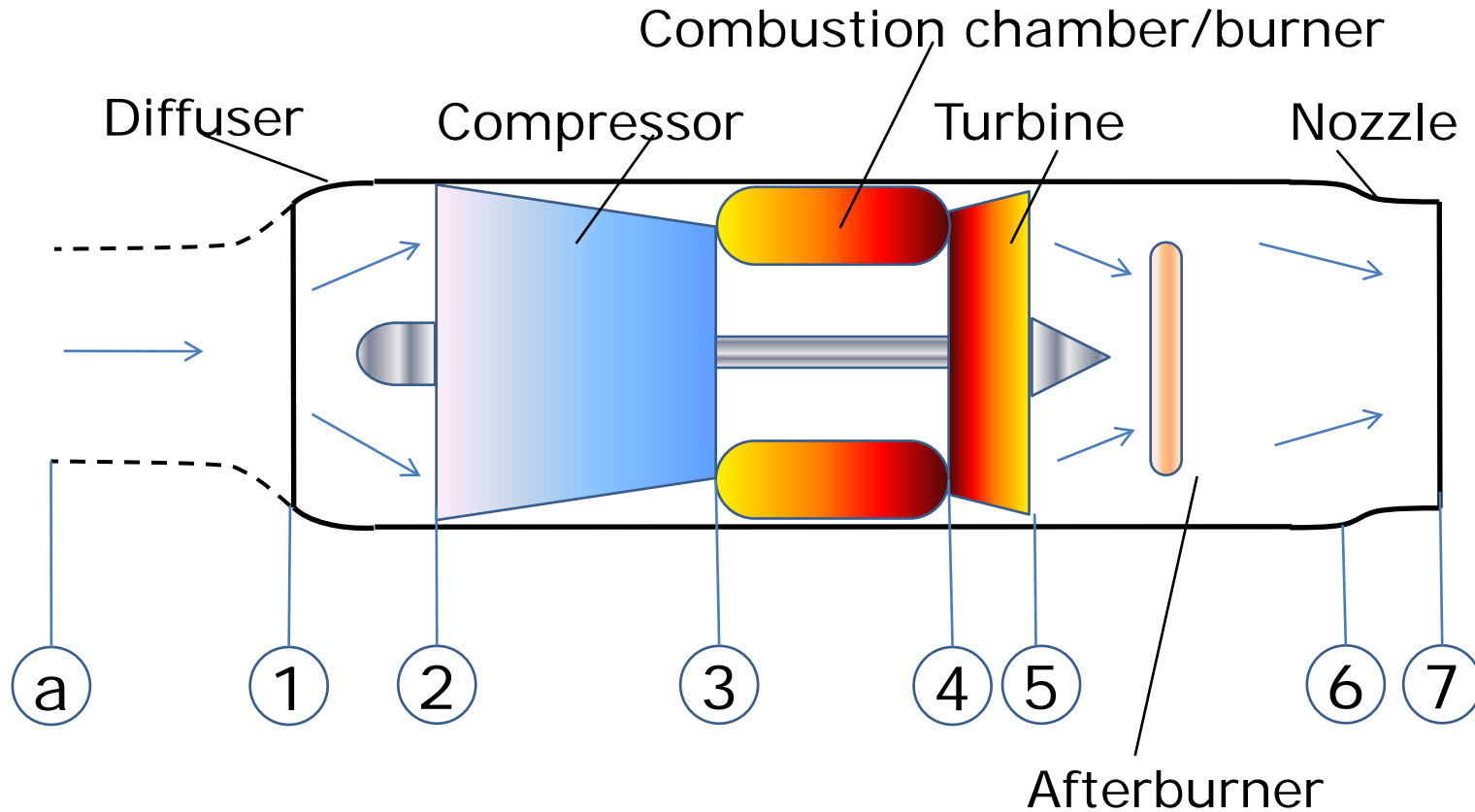
- For engine (like turboprop) that produce both, equivalent brake specific fuel consumption,

$$EBSFC = \frac{\dot{m}_f}{P_{es}} = \frac{\dot{m}_f}{P_s + \mathfrak{T}u}$$

Ideal cycle for jet engines

- All air-breathing jet engines operate on the Brayton cycle (open cycle mode).
- The most basic form of a jet engine is a turbojet engine.
- Some of the parameters of a jet engine cycle are usually design parameters and hence often fixed *a priori*: eg. compressor pressure ratio, turbine inlet temperature etc.
- Cycle analysis involves determining the performance parameters of the cycle with the known design parameters.

Ideal cycle for jet engines



Schematic of a turbojet engine and station numbering scheme

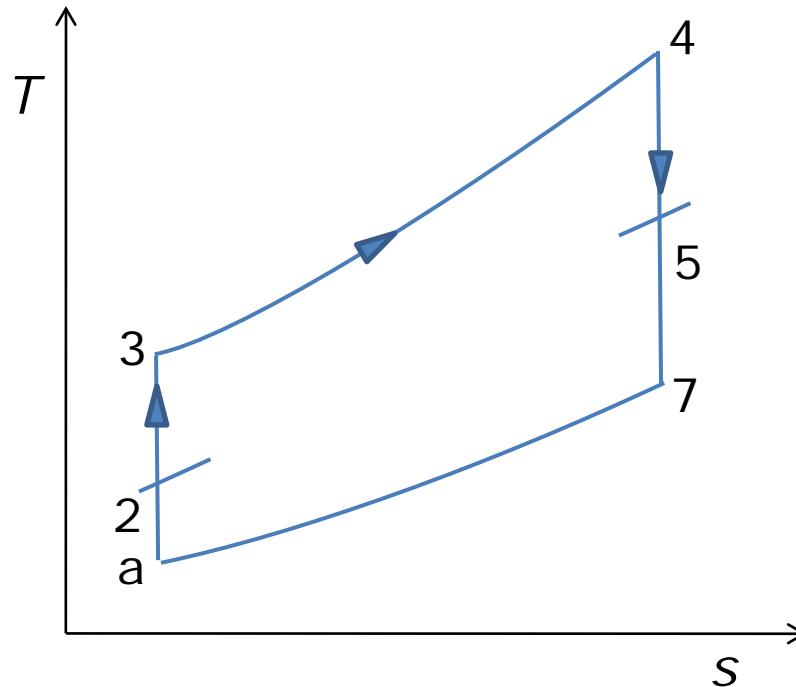
Ideal cycle for jet engines

- The different processes in a turbojet cycle are the following:
- a-1: Air from far upstream is brought to the air intake (diffuser) with some acceleration/deceleration
- 1-2: Air is decelerated as it passes through the diffuser
- 2-3: Air is compressed in a compressor (axial or centrifugal)
- 3-4 The air is heated using a combustion chamber/burner

Ideal cycle for jet engines

- 4-5: The air is expanded in a turbine to obtain power to drive the compressor
- 5-6: The air may or may not be further heated in an afterburner by adding further fuel
- 6-7: The air is accelerated and exhausted through the nozzle.

Ideal cycle for jet engines



Ideal turbojet cycle (without afterburning)
on a T-s diagram

Ideal cycle for jet engines

- For cycle analysis we shall take up each component and determine the exit conditions based on known inlet parameters.
- Intake: Ambient pressure, temperature and Mach number are known, P_a , T_a and M
- Intake exit stagnation temperature and pressure are determined from the isentropic relations:

$$T_{02} = T_a \left(1 + \frac{\gamma - 1}{2} M^2 \right)$$

$$P_{02} = P_a \left(\frac{T_{02}}{T_a} \right)^{\gamma/(\gamma-1)}$$

Ideal cycle for jet engines

- Compressor: Let the known compressor pressure ratio be denoted as π_c

$$P_{03} = \pi_c P_{02}$$

$$T_{03} = T_{02} (\pi_c)^{(\gamma-1)/\gamma}$$

- Combustion chamber: From energy balance,

$$h_{04} = h_{03} + fQ_R$$

$$\text{or, } f = \frac{T_{04}/T_{03} - 1}{Q_R / c_p T_{03} - T_{04}/T_{03}}$$

- Hence, we can determine the fuel-air ratio.

Ideal cycle for jet engines

- Turbine: Since the turbine produces work to drive the compressor, $W_{turbine} = W_{compressor}$

$$\dot{m}_t c_p (T_{04} - T_{05}) = \dot{m}_a c_p (T_{03} - T_{02})$$

$$\text{or, } (1 + f)(T_{04} - T_{05}) = (T_{03} - T_{02})$$

$$T_{05} = T_{04} - (T_{03} - T_{02}) / (1 + f)$$

$$\text{Hence, } P_{05} = P_{04} \left(\frac{T_{05}}{T_{04}} \right)^{\gamma / (\gamma - 1)}$$

For an ideal combustion chamber, $P_{04} = P_{03}$

Ideal cycle for jet engines

- Nozzle: With no afterburner, $T_{06} = T_{05}$, $P_{06} = P_{05}$

Therefore, the nozzle exit kinetic energy,

$$\frac{u_e^2}{2} = h_{07} - h_7$$

Since, $h_{07} = h_{06}$

$$u_e = \sqrt{2c_p T_{06} \left[1 - \left(P_a / P_{06} \right)^{(\gamma-1)/\gamma} \right]}$$

- Thrust, TSFC and efficiencies can now be determined using the formulae derived earlier.

Ideal cycle for jet engines

- Thrust, $\mathcal{T} = \dot{m}_a [(1 + f)u_e - u] + (P_e - P_a)A_e$

If $(P_e - P_a)A_e$ is negligible,

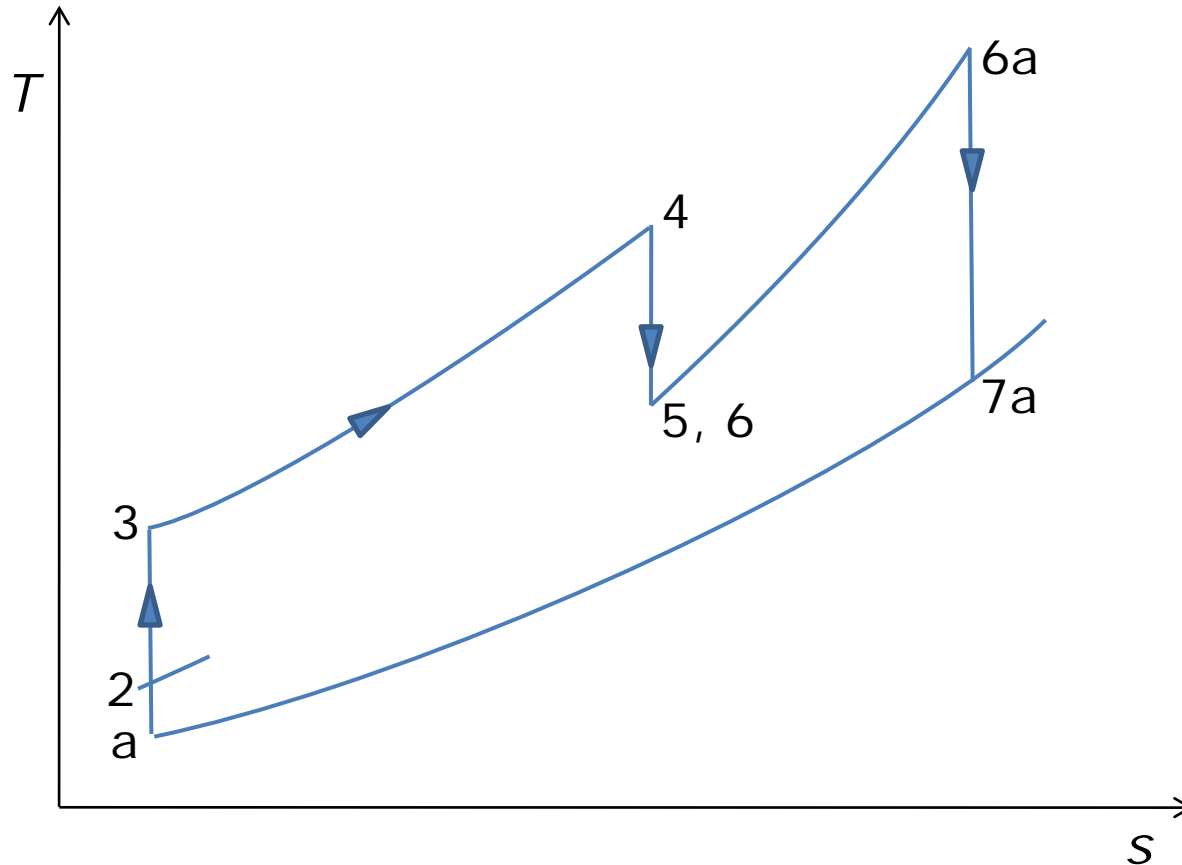
$$\mathcal{T} = \dot{m}_a [(1 + f)u_e - u]$$

- $TSFC = \frac{\dot{m}_f}{\mathcal{T}} \approx \frac{\dot{m}_f}{\dot{m}_a [(1 + f)u_e - u]}$

- Propulsion efficiency, $\eta_P = \frac{\mathcal{T}u}{\dot{m}_a [(1 + f)(u_e^2 / 2) - u^2 / 2]}$

- Thermal efficiency, $\eta_{th} = \frac{[(1 + f)(u_e^2 / 2) - u^2 / 2]}{fQ_R}$

Ideal cycle for jet engines



Ideal turbojet cycle with afterburning on a T - s diagram

Ideal cycle for jet engines

- Afterburning: used when the aircraft needs a substantial increment in thrust. For eg. to accelerate to and cruise at supersonic speeds.
- Since the air-fuel ratio in gas turbine engines are much greater than the stoichiometric values, there is sufficient amount of air available for combustion at the turbine exit.
- There are no rotating components like a turbine in the afterburner, the temperatures can be taken to much higher values than that at turbine entry.

Ideal cycle for jet engines

- For calculating the fuel flow rate required to achieve a temperature of T_{6a} , we carry out an energy balance,

$$h_{06a} = h_{05} + f_2 Q_R$$

$$\text{or, } f_2 = \frac{T_{06a} / T_{05} - 1}{Q_R / c_p T_{05} - T_{06} / T_{05}}$$

Where, $f = f_1 + f_2$, f is the total fuel flow ratio, f_1 is the fuel flow ratio in the main combustor.

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In the next lecture ...

- Ideal cycle for jet engines
 - Turbofan engine
 - Different configurations of turbofan engines
 - Turboprop engines
 - Turboshaft engines
 - Ramjets