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In this lecture...

• Performance parameters: cascade analysis

TURBOMACHINERY AERODYNAMICS

 2-D losses in axial compressor stage – primary losses

Performance parameters

- Measurements from cascade: velocities, pressures, flow angles ...
- Loss in total pressure expressed as total pressure loss coefficient

$$\overline{\omega}_{\text{PLC}} = \frac{\mathsf{P}_{01} - \mathsf{P}_{02}}{\frac{1}{2}\,\rho\mathsf{V}_1^2}$$

- Total pressure loss is very sensitive to changes in the incidence angle.
- At very high incidences, flow is likely to separate from the blade surfaces, eventually leading to stalling of the blade.

Performance parameters

 Blade performance/loading can be assessed using static pressure coefficient:

$$C_{P} = \frac{P_{local} - P_{ref}}{\frac{1}{2}\rho V_{1}^{2}}$$

Where, P_{local} is the blade surface static pressure and P_{ref} is the reference static pressure (usually measured at the cascade inlet)

 The C_P distribution (usually plotted as C_P vs. x/C) gives an idea about the chordwise load distribution.

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Performance parameters



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Performance parameters



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Performance parameters



- Nature of losses in an axial compressor
 - Viscous losses
 - 3-D effects like tip leakage flows, secondary flows etc.
 - Shock losses
 - Mixing losses
- Estimating the losses crucial designing loss control mechanisms.
- However isolating these losses not easy and often done through empirical correlations.
- Total losses in a compressor is the sum of the above losses.

- Viscous losses
 - Profile losses: on account of the profile or nature of the airfoil cross-sections
 - Annulus losses: growth of boundary layer along the axis
 - Endwall losses: boundary layer effects in the corner (junction between the blade surface and the casing/hub)
- 3-D effects:
 - Secondary flows: flow through curved blade passages
 - Tip leakage flows: flow from pressure surface to suction surface at the blade tip

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Losses in a compressor blade

• The loss manifests itself in the form of stagnation pressure loss (or entropy increase).

$$\frac{\Delta s}{R} = -\ln \frac{P_{02}}{P_{01}} = -\ln \left[1 - \frac{(\Delta P_o)_{loss}}{P_{01}}\right]$$

Expanding the above equation in an infinite series,

$$\frac{\Delta S}{R} = \frac{(\Delta P_o)_{loss}}{P_{01}} + \frac{1}{2} \left(\frac{(\Delta P_o)_{loss}}{P_{01}}\right)^2 + \dots$$

Neglecting higher order terms, $\frac{\Delta}{c}$

$$\frac{\Delta s}{R} = \frac{(\Delta P_o)_{loss}}{P_{01}}$$

Since,
$$\omega = \frac{(\Delta P_o)_{loss}}{\frac{1}{2}\rho V_1^2} = \frac{\Delta s}{R} \frac{P_{01}}{\frac{1}{2}\rho V_1^2}$$

or, $\frac{\Delta s}{R} = \left(\frac{\omega \rho V_1^2}{2P_{01}}\right)$

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Losses in a compressor blade

• The overall losses in a turbomachinery can be summarised as:

$$\begin{split} & \omega = \omega_{\text{P}} + \omega_{\text{sh}} + \omega_{\text{s}} + \omega_{\text{L}} + \omega_{\text{E}} \\ & \text{Where, } \omega_{\text{P}} : \text{profile losses} \\ & \omega_{\text{sh}} : \text{shock losses} \\ & \omega_{\text{s}} : \text{secondary flow loss} \\ & \omega_{\text{L}} : \text{tip leakage loss} \\ & \omega_{\text{F}} : \text{Endwall losses} \end{split}$$

- 2-D losses are relevant only to axial flow turbomachines.
- These are mainly associated with blade boundary layers, shock-boundary layer interactions, separated flows and wakes.
- The mixing of the wake downstream produces additional losses called mixing losses.
- The maximum losses occur near the blade surface and minimum loss occurs near the edge of the boundary layer.

- 2-D losses can be classified as:
 - Profile loss due to boundary layer, including laminar and/or turbulent separation.
 - Wake mixing losses
 - Shock losses
 - Trailing edge loss due to the blade.

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- The profile loss depends upon:
 - Flow parameters like Reynolds number, Mach number, longitudinal curvature of the blade, inlet turbulence, free-stream unsteadiness and the resulting unsteady boundary layers, pressure gradient, and shock strength
 - Blade parameters like: thickness, camber, solidity, sweep, skewness of the blade, stagger angle and blade roughness.

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- The mixing losses arise as a result of the mixing of the wake with the freestream.
- This depends upon, in addition to the parameters mentioned in the previous slide, the distance downstream.
- The physical mechanism is the exchange of momentum and energy between the wake and the freestream.
- This transfer of energy results in the decay of the free shear layer, increased wake centre line velocity and increased wake width.

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- At far downstream, the flow becomes uniform.
- Theoretically, the difference between the stagnation pressure far downstream and the trailing edge represents the mixing loss.
- Most loss correlations are based on measurements downstream of the trailing edge (1/2 to 1 chord length) and therefore do not include all the mixing losses.
- If there is flow separation, the losses would include losses due to this zone and at its eventual mixing downstream.

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2-D Losses in a compressor blade

The profile and mixing losses along a streamline can be written as :

$$\overline{\omega}_{p+m} = \frac{2(\mathsf{P}_{0t} - \mathsf{P}_{02})}{\rho \mathsf{V}_1^2}$$

To determine the above, it is necessary to relate the static pressure difference and velocities to the displacement and momentum thickness of the blade boundary layer at the trailing edge.

2-D Losses in a compressor blade

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Detailed derivation of these correlations are given in Lakshminarayana's book (Chapter 6).

$$\overline{\omega}_{p+m} = \frac{2(P_{0t} - P_{02})}{\rho V_1^2} = \frac{2(p_t - p_2)}{\rho V_1^2} + \frac{V_t^2 - V_2^2}{V_1^2}$$

This is further expressed as :

$$\overline{\omega}_{p+m} \sec^2 \alpha_1 = \left[\frac{2\Theta + \Delta^2}{(1 - \Delta)^2} + \tan^2 \alpha_2 \left\{ \frac{(1 - \Delta)^2}{(1 - \Theta - \Delta)^2} - 1 \right\} \right]$$

Neglecting higher order terms,

$$\overline{\omega}_{p+m} \sec^2 \alpha_1 = 2(\Theta + \Theta \tan^2 \alpha_2)$$

Where, Δ is the blockage (related to displacement thickness) and Θ is the momentum thicknesss.

- Thus, in a simplified manner, we see that the profile loss can be estimated based on the momentum thickness.
- The above loss correlation includes both profile and wake mixing loss.
- If flow separation occurs, additional losses are incurred. This is because the pressure distribution is drastically altered beyond the separation point.
- The losses increase due to increase in boundary layer displacement and momentum thicknesses.

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2-D Losses in a compressor blade

- In addition to the losses discussed above, boundary layer growth and subsequent decay of the wake causes deviation in the outlet angle.
- An estimate of this is given as:

 $\tan \alpha_2 \approx (1 - \Theta - \Delta) \tan \alpha_t$

- Hence, viscous effect in a turbomachine always leads to decrease in the turning angle.
- The values of displacement and momentum thicknesses, depend upon, variation of freestream velocity, Mach number, skin friction, pressure gradient, turbulence intensity and Reynolds number.

- In general, the loss estimation may be carried out using one of the following methods:
 - Separate calculation of the potential or inviscid flow and the displacement and momentum thicknesses. Subsequently, use the equation discussed previously.
 - Using a Navier-Stokes based computational code. Here the local and the integrated losses can be computed directly.

Mach number and shock losses

- The static pressure rise in a compressor increases with Mach number.
- Thus the pressure gradient increases with increase in Mach number.
- This means that the momentum thickness and hence the losses increase with Mach number.
- Increasing Mach numbers also lead to increase in shock losses.
- At transonic speeds, the shock losses are very sensitive to leading and trailing edge geometries.

Mach number and shock losses

- An estimate of the 2-D shock losses for a compressor must include:
 - The losses due to the leading edge bluntness with supersonic upstream Mach number.
 - The location of the passage shock can be determined from inviscid theories. If the shock strength is known, the losses can be estimated.
 - The losses due to boundary layer growth and the shock-boundary layer interaction are most difficult to estimate. The contribution however is small for weak shocks.

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Mach number and shock losses

 One of the empirical correlations for the shock loss was given by Freeman and Cumpsty (1989).

$$\omega_{sh} = \frac{(\Delta P_0)_{loss}}{P_{01} - P_1} = \left[\frac{(\Delta P_0)_{loss}}{P_{01} - P_1}\right]_{normal shock} + \left[2.6 + 0.18(\alpha_1 - 65^0)\right] 10^{-2}(\alpha_1 - \alpha_1)$$

where, α_1 is the blade inlet angle.

- This is valid for an incidence angle upto 5°.
- These empirical correlations are however, derived using the 2-D assumption.
- Actual flows are seldom 2-D in nature.

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In the next lecture...

• Tutorial: solved examples and tutorial problems.