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Prof. Bhaskar Roy, Prof. A M Pradeep **Department of Aerospace Engineering, IIT Bombay**

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In this lecture...

• Performance parameters: cascade analysis

TURBOMACHINERY AERODYNAMICS

• 2-D losses in axial compressor stage – primary losses

Performance parameters

- Measurements from cascade: velocities, pressures, flow angles ...
- Loss in total pressure expressed as total pressure loss coefficient

$$
\overline{\omega}_{\text{PLC}} = \frac{P_{01} - P_{02}}{\frac{1}{2}\rho V_1^2}
$$

- Total pressure loss is very sensitive to changes in the incidence angle.
- At very high incidences, flow is likely to separate from the blade surfaces, eventually leading to stalling of the blade.

Performance parameters

• Blade performance/loading can be assessed using static pressure coefficient:

$$
C_{\text{P}} = \frac{P_{\text{local}} - P_{\text{ref}}}{\frac{1}{2}\rho V_1^2}
$$

at the cascade inlet) P_{ref} is the reference static pressure (usually measured Where, $\mathsf{P}_\mathsf{local}$ is the blade surface static pressure and

• The C_P distribution (usually plotted as C_P *vs. x/C*) gives an idea about the chordwise load distribution.

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Performance parameters

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Performance parameters

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Performance parameters

- Nature of losses in an axial compressor
	- Viscous losses
	- 3-D effects like tip leakage flows, secondary flows etc.
	- Shock losses
	- Mixing losses
- Estimating the losses crucial designing loss control mechanisms.
- However isolating these losses not easy and often done through empirical correlations.
- Total losses in a compressor is the sum of the above losses.

- Viscous losses
	- Profile losses: on account of the profile or nature of the airfoil cross-sections
	- Annulus losses: growth of boundary layer along the axis
	- Endwall losses: boundary layer effects in the corner (junction between the blade surface and the casing/hub)
- 3-D effects:
	- Secondary flows: flow through curved blade passages
	- Tip leakage flows: flow from pressure surface to suction surface at the blade tip

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Losses in a compressor blade

• The loss manifests itself in the form of stagnation pressure loss (or entropy increase).

$$
\frac{\Delta s}{R} = -\ln \frac{P_{02}}{P_{01}} = -\ln \left[1 - \frac{(\Delta P_o)_{loss}}{P_{01}} \right]
$$

Expanding the above equation in an infinite series,

$$
\frac{\Delta s}{R} = \frac{(\Delta P_o)_{\text{loss}}}{P_{01}} + \frac{1}{2} \left(\frac{(\Delta P_o)_{\text{loss}}}{P_{01}} \right)^2 + \dots
$$

Neglecting higher order terms, $\frac{\Delta s}{R} = \frac{(\Delta s)^2}{4\Delta}$

$$
\frac{\Delta S}{R} = \frac{(\Delta P_o)_{loss}}{P_{01}}
$$

Since,
$$
\omega = \frac{(\Delta P_o)_{loss}}{\frac{1}{2}\rho V_1^2} = \frac{\Delta s}{R} \frac{P_{01}}{\frac{1}{2}\rho V_1^2}
$$

or, $\frac{\Delta s}{R} = \left(\frac{\omega \rho V_1^2}{2P_{01}}\right)$

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Losses in a compressor blade

• The overall losses in a turbomachinery can be summarised as:

> ω_{E} : Endwall losses $\omega_{\text{\tiny L}}$: tip leakage loss ω_{s} : secondary flow loss $\omega_{\sf sh}$: shock losses Where, $\omega_\text{\tiny{P}}$: profile losses $\omega = \omega_{\rm p} + \omega_{\rm sh} + \omega_{\rm s} + \omega_{\rm L} + \omega_{\rm E}$

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- 2-D losses are relevant only to axial flow turbomachines.
- These are mainly associated with blade boundary layers, shock-boundary layer interactions, separated flows and wakes.
- The mixing of the wake downstream produces additional losses called mixing losses.
- The maximum losses occur near the blade surface and minimum loss occurs near the edge of the boundary layer.

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- 2-D losses can be classified as:
	- Profile loss due to boundary layer, including laminar and/or turbulent separation.
	- Wake mixing losses
	- Shock losses
	- Trailing edge loss due to the blade.

2-D Losses in a compressor blade

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- The profile loss depends upon:
	- Flow parameters like Reynolds number, Mach number, longitudinal curvature of the blade, inlet turbulence, free-stream unsteadiness and the resulting unsteady boundary layers, pressure gradient, and shock strength
	- Blade parameters like: thickness, camber, solidity, sweep, skewness of the blade, stagger angle and blade roughness.

- The mixing losses arise as a result of the mixing of the wake with the freestream.
- This depends upon, in addition to the parameters mentioned in the previous slide, the distance downstream.
- The physical mechanism is the exchange of momentum and energy between the wake and the freestream.
- This transfer of energy results in the decay of the free shear layer, increased wake centre line velocity and increased wake width.

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- At far downstream, the flow becomes uniform.
- Theoretically, the difference between the stagnation pressure far downstream and the trailing edge represents the mixing loss.
- Most loss correlations are based on measurements downstream of the trailing edge (1/2 to 1 chord length) and therefore do not include all the mixing losses.
- If there is flow separation, the losses would include losses due to this zone and at its eventual mixing downstream.

2-D Losses in a compressor blade

streamline can be written as : The profile and mixing losses along a

$$
\overline{\omega}_{p+m} = \frac{2(P_{0t} - P_{02})}{\rho V_1^2}
$$

boundary layer at the trailing edge. displacement and momentum thickness of the blade the static pressure difference and velocities to the To determine the above, it is necessary to relate

2-D Losses in a compressor blade

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given in Lakshminarayana's book (Chapter 6). Detailed derivation of these correlations are

$$
\overline{\omega}_{p+m} = \frac{2(P_{0t} - P_{02})}{\rho V_1^2} = \frac{2(p_t - p_2)}{\rho V_1^2} + \frac{V_t^2 - V_2^2}{V_1^2}
$$

This is further expressed as :

$$
\overline{\omega}_{p+m} \sec^2 \alpha_1 = \left[\frac{2\Theta + \Delta^2}{(1-\Delta)^2} + \tan^2 \alpha_2 \left\{ \frac{(1-\Delta)^2}{(1-\Theta - \Delta)^2} - 1 \right\} \right]
$$

Neglecting higher order terms,

$$
\overline{\omega}_{p+m}
$$
 sec² $\alpha_1 = 2(\Theta + \Theta \tan^2 \alpha_2)$

thickness) and Θ is the momentum thicknesss. Where, Δ is the blockage (related to displacement

- Thus, in a simplified manner, we see that the profile loss can be estimated based on the momentum thickness.
- The above loss correlation includes both profile and wake mixing loss.
- If flow separation occurs, additional losses are incurred. This is because the pressure distribution is drastically altered beyond the separation point.
- The losses increase due to increase in boundary layer displacement and momentum thicknesses.

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2-D Losses in a compressor blade

- In addition to the losses discussed above, boundary layer growth and subsequent decay of the wake causes deviation in the outlet angle.
- An estimate of this is given as:

 $\tan \alpha_2 \approx (1 - \Theta - \Delta) \tan \alpha_1$

- Hence, viscous effect in a turbomachine always leads to decrease in the turning angle.
- The values of displacement and momentum thicknesses, depend upon, variation of freestream velocity, Mach number, skin friction, pressure gradient, turbulence intensity and Reynolds number.

- In general, the loss estimation may be carried out using one of the following methods:
	- Separate calculation of the potential or inviscid flow and the displacement and momentum thicknesses. Subsequently, use the equation discussed previously.
	- Using a Navier-Stokes based computational code. Here the local and the integrated losses can be computed directly.

Mach number and shock losses

- The static pressure rise in a compressor increases with Mach number.
- Thus the pressure gradient increases with increase in Mach number.
- This means that the momentum thickness and hence the losses increase with Mach number.
- Increasing Mach numbers also lead to increase in shock losses.
- At transonic speeds, the shock losses are very sensitive to leading and trailing edge geometries.

Mach number and shock losses

- An estimate of the 2-D shock losses for a compressor must include:
	- The losses due to the leading edge bluntness with supersonic upstream Mach number.
	- The location of the passage shock can be determined from inviscid theories. If the shock strength is known, the losses can be estimated.
	- The losses due to boundary layer growth and the shock-boundary layer interaction are most difficult to estimate. The contribution however is small for weak shocks.

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Mach number and shock losses

• One of the empirical correlations for the shock loss was given by Freeman and Cumpsty (1989).

$$
\omega_{sh} = \frac{(\Delta P_0)_{loss}}{P_{01} - P_1} = \left[\frac{(\Delta P_0)_{loss}}{P_{01} - P_1} \right]_{normalshock} + [2.6 + 0.18(\alpha_1' - 65^\circ)] 10^{-2} (\alpha_1 - \alpha_1')
$$

where, $\alpha_1^{'}$ is the blade inlet angle.

- This is valid for an incidence angle upto 5^o.
- These empirical correlations are however, derived using the 2-D assumption.
- Actual flows are seldom 2-D in nature.

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In the next lecture...

• Tutorial: solved examples and tutorial problems.