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In this lecture...

- Axial flow turbine
 - Impulse and reaction turbine stages
 - Work and stage dynamics
 - Turbine blade cascade

TURBOMACHINERY AERODYNAMICS

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Axial flow turbines

• Axial turbines like axial compressors usually consists of one or more stages.

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- The flow is accelerated in a nozzle/stator and then passes through a rotor.
- In the rotor, the working fluid imparts its momentum on to the rotor, that converts the kinetic energy to power output.
- Depending upon the power requirement, this process is repeated in multiple stages.

Axial flow turbines

- Due to motion of the rotor blades→ two distinct velocity components: absolute and relative velocities in the rotor.
- This is very much the case in axial compressors that was discussed earlier.
- Since turbines operate with a favourable pressure gradient, it is possible to have much higher pressure drop per stage as compared with compressors.
- Therefore, a single turbine stage can drive several stages of an axial compressor.

Axial flow turbines

- Turbines can be either axial, radial or mixed.
- Axial turbines can handle large mass flow rates and are more efficient.
- Axial turbine have same frontal area as that of the compressor.
- They can also be used with a centrifugal compressor.
- Efficiency of turbines higher than that of compressors.
- Turbines are in general aerodynamically "easier" to design.

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Axial flow turbines



Velocity triangles

- Elementary analysis of axial turbines too begins with velocity triangles.
- The analysis will be carried out at the mean height of the blade, where the peripheral velocity or the blade speed is, *U*.
- The absolute component of velocity will be denoted by, *C* and the relative component by, *V*.
- The axial velocity (absolute) will be denoted by C_a and the tangential components will be denoted by subscript w (for eg, C_w or V_w)
- α denotes the angle between the absolute velocity with the axial direction and β the corresponding angle for the relative velocity.

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Velocity triangles



Types of axial turbines

- There are two types of axial turbine configurations: Impulse and reaction
- Impulse turbine
 - Entire pressure drop takes place in the nozzle.
 - Rotor blades simply deflect the flow and hence have symmetrical shape.
- Reaction turbine
 - Pressure drop shared by the rotor and the stator
 - The amount of pressure drop shared is given by the degree of reaction.

Work and stage dynamics

Applying the angular momentum equation, $P = \dot{m}(U_2C_{w2} - U_3C_{w3})$ In an axial turbine, $U_2 \approx U_3 = U$. Therefore, the work per unit mass is $W_{t} = U(C_{w2} - C_{w3})$ or $W_{t} = C_{p}(T_{01} - T_{03})$ Let $\Delta T_0 = T_{01} - T_{03} = T_{02} - T_{03}$ The stage work ratio is, $\frac{\Delta T_0}{T_{01}} = \frac{U(C_{w2} - C_{w3})}{C_p T_{01}}$

Work and stage dynamics

- Turbine work per stage is limited by
 - Available pressure ratio
 - Allowable blade stresses and turning
- Unlike compressors, boundary layers are generally well behaved, except for local pockets of separation
- The turbine work ratio is also often defined in the following way:

$$\frac{\mathsf{W}_{\mathsf{t}}}{\mathsf{U}^2} = \frac{\Delta \mathsf{h}_0}{\mathsf{U}^2} = \frac{\mathsf{C}_{\mathsf{w}2} - \mathsf{C}_{\mathsf{w}3}}{\mathsf{U}}$$

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Impulse turbine stage



Impulse turbine stage

In an impulse turbine, the rotor simply deflects the flow. Therefore,

$$\beta_{3} = -\beta_{2} \implies V_{w3} = -V_{w2}$$

and $C_{w2} - C_{w3} = 2V_{w2} = 2(C_{w2} - U)$
$$= 2U\left(\frac{C_{a}}{U}\tan\alpha - 1\right)$$

Or, the turbine work ratio is

$$\frac{\Delta h_0}{U^2} = 2U \left(\frac{C_a}{U} \tan \alpha_2 - 1 \right)$$

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50% Reaction turbine stage



Stator/Nozzle Rotor

Impulse turbine stage

In a 50% reaction turbine, the velocity triangles are symmetrical. Therefore, for constant axial velocity,

$$C_{w3} = -(C_a \tan \alpha_2 - U)$$

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And the turbine work ratio becomes

$$\frac{\Delta h_0}{U^2} = \left(2\frac{C_a}{U}\tan\alpha_2 - 1\right)$$

- A cascade is a stationary array of blades.
- Cascade is constructed for measurement of performance similar to that used in axial turbines.
- Cascade usually has porous end-walls to remove boundary layer for a two-dimensional flow.
- Radial variations in the velocity field can therefore be excluded.
- Cascade analysis relates the fluid turning angles to blading geometry and measure losses in the stagnation pressure.

- Turbine cascades are tested in wind tunnels similar to what was discussed for compressors.
- However, turbines operate in an accelerating flow and therefore, the wind tunnel flow driver needs to develop sufficient pressure to cause this acceleration.
- Turbine blades have much higher camber and are set at a negative stagger unlike compressor blades.
- Cascade analysis provides the blade loading from the surface static pressure distribution and the total pressure loss across the cascade.

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Turbine Cascade



- From elementary analysis of the flow through a cascade, we can determine the lift and drag forces acting on the blades.
- This analysis could be done using inviscid or potential flow assumption or considering viscous effects (in a simple manner).
- Let us consider V_m as the mean velocity that makes and angle α_m with the axial direction.
- We shall determine the circulation developed on the blade and subsequently the lift force.
- In the inviscid analysis, lift is the only force.

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Turbine Cascade



Inviscid flow through a turbine cascade

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Turbine Cascade

Circulation, $\Gamma = S(V_{w2} - V_{w1})$ and lift, $L = \rho V_m \Gamma = \rho V_m S(V_{w2} - V_{w1})$ Expressing lift in a non - dimensional form, Lift coefficient, $C_L = \frac{L}{\frac{1}{2}\rho V_m^2 C} = \frac{\rho V_m S(V_{w2} - V_{w1})}{\frac{1}{2}\rho V_m^2 C}$ Circulation axis $\sqrt[V_{n}]{} = 2\frac{S}{C}(\tan\alpha_{2} - \tan\alpha_{1})\cos\alpha_{m}$ νm ۲, V2

- Viscous effects manifest themselves in the form to total pressure losses.
- Wakes from the blade trailing edge lead to non-uniform velocity leaving the blades.
- In addition to lift, drag is another force that will be considered in the analysis.
- The component of drag actually contributes to the effective lift.
- We define total pressure loss coefficient as:

$$\overline{\omega} = \frac{\mathsf{P}_{01} - \mathsf{P}_{02}}{\frac{1}{2}\,\rho\mathsf{V}_2^2}$$

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Turbine Cascade



Viscous flow through a turbine cascade

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Drag is given by, $D = \overline{\omega} S \cos \alpha_m$ The effective lift $L + \overline{\omega} S \cos \alpha_m = \rho V_m \Gamma + \overline{\omega} S \cos \alpha_m$ Therefore, the lift coefficient, $C_L = 2 \frac{S}{C} (\tan \alpha_2 - \tan \alpha_1) \cos \alpha_m + C_D \tan \alpha_m$

- Based on the calculation of the lift and drag coefficients, it is possible to determine the blade efficiency.
- Blade efficiency is defined as the ratio of ideal static pressure drop to obtain a certain change in KE to the actual static pressure drop to produce the same change in KE.

$$\eta_{\text{b}} = \frac{1 - \frac{C_{\text{D}}}{C_{\text{L}}} \tan \alpha_{\text{m}}}{1 + \frac{C_{\text{D}}}{C_{\text{L}}} \cot \alpha_{\text{m}}}$$

If we neglect the C_D term in the lift definition,

$$\eta_{\text{b}} = \frac{1}{1 + \frac{2C_{\text{D}}}{C_{\text{L}} \sin 2\alpha_{\text{m}}}}$$

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In the next lecture...

- Axial flow turbine
 - Degree of Reaction, Losses and Efficiency