#### <u>Lecture – 26</u>

<u>Classical Numerical Methods to Solve</u> Optimal Control Problems

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# Necessary Conditions of Optimality in Optimal Control

State Equation

$$\dot{X} = \frac{\partial H}{\partial \lambda} = f(t, X, U)$$

Costate Equation

$$\dot{\lambda} = -\left(\frac{\partial H}{\partial X}\right) = g\left(t, X, U\right)$$

 Optimal Control Equation

$$\left(\frac{\partial H}{\partial U}=0\right) \quad \Rightarrow \quad U=\psi(X,\lambda)$$

• Boundary Condition  $\lambda$ 

$$_{f} = \frac{\partial \varphi}{\partial X_{f}} \qquad X(t_{0}) = X_{0}:$$
 Fixed

# **Necessary Conditions of Optimality: Salient Features**

- State and Costate equations are dynamic equations
- State equation develops forward whereas Costate equation develops backwards
- Optimal control equation is a stationary equation
- The formulation leads to Two-Point-Boundary-Value Problems (TPBVPs), which demand computationally-intensive iterative numerical procedures to obtain the optimal control solution

### **Classical Methods to Solve TPBVPs**

Gradient Method

Shooting Method

Quasi-Linearization Method

Gradient Method

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# **Gradient Method**

- Assumptions:
  - State equation satisfied
  - Costate equation satisfied
  - Boundary conditions satisfied
- Strategy:
  - Satisfy the optimal control equation

### **Gradient Method**

$$\begin{split} \delta \overline{J} &= \left(\delta X_{f}\right)^{T} \left[\frac{\partial \phi}{\partial X_{f}} - \lambda_{f}\right] \\ &+ \int_{t_{0}}^{t_{f}} \left(\delta X\right)^{T} \left[\frac{\partial H}{\partial X} + \dot{\lambda}\right] dt \\ &+ \int_{t_{0}}^{t_{f}} \left(\delta U\right)^{T} \left[\frac{\partial H}{\partial U}\right] dt \\ &+ \int_{t_{0}}^{t_{f}} \left(\delta \lambda\right)^{T} \left[\frac{\partial H}{\partial \lambda} - \dot{X}\right] dt \end{split}$$

### **Gradient Method**

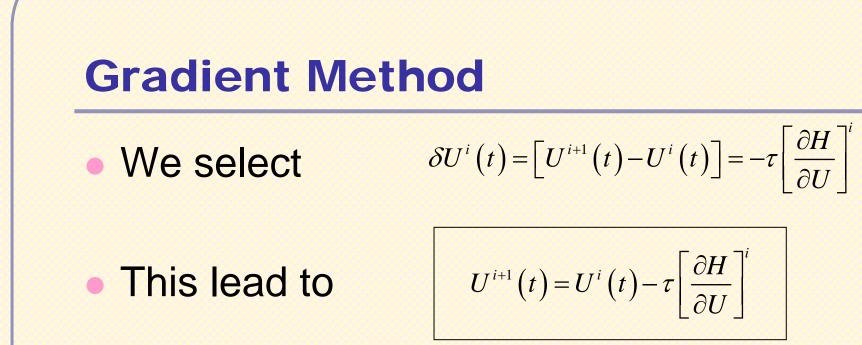
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 After satisfying the state & costate equations and boundary conditions, we have

$$\delta \overline{J} = \int_{t_0}^{t_f} \left(\delta U\right)^T \left[\frac{\partial H}{\partial U}\right] dt$$

$$\delta U(t) = -\tau \left[\frac{\partial H}{\partial U}\right], \quad \tau > 0$$

• This leads to 
$$\delta \overline{J} = -\tau \int_{t_0}^{t_f} \left[\frac{\partial H}{\partial U}\right]^T \left[\frac{\partial H}{\partial U}\right] dt$$



• Note: 
$$\delta \overline{J} = -\tau \int_{t_0}^{t_f} \left[ \frac{\partial H}{\partial U} \right]^T \left[ \frac{\partial H}{\partial U} \right] dt \le 0$$
  
• Eventually,  $\delta \overline{J} = 0 \implies \frac{\partial H}{\partial U} = 0$ 

# **Gradient Method: Procedure**

- Assume a control history (not a trivial task)
- Integrate the state equation forward
- Integrate the costate equation backward
- Update the control solution
  - This can either be done at each step while integrating the costate equation backward or after the integration of the costate equation is complete
- Repeat the procedure until convergence

 $\int_{0}^{t_{f}} \left[ \frac{\partial H}{\partial U} \right]^{t} \left[ \frac{\partial H}{\partial U} \right] dt \leq \gamma \quad \text{(a pre-selected constant)}$ 



- Select τ so that it leads to a certain percentage reduction of J
- Let the percentage be  $\alpha$
- Then  $\tau \int_{t_0}^{t_f} \left[ \frac{\partial H}{\partial U} \right]$

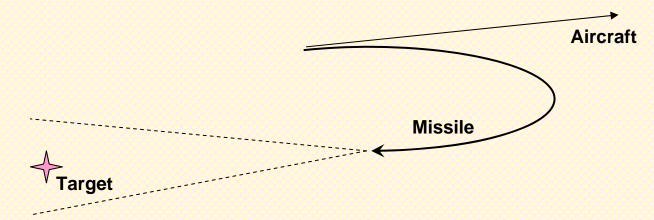
$$\int_{-\infty}^{T} \left[ \frac{\partial H}{\partial U} \right] dt = \frac{\alpha}{100} \left| \overline{J} \right|$$

This leads to

$$\tau = \frac{\frac{\alpha}{100} |\overline{J}|}{\int_{t_0}^{t_f} \left[\frac{\partial H}{\partial U}\right]^T \left[\frac{\partial H}{\partial U}\right] dt}$$

#### **Objective:**

Air-to-air missiles are usually launched from an aircraft in the forward direction. However, the missile should turn around and intercept a target "behind the aircraft".



To execute this task, the missile should turn around by -180° and lock onto its target (after that it can be guided by its own homing guidance logic). <u>Note:</u> Every other case can be considered as a subset of this extreme scenario!

#### **MATHEMATICAL PERSPECTIVE:**

- Minimum time optimization problem
- Fixed initial conditions and free final time problem

#### **SYSTEM DYNAMICS:**

Equations of motion for a missile in vertical plane. The non-dimensional equations of motion (point mass) in a vertical plane are:

 $M' = -S_w M^2 C_D - \sin(\gamma) + T_w \cos(\alpha)$  $\gamma' = \frac{1}{M} [S_w M^2 C_L + T_w \sin(\alpha) - \cos(\gamma)]$ 

where prime denotes differentiation with respect to the non-dimensional time  $\tau$ 

The non-dimensional parameters are defined as follows:

$$\tau = \frac{g}{at}; \quad T_w = \frac{T}{mg}; \quad S_w = \frac{\rho a^2 S}{2mg}; \quad M = \frac{V}{a}$$

where M = flight Mach number

- $\gamma$  = flight path angle T = thrust
- m = mass of the missile S = reference aerodynamic area
- V = speed of the missile  $C_L =$  lift coefficient
- $C_D$  = drag coefficient g = the acceleration due to gravity
- a = the local speed of sound  $\rho =$  the atmospheric density
- the atmospheric density
- t =flight time after launch

NOTE:  $C_L, C_D$  are usually functions of  $\alpha \& M$  (tabulated data)

#### **COST FUNCTION:**

Mathematically the problem is possed as follows to find the control minimizing cost function:

$$J = \int_{0}^{t_{f}} dt$$

Constraints  $\gamma(0) = 0^{\circ}$ , M(0) = initial Mach number  $\gamma(t_f) = -180^{\circ}$ ,  $M(t_f) = 0.8$ 

Choosing  $\gamma$  as the independent variable the equations are reformulated as follows:

$$\frac{dM}{d\gamma} = \frac{\left(-S_w M^2 C_D - \sin(\gamma) + T_w \cos(\alpha)\right) M}{S_w M^2 C_L - \cos(\gamma) + T_w \sin(\alpha)}$$
$$\frac{dt}{d\gamma} = \frac{aM}{g\left(S_w M^2 C_L - \cos(\gamma) + T_w \sin(\alpha)\right)}$$

and the transformed cost function is

$$J = \int_{0}^{t_{f}} dt = \int_{0}^{-\pi} \frac{dt}{d\gamma} d\gamma = \int_{0}^{-\pi} \frac{aM}{g\left(S_{w}M^{2}C_{L} - \cos(\gamma) + T_{w}\sin(\alpha)\right)} d\gamma$$

A difficult minimum-time problem has been converted to a relatively easier fixed final-time problem (with hard constraint:  $M(\gamma_f) = 0.8$ )!

# Task

Solve the problem using gradient method. Assume M(0) = 0.5 and engagement height as 5 km. Next, generate the trajectories and tabulate the values of  $M_f$  for various q values.

Use the following system parameters

(typical for an air-to-air missile):

$$m = 240 \ kg$$

$$S = 0.0707 m^2$$

T = 24,000 N

$$C_{D} = 0.5$$

 $C_L = 3.12$ 

Use standard atmosphere chart for the atmospheric data.

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# Necessary Conditions of Optimality (TPBVP): A Summary

State Equation

$$\dot{X} = \frac{\partial H}{\partial \lambda} = f(t, X, U)$$

Costate Equation

$$\dot{t} = -\left(\frac{\partial H}{\partial X}\right) = g(t, X, U, \lambda)$$

 Optimal Control Equation

$$\frac{\partial H}{\partial U} = 0$$

• Boundary Condition  $\lambda_f = \frac{\partial \varphi}{\partial X}$ 

$$- X(t_0) = X_0$$
: Fixed

• Form a Meta State Vector 
$$Z = \begin{bmatrix} X \\ \lambda \end{bmatrix}$$
. This implies  $dZ = \begin{bmatrix} dX \\ d\lambda \end{bmatrix}$ .

• Guess  $\lambda(t_0)$ . Note that  $X(t_0)$  is given. This leads to

$$\dot{Z} \equiv \begin{bmatrix} \dot{X} \\ \dot{\lambda} \end{bmatrix} = F(Z) \tag{1}$$

$$Z(t_0) = \begin{bmatrix} X(t_0) \\ \lambda(t_0) \end{bmatrix}$$

• Obtain the linearized Error Dynamics Equation

$$d\dot{Z} = \left[\frac{\partial F}{\partial Z}\right] dZ$$

ADVANCED CONTROL SYSTEM DESIGN Dr. Radhakant Padhi, AE Dept., IISc-Bangalore (2)

Define a State Transition Matrix (STM) Φ, such that at any two times t<sub>i</sub> and t<sub>j</sub>

$$dZ(t_j) = \Phi(t_j, t_i) \quad dZ(t_i) \tag{3}$$

• The dynamics and initial conditions for the STM can be shown to be

$$\dot{\Phi} = \left[\frac{\partial F}{\partial Z}\right] \Phi \tag{4}$$

$$\Phi(t_0, t_0) = I_{2n \times 2n}$$

 Numerically integrate the equations (2) and (4) from t<sub>0</sub> to t<sub>f</sub>; solving for the optimal control U at each instant of time.

• Finally, at  $t = t_f$ ,

$$dZ_f \equiv \begin{bmatrix} dX_f \\ d\lambda_f \end{bmatrix} = \Phi(t_f, t_0) \quad dZ_0 \tag{5}$$

• Thus, at  $t = t_0$ ,

$$dZ_0 \equiv \begin{bmatrix} dX_0 \\ d\lambda_0 \end{bmatrix} = \Phi^{-1}(t_f, t_0) \quad dZ_f \tag{6}$$

• Since  $X_0$  is fixed, force  $dX_0 = 0$ . Update only  $\lambda_0$ . Repeat until convergence.

• Computational Load Reduction

Partition the STM ( $\Phi$ ) as  $\Phi = \begin{bmatrix} \Phi_1 & \vdots & \Phi_2 \end{bmatrix}$ . Then,

$$dZ_f = \Phi_{1f} \, dX_0 + \Phi_{2f} \, d\lambda_0 = \Phi_{2f} \, d\lambda_0 \tag{7}$$

• For convenience, let  $h = (\lambda_f)_{n \times 1}$  be the vector of n boundary conditions at  $t_f$ . Then,

$$\left(\frac{\partial h}{\partial Z}\right)_f dZ_f = dh = \left(\lambda_f - \lambda_f^*\right)_{n \times 1}$$
(8)

Where,  $\lambda_f^*$  is the true (desired) value of  $\lambda_f$ .

- Finally, at  $t = t_f$ ,  $d\lambda_0 = \left[ \left( \frac{\partial h}{\partial Z} \right)_f \Phi_{2f} \right]^{-1} dh$ (9)
- Hence, obtain dλ<sub>0</sub>(k) and update λ<sub>0</sub>(k) to λ<sub>0</sub>(k + 1). Repeat until convergence.

# Quasi-Linearization Method

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# **Quasi-Linearization Method**

#### **Problem:**

Differential Equation:  $\dot{Z} = F(Z, t), \qquad Z \triangleq \begin{bmatrix} X^T & \lambda^T \end{bmatrix}^T$ Boundary condition:  $\langle C(t_i), Z(t_i) \rangle = C_i^T Z_i = b_i$  $t_i \in t, \quad i \in \{1, \dots, n\}$ 

#### **Assumption:**

This vector differential equation has a unique solution over  $t \in [t_0, t_f]$ 

#### Trick:

The nonlinear multi-point boundary value problem is transformed into a sequence of linear non-stationary boundary value problems, the solution of which is made to approximate the solution of the true problem.

# **Quasi-Linearization Method**

(1) Guess an approximate solution  $Z^{N}(t)$  (N=1) (it need not satisfy the B.C.)

For updating this solution, proceed with the following steps:

(2) Linearize the system dynamics about  $Z^{N}(t)$  $\Delta \dot{Z}^{N} = \left[\frac{\partial F}{\partial Z}\right]_{Z^{N}} \Delta Z^{N}, \quad \text{where, } \Delta Z^{N}(t) \triangleq \underbrace{Z^{N+1}(t)}_{\text{To be found}} - Z^{N}(t)$   $\Delta \dot{Z}^{N} = A(t) \Delta Z^{N}$ 

(3) Enforce the boundary with respect to the updated solution  $Z^{N+1}(t)$   $\langle C(t_i), Z^{N+1}(t_i) \rangle = \langle C(t_i), Z^N(t_i) + \Delta Z^N(t_i) \rangle = b_i$  $\langle C(t_i), \Delta Z^N(t_i) \rangle = -\langle C(t_i), Z^N(t_i) \rangle + b_i$ Philosophy: Solve this linear system and update the solution!

# **Quasi-Linearization Method: Solution by STM Approach**

(1) From the linearized system dynamics, we can write

 $\dot{Z}^{N+1} = \dot{Z}^{N} + A(t) \left( Z^{N+1} - Z^{N} \right)$  $= \underbrace{A(t) Z^{N+1}}_{\text{Homogeneous}} + \underbrace{\left[ F(Z^{N}, t) - A(t) Z^{N} \right]}_{\text{Forcing function}}$ 

(2) The solution  $Z^{N+1}(t)$  to the above equation is given by

$$Z^{N+1}(t) = \underbrace{\Phi^{N+1}(t, t_0)}_{\text{State transition matrix (STM)}} Z^{N+1}(t_0) + \underbrace{p^{N+1}(t)}_{\text{Particular solution}}$$

(3) The solution for STM  $\Phi^{N+1}(t, t_0)$  can be obtained from the fact that it satisfies the following differential equation and boundary conditions  $\frac{\partial}{\partial t} \left[ \Phi^{N+1}(t, t_0) \right] = A(t) \Phi^{N+1}(t, t_0)$  $\Phi^{N+1}(t_0, t_0) = I$ 

# **Quasi-Linearization Method: Solution by STM Approach**

(4) The particular solution  $p^{N+1}(t)$  can be obtained by observing that it satisfies the the following differential equation and boundary condition

Substituting the complete solution  $Z^{N+1}(t)$  in the original equation

 $\frac{\partial}{\partial t} \Big[ \Phi^{N+1}(t,t_0) Z^{N+1}(t_0) \Big] + \dot{p}^{N+1}(t) = A(t) \Big[ \Phi^{N+1}(t,t_0) Z^{N+1}(t_0) + p^{N+1}(t) \Big] \\ + \Big[ F(Z^N,t) - A(t) Z^N \Big] \\ \dot{p}^{N+1}(t) = A(t) p^{N+1}(t) + \Big[ F(Z^N,t) - A(t) Z^N \Big]$ 

(5) The boundary condition  $p^{N+1}(t_0)$  can be obtained by observing that  $Z^{N+1}(t_0) = \underbrace{\Phi^{N+1}(t_0, t_0)}_{I} Z^{N+1}(t_0) + p^{N+1}(t_0)$   $p^{N+1}(t_0) = 0$ 

# **Quasi-Linearization Method: Solution by STM Approach**

(6) The boundary condition  $Z^{N+1}(t_0)$  can be obtained as follows  $\langle C(t_i), Z^{N+1}(t_i) \rangle = b_i$   $\langle C(t_i), \Phi^{N+1}(t_i, t_0) Z^{N+1}(t_0) + p^{N+1}(t_i) \rangle = b_i$  $\langle C(t_i), \Phi^{N+1}(t_i, t_0) Z^{N+1}(t_0) \rangle = -\langle C(t_i), p^{N+1}(t_i) \rangle + b_i$ 

Solve the above system to obtain  $Z^{N+1}(t_0)$ 

Once  $Z^{N+1}(t_0)$  is determined, the solution  $Z^{N+1}(t)$  is available from the STM solution:  $Z^{N+1}(t) = \underbrace{\Phi^{N+1}(t, t_0)}_{\text{STM}} Z^{N+1}(t_0) + \underbrace{p^{N+1}(t)}_{\text{Particular solution}}$ 

# **Quasi-Linearization Method: Convergence Property**

Under the assumption that the problem admits a unique solution for  $t \in [t_0, t_f]$ it can be shown that the sequence of vectors  $\{Z^{N+1}(t)\}$  converge to the true solution.

Morover, the process can be shown to have "quadratic convergence" in general i.e., it can be shown that  $\|Z^{N+1}(t) - Z^N(t)\| \le k \|Z^N(t) - Z^{N-1}(t)\|$ , where  $k \ne f(N)$ .

Further more, for a large class of systems, it can be shown to have "monotone convergence" as well, i.e. there won't be any over-shooting in the convergence process.

Reference : R. Kabala, "On Nonlinear Differential Equations, The Maximum Operation and Monotone Convergence", J. of Mathematics and Mechanics, Vol. 8, 1959, pp. 519-574.

### **A Demonstrative Example**

**Problem:** Minimize  $J = \frac{1}{2} \int_{0}^{1} (x^2 + u^2) dt$  for the system  $\dot{x} = -x^2 + u$ , x(0) = 10. Solution: Hamiltonian:  $H = \frac{1}{2}(x^2 + u^2) + \lambda(-x^2 + u)$  $\dot{x} = -x^2 + u$ 1) State Equation: 2) Optimal Control Equation:  $u + \lambda = 0 \implies u = -\lambda$ 3) Costate Equation:  $\dot{\lambda} = -(\partial H / \partial x) = -x + 2\lambda x$ 4) Bounary Conditions:  $x(0) = 10, \lambda(1) = (\partial \Phi / \partial x) = 0$ Substituting the expression for u in the state equation, we can write  $\dot{x} = -x^2 - \lambda, \qquad x(0) = 10$  $\dot{\lambda} = -x + 2\lambda x, \qquad \lambda(1) = 0$ 

Task : Solve this problem using shooting and quasi-linearization methods.

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- D. E. Kirk, Optimal Control Theory: An Introduction, Prentice Hall, 1970.
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 H. J. Pesch (1994), "A Practical Guide to the Solution of Real-Life Optimal Control Problems", Control and Cybernetics, Vol.23, No.1/2, 1994, pp.7-60.

