
Chemical Reaction Engineering

Lecture 2: Review of Undergraduate Material

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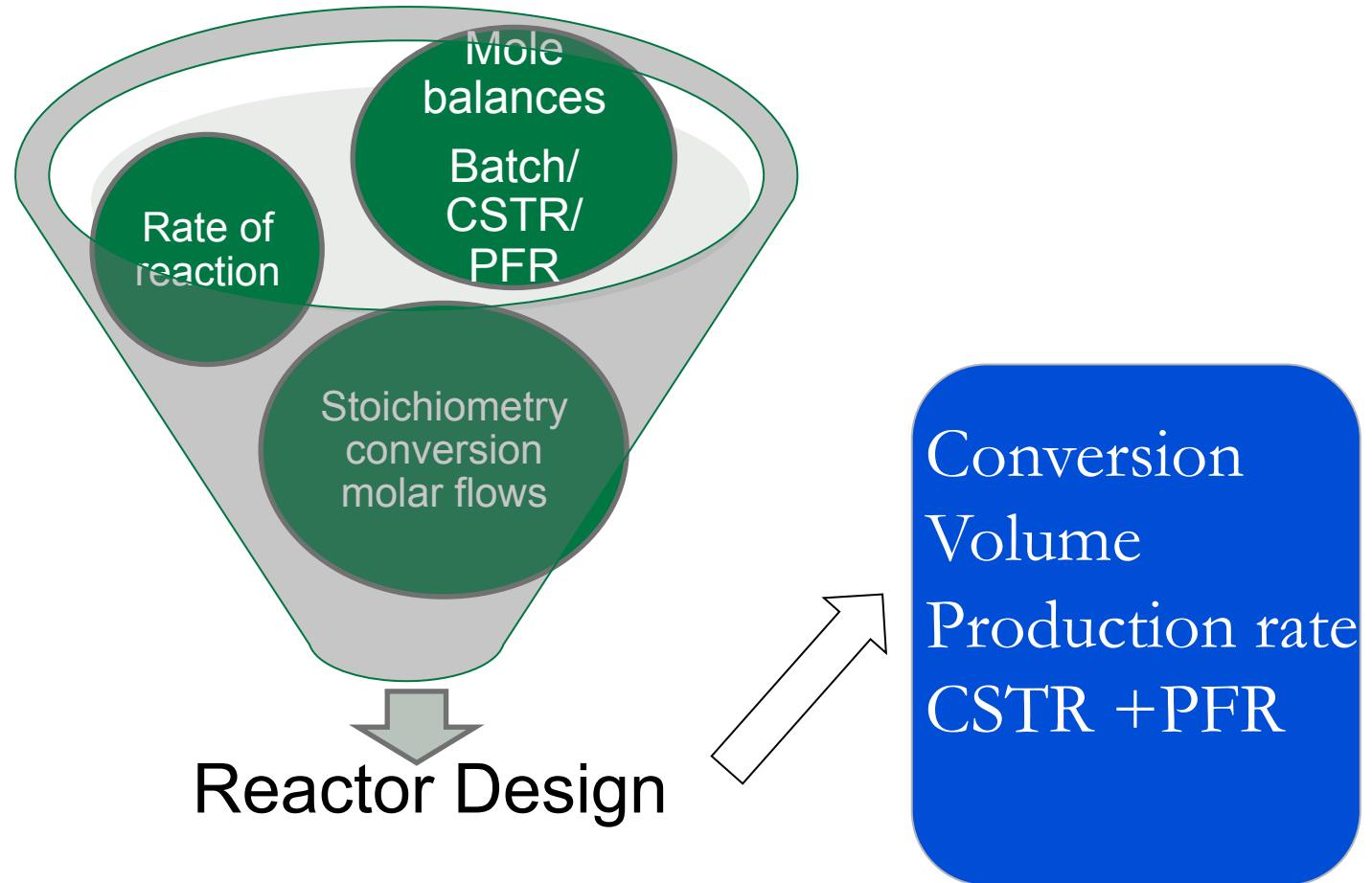
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Ethylene production by thermal cracking of ethane

- The thermal cracking of ethane is carried out in multitubular reactor. Typical production capacity of each tube is 10000 Tons per annum.
- Reactor specifications:
 - ❑ Feed to the reactor: ethane + steam (?)
 - ❑ Inlet pressure - 2.99 atm; temperature - 680°C
 - ❑ Tube length 95 m, ethylene conversion – 60%



Cracking of ethane to ethylene



Topic 1: Basic concepts

- Representation of reaction
- Extent of reaction and conversion
- Thermodynamics and chemical reactions
 - ❑ Heat of reaction
 - ❑ Condition of equilibrium



Representation of chemical reaction – single reaction

- Consider a single chemical reaction in N species

A_1, A_2, \dots, A_N

- General representation:

$$\sum_{j=1}^N \nu_j A_j = 0$$



Representation of chemical reaction – multiple reactions

- Consider R chemical reactions in N species A_1, A_2, \dots, A_N
- General representation:

$$\sum_{j=1}^N \nu_{ij} A_j = 0, \quad i = 1, 2, \dots, R$$



Representation of chemical reaction – independent reactions

➤ Stoichiometric matrix

$$\underline{v} = \begin{pmatrix} v_{11} & \cdots & v_{1N} \\ \vdots & \ddots & \vdots \\ v_{R1} & \cdots & v_{RN} \end{pmatrix}$$

➤ Number of independent reaction

$$R = \text{rank} \left[\underline{v} \right]$$



Progress of chemical reaction – single reaction

- Consider a reaction $\sum v_j A_j = 0$ taking place in a **closed system**

n_{j0} = number of moles of species j present initially

n_j = number of moles of species j at any time t

- Molar extent of reaction - α

$$\alpha = \frac{n_j - n_{j0}}{v_j}$$



Molar extent of reaction

$$\alpha = \frac{n_j - n_{j0}}{\nu_j}$$

► Properties of α

- defined for the reaction

$$\alpha = \frac{n_j - n_{j0}}{\nu_j} = \frac{n_k - n_{k0}}{\nu_k}$$

$$\Rightarrow n_k = n_{k0} + \frac{\nu_k}{\nu_j} (n_j - n_{j0})$$

- Extensive property in moles
- Always positive



Conversion of species

➤ Conversion X

$$X = \frac{n_{j0} - n_j}{n_{j0}}$$

➤ Stoichiometrically limiting species “k”

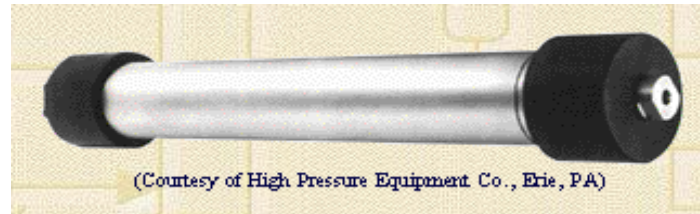
$$\min \left(-\frac{n_{j0}}{\nu_j} \right)$$



Cracking of ethane to ethylene

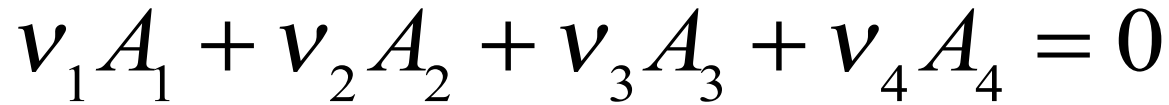


Molar flow at
entry
Ethane, F_{10}



Molar flow at
exit
Ethane, F_1
Ethylene, $F_2 \dots$

Stoichiometric tables – Flow reactor



Species	Entry (mol/ min)	Change (mol/ min)	Exit from the reactor (mol/min)
A ₁	F ₁₀	-(F ₁₀ X)	F ₁ = F ₁₀ - F ₁₀ X
A _j j=2,3, 4	F _{j0}	- ν _j /ν ₁ (F ₁₀ X)	F _j = F _{j0} - ν _j /ν ₁ F ₁₀ X
I (inerts)	F _{I0}	-----	F _I = F _{I0}
Total	F _{T0}		F _T = F _{T0} - (Σν _j /ν ₁)F ₁₀ X F _T = F _{T0} + δF ₁₀ X



Concentrations in terms of conversion

$$\left. \begin{aligned} P v &= Z F_T R T \\ P_0 v_0 &= Z_0 F_{T0} R T_0 \end{aligned} \right\} v = v_0 \left(\frac{P_0}{P} \right) \left(\frac{Z}{Z_0} \right) \left(\frac{T}{T_0} \right) \left(\frac{F_T}{F_{T0}} \right)$$

$$F_T = F_{T0} + \delta F_{10} X$$

$$\frac{F_T}{F_{T0}} = 1 + \delta \frac{F_{10}}{F_{T0}} X = 1 + \delta y_{10} X = 1 + \varepsilon X$$

$$v = v_0 \left(\frac{P_0}{P} \right) \left(\frac{Z}{Z_0} \right) \left(\frac{T}{T_0} \right) (1 + \varepsilon X)$$

Concentrations in terms of conversion

$$C_{A0} = \frac{F_{A0}}{v_0}$$

$$C_A = \frac{F_A}{v} = \frac{F_{A0} - F_{A0}X}{v}$$

$$C_A = C_{A0} \left(\frac{1-X}{1+\varepsilon X} \right) \left(\frac{P}{P_0} \right) \left(\frac{Z_0}{Z} \right) \left(\frac{T_0}{T} \right)$$

$$C_B = C_{A0} \left(\frac{\Theta_B - b/aX}{1+\varepsilon X} \right) \left(\frac{P}{P_0} \right) \left(\frac{Z_0}{Z} \right) \left(\frac{T_0}{T} \right)$$

Summary – Stoichiometry of reaction

- Keywords & concepts
 - ❑ Stoichiometric coefficients
 - ❑ Multiple reactions
 - ❑ Set of independent reactions
 - ❑ Extent of reaction
 - ❑ Conversion
 - ❑ Stoichiometric tables



Chemical Reaction Engineering

Lecture 3: Review of Undergraduate Material

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Ethylene production by thermal cracking of ethane

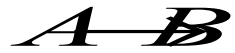
- The thermal cracking of ethane is carried out in multitubular reactor. Typical production capacity of each tube is 10000 Tons per annum.
- Reactor specifications:
 - ❑ Feed to the reactor: ethane + steam (?)
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 - ❑ Tube length 95 m, ethylene conversion – 60%



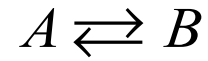
Thermodynamic considerations

- Equilibrium conversion
- Working conditions of the reactor
- Heat effects in a chemical reaction

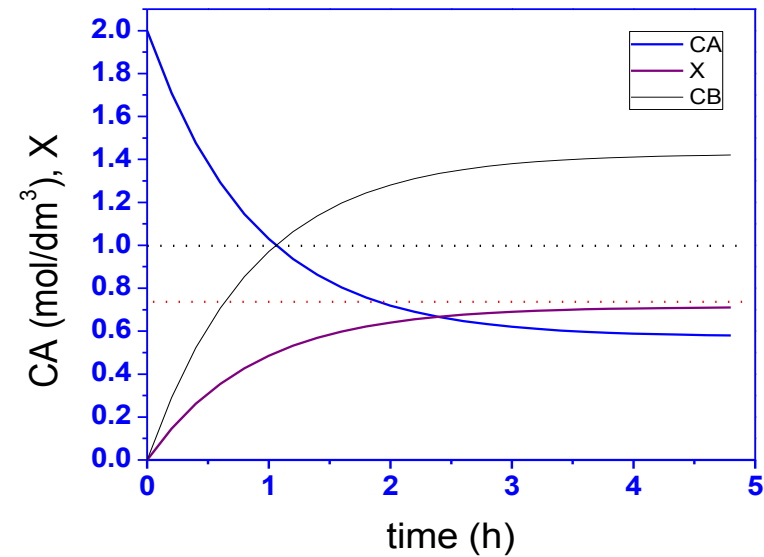
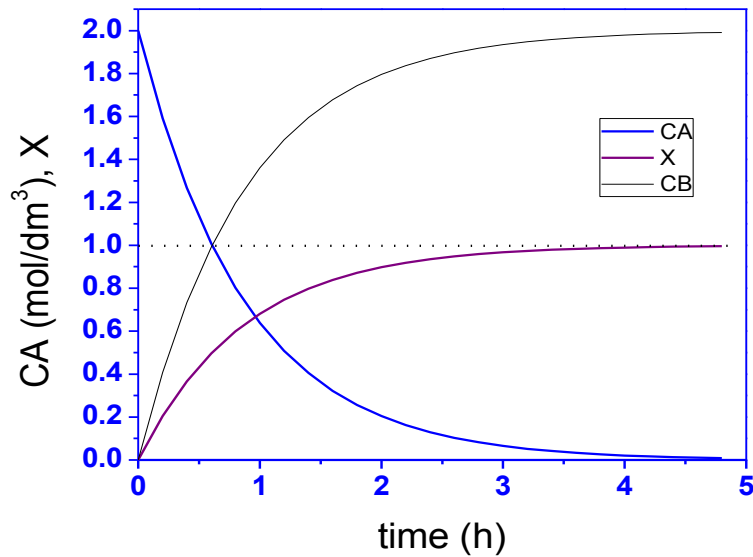
Why thermodynamics



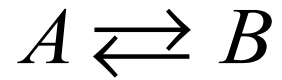
$$r = 2.6 \times 10^6 e^{-\left(\frac{15000}{T}\right)} C_A$$



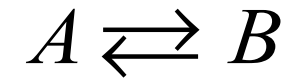
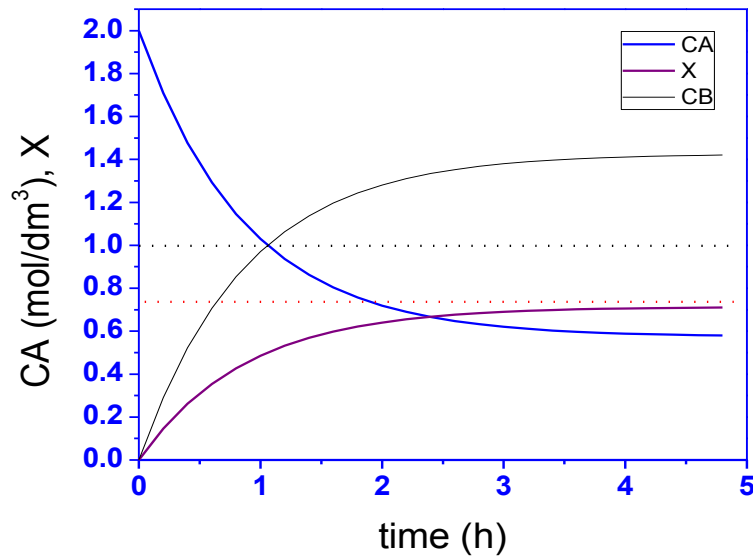
$$r = 2.6 \times 10^6 e^{-\left(\frac{15000}{T}\right)} C_A - 3.9 \times 10^{33} e^{-\left(\frac{25000}{T}\right)} C_B$$



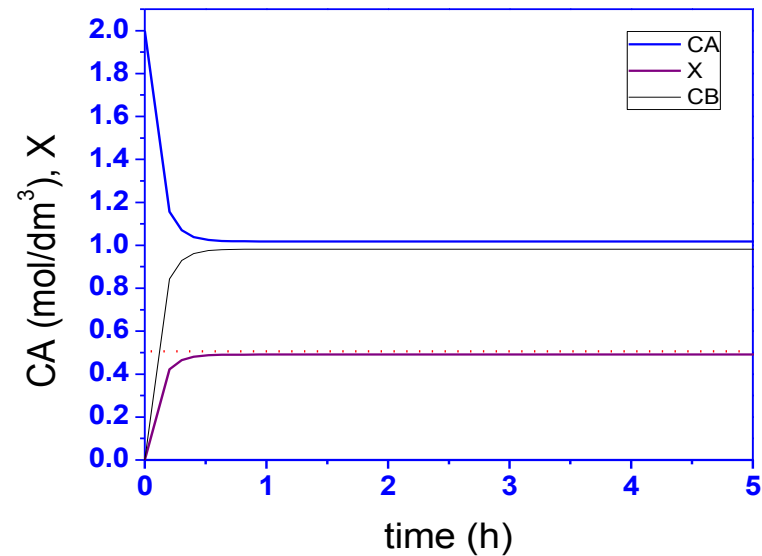
Effect of temperature



$$T = 320$$



$$T = 330$$



Chemical Equilibrium

- Consider a reaction $\sum v_j A_j = 0$ taking place at constant temperature T and pressure P . The system will spontaneously change in the direction of increasing entropy, reaching equilibrium when entropy can not increase further.
- Free energy and Gibb' s equations

$$dG = Vdp - SdT + \sum_{j=1}^N \mu_j dn_j,$$

$$\text{Chemical Potential } \mu_j = \left(\frac{\partial G}{\partial n_j} \right)_{T, P, n_k}$$



Chemical Equilibrium

$$\text{Gibb's Equation} \quad dG = Vdp - SdT + \sum_{j=1}^N \mu_j dn_j$$

$$\text{Progress of reaction} \quad n_j = n_{j0} + \nu_j \alpha \quad \text{or} \quad dn_j = \nu_j d\alpha$$

$$\Rightarrow dG = Vdp - SdT + \sum_{j=1}^N \nu_j \mu_j d\alpha$$

➤ **Equilibrium condition**

$$\left(\frac{\partial G}{\partial \alpha} \right)_{T,P} = \sum_{j=1}^N \nu_j \mu_j = 0$$



Chemical potential

➤ Perfect gas mixture

$$\mu_j(T, P, \underline{y}) = \mu_{j0}(T, P^r, \underline{y}^r) + RT \ln \frac{Py_j}{P^r}$$

\underline{y} = composition ,

T = temperature,

P = pressure

superscript r = reference

$P^r = 1 \text{ atm}$

➤ Non-ideal gas mixture

$$\mu_j(T, P, \underline{y}) = \mu_{j0}(T, P^r, \underline{y}^r) + RT \ln \frac{f_j}{f_j^r}$$

\underline{y}^r = pure j

f_j = fugacity



Chemical potential

➤ Solution

$$\mu_j(T, P, \underline{x}) = \mu_{j0}(T, P^r, \underline{x}^r) + RT \ln \gamma_j x_j$$

\underline{x} = composition ,

T = temperature,

P = pressure

superscript r = reference

γ = activity coefficient



Free energy change

$$\nu_1 A_1 + \nu_2 A_2 + \nu_3 A_3 + \nu_4 A_4 = 0$$

$$\mu_j = \mu_{j0} + RT \ln(a_j)$$

$$\sum_{j=1}^N \nu_j \mu_j = \sum_j \nu_j \mu_{j0} + RT \sum_j \nu_j \ln(a_j)$$

$$\Delta G = \Delta G^0 + RT \ln \left(\prod_j a_j^{\nu_j} \right)$$

$$\Delta G = \Delta G^0 + RT \ln K_a$$



Equilibrium condition

$$\nu_1 A_1 + \nu_2 A_2 + \nu_3 A_3 + \nu_4 A_4 = 0$$

$$\Delta G = \Delta G^0 + RT \ln \left(\prod_j a_j^{\nu_j} \right) = 0$$

$$\Delta G = \Delta G^0 + RT \ln K_a = 0$$

$$K_a = \left(\prod_j a_j^{\nu_j} \right) = \exp \left(\frac{-\Delta G^0}{RT} \right)$$

Equilibrium constant

$$\nu_1 A_1 + \nu_2 A_2 + \nu_3 A_3 + \nu_4 A_4 = 0$$

$$K_a = \left(\prod_j a_j^{\nu_j} \right) = \exp\left(\frac{-\Delta G^0}{RT} \right)$$

Pressure
$$K_P = \left(\prod_i P_j^{\nu_j} \right) = \left(\prod_i (P y_j)^{\nu_j} \right)$$

Fugacity
$$K_f = \left(\prod_i f_j^{\nu_j} \right)$$

Concentration
$$K_C = \left(\prod_i C_j^{\nu_j} \right)$$



Equilibrium extent of reaction

$$\nu_1 A_1 + \nu_2 A_2 + \nu_3 A_3 + \nu_4 A_4 = 0$$

$$K_P = \left(\prod_j P_j^{\nu_j} \right) \quad P_j = y_j P = \frac{N_j}{N_T} P$$

$$N_j = N_{j0} + \nu_j \alpha$$

$$K_P = \left(\prod_j \left[P \frac{N_{j0} + \nu_j \alpha}{N_{T0} + \alpha \sum_j \nu_j} \right]^{\nu_j} \right) = F(\alpha)$$

Extent of reaction and operating conditions

$$\nu_1 A_1 + \nu_2 A_2 + \nu_3 A_3 + \nu_4 A_4 = 0$$

$$K_P(T) = \left(\prod_j \left[P \frac{N_{j0} + \nu_j \alpha}{N_{T0} + \alpha \sum_j \nu_j} \right]^{\nu_j} \right) = F(\alpha, P, N_{j0})$$

$$\frac{d}{dY} [\ln K_P(T)] = \frac{d}{dY} [F(\alpha, P, N_{j0})] = \frac{\partial F}{\partial Y} + \frac{\partial F}{\partial \alpha} \frac{d\alpha}{dY}$$



Extent of reaction and operating conditions

$$v_1 A_1 + v_2 A_2 + v_3 A_3 + v_4 A_4 = 0$$

$$\frac{d\alpha}{dY} = C \frac{F(\alpha)}{F'(\alpha)}$$

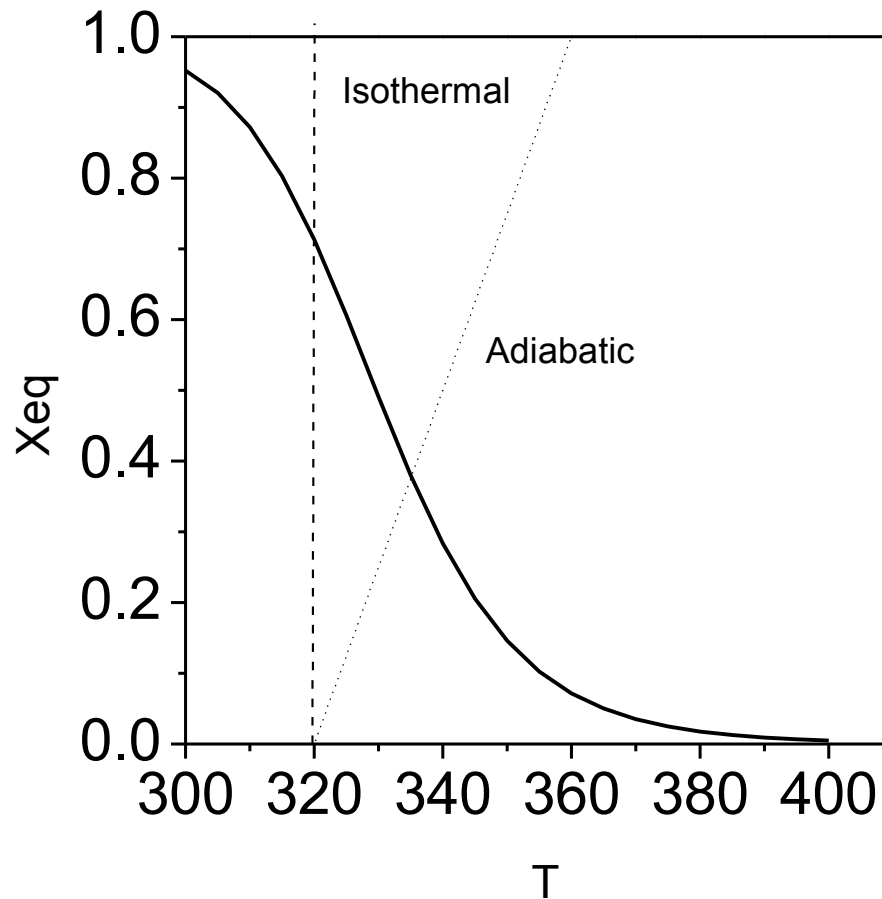
Temperature $C = \frac{\Delta H}{RT^2}$ $\Delta H = \text{heat of reaction}$

Pressure $C = -\frac{\sum_j v_j}{P}$ $\sum_j v_j = \text{change in no. of moles}$

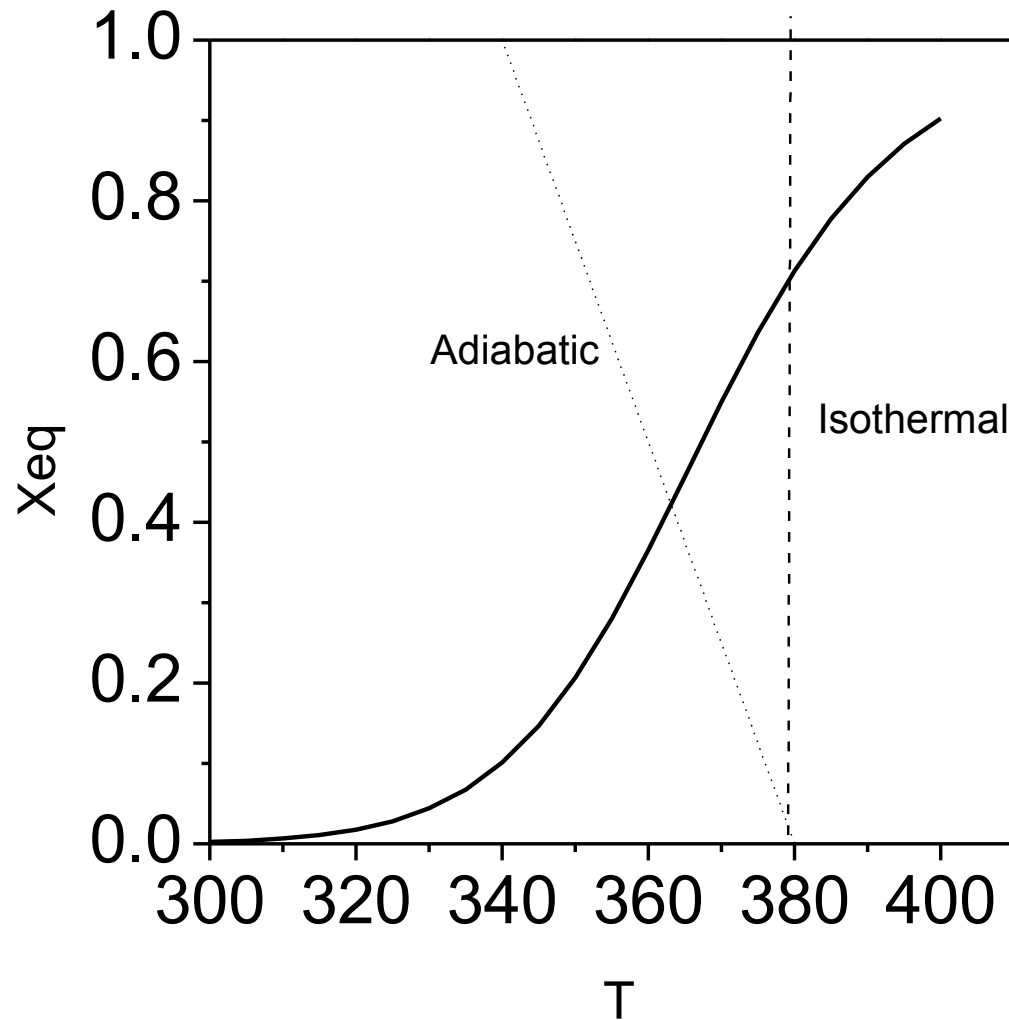
Inerts $C = ?$



Equilibrium conversion - Exothermic reaction



Equilibrium conversion - Endothermic reaction



Equilibrium extent of reaction

$$\sum_{j=1}^N \nu_{ij} A_j = 0, \quad i = 1, 2, \dots, R$$

$$K_{Pi} = \left(\prod_j P_j^{\nu_{ij}} \right)$$

$$N_j = N_{j0} + \sum_{i=1}^R \nu_{ij} \alpha_i$$

Heat of reaction

$$\nu_1 A_1 + \nu_2 A_2 + \nu_3 A_3 + \nu_4 A_4 = 0$$

$$\Delta H_R = \sum_j \nu_j h_j$$

$$h_j(T) = h_j^0 + \int_{298}^T C_{Pj} dT$$

$$\Delta H_R = \sum_j \nu_j h_j^0 + \sum_j \nu_j \int_{298}^T C_{Pj} dT$$

$$\Delta H_R = \Delta H_R^0 + \sum_j \nu_j \int_{298}^T C_{Pj} dT$$



Summary

- Free energy
- Chemical potential
- Condition of Equilibrium
- Equilibrium constant
- Equilibrium extent of reaction
- Operating conditions



Chemical Reaction Engineering

Lecture 4: Review of Undergraduate Material

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Chemical Kinetics: Basic concepts

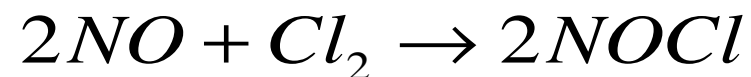
- Kinetics of irreversible and reversible reactions
 - ❑ Power law kinetics
 - ❑ Law of mass action kinetics
- Rate of simple reactions



Classification of reactions

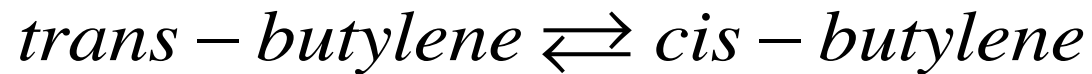
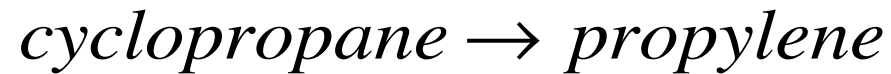
- Based on mechanism of the reaction
 - ❑ Elementary and nonelementary reactions

Example: chlorination of nitric oxide to give nitrosyl chloride



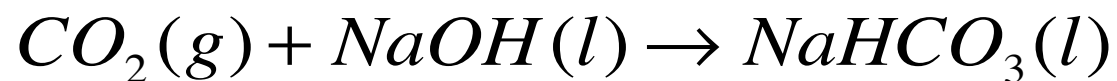
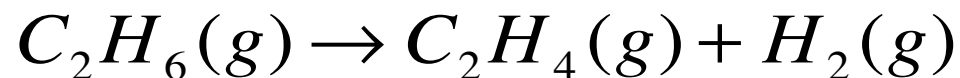
Classification of reactions

- Based on the direction of the reaction
 - ❑ Irreversible and reversible reactions



Classification of reactions

- Based on number of phases present in the system
 - ▣ Homogenous and heterogeneous reactions



Rate of chemical reaction – single reaction

- Consider a reaction $\sum v_j A_j = 0$ taking place in a **closed, isothermal, constant pressure system**
- Rate of reaction - r

$$r = \frac{1}{V} \frac{d\alpha}{dt} \quad \alpha = \frac{n_j - n_{j0}}{\nu_j}$$

$$r_j = \frac{1}{V} \frac{dn_j}{dt}$$



Reaction rate

- Consider a reaction $\sum v_j A_j = 0$ taking place in a **closed, isothermal, constant pressure system**

$$\begin{aligned} r &= r(T, P, y_1, y_2 \dots y_{N-1}) \\ &= r(T, P, C_1, C_2 \dots C_{N-1}) \\ &= r(T, C_1, C_2 \dots C_{N-1}, C_N) \end{aligned}$$



Reaction rate – power law kinetics

- Consider a reaction $\sum v_j A_j = 0$ taking place in a **closed, isothermal, constant pressure system**

$$r = k C_1^{q_1} C_2^{q_2} \dots C_N^{q_N} = k \prod_{j=1}^N C_j^{q_j}$$

q_j is the order of the reaction wrt species A_j

$q = \sum q_j$ is the overall order



Reaction rate – law of mass action kinetics

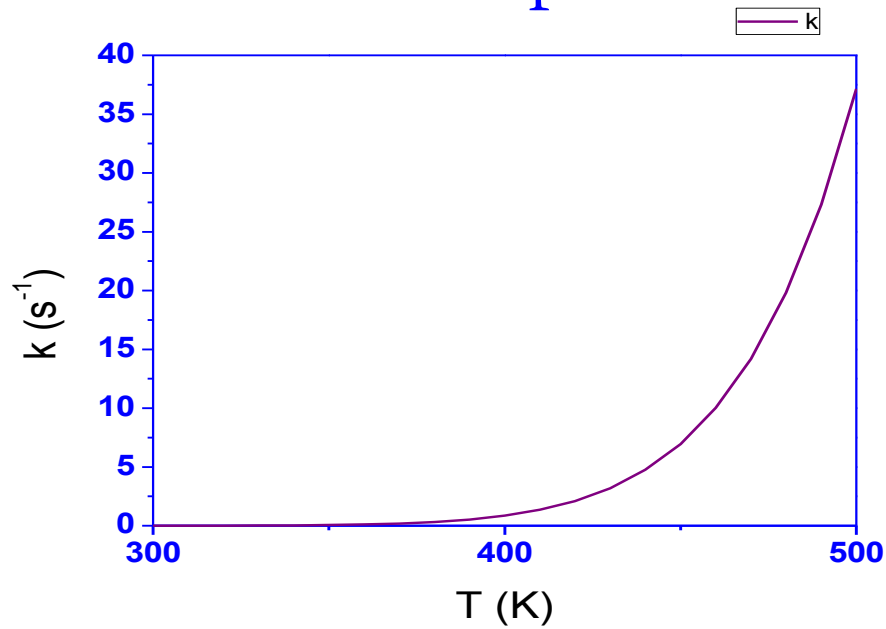
- Consider a reaction $\sum v_j A_j = 0$ taking place in a **closed, isothermal, constant pressure system**

$$r = k \prod_{j=1}^N C_j^{q_j}$$

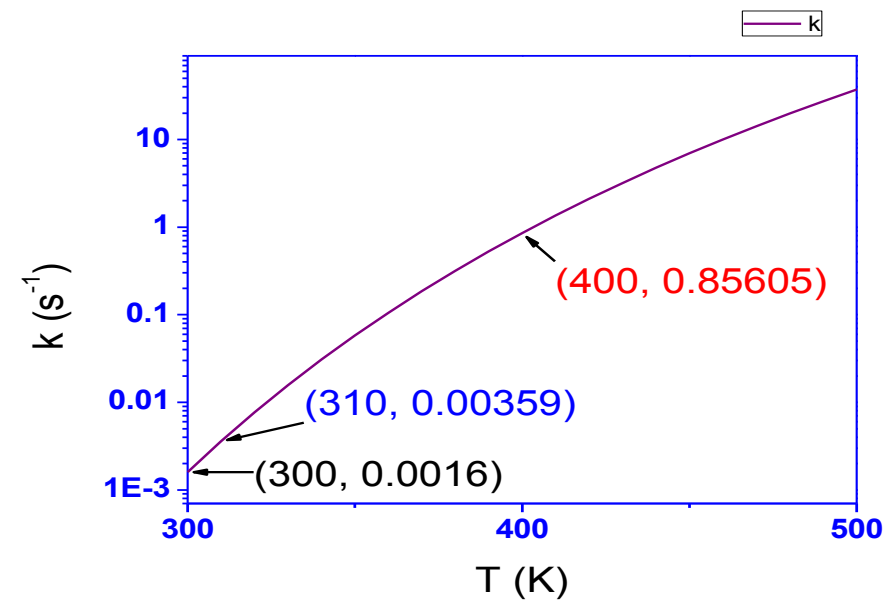
$$q_j = \frac{1}{2} (|\nu_j| - \nu_j)$$



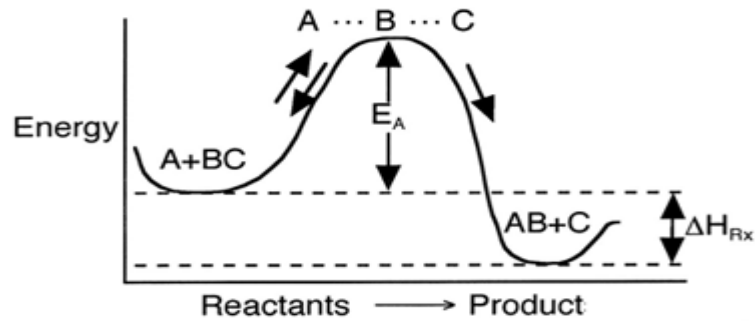
Effect of temperature on rate



$$k = A e^{-\left(\frac{E}{RT}\right)}$$

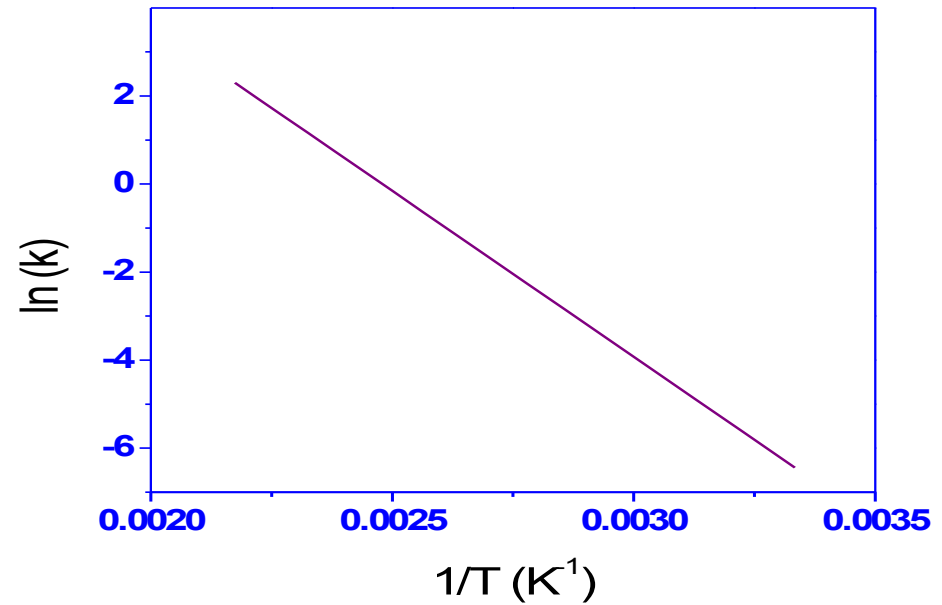


Activation energy



$$k = Ae^{-\left(\frac{E}{RT}\right)}$$

$$\ln k = \ln A - \frac{E}{RT}$$



Reaction rate – reversible reaction

- Consider a reaction $\sum v_j A_j = 0$ taking place in a closed, isothermal, constant pressure system

$$r = k_f \prod_{j=1}^N C_j^{q_j} - k_b \prod_{j=1}^N C_j^{q'_j}$$

$$q_j = \frac{1}{2} (|\nu_j| - \nu_j)$$

$$q'_j = \frac{1}{2} (|\nu_j| + \nu_j)$$



Variation of reaction rate with progress of reaction

- Consider a reaction $\sum v_j A_j = 0$ taking place in a **closed, isothermal, constant pressure system**

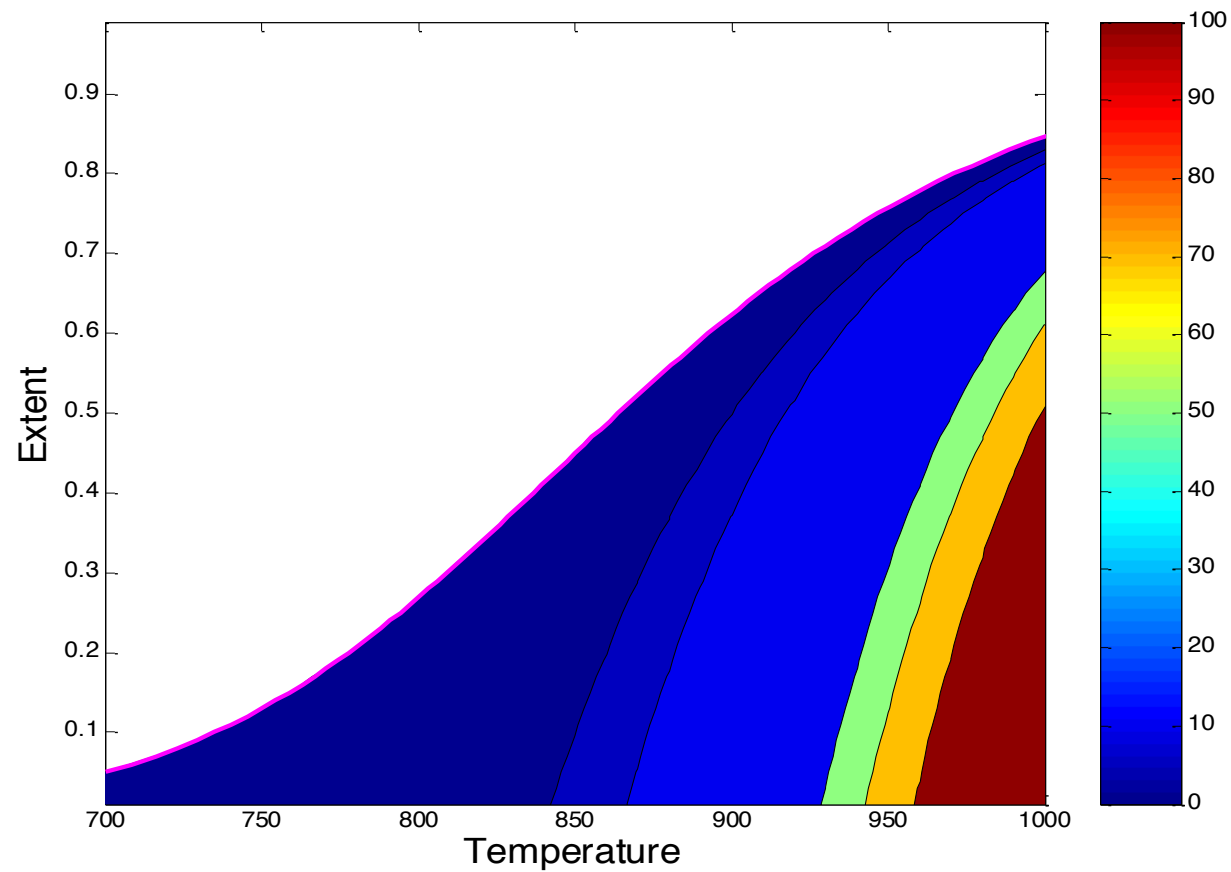
$$r = r_f - r_b = k_f(T) \prod_{j=1}^N C_j^{q_j} - k_b(T) \prod_{j=1}^N C_j^{q'_j}$$

$$C_j = C_{j0} + \alpha v_j$$

$$r(\alpha, T) = r_f(\alpha, T) - r_b(\alpha, T)$$

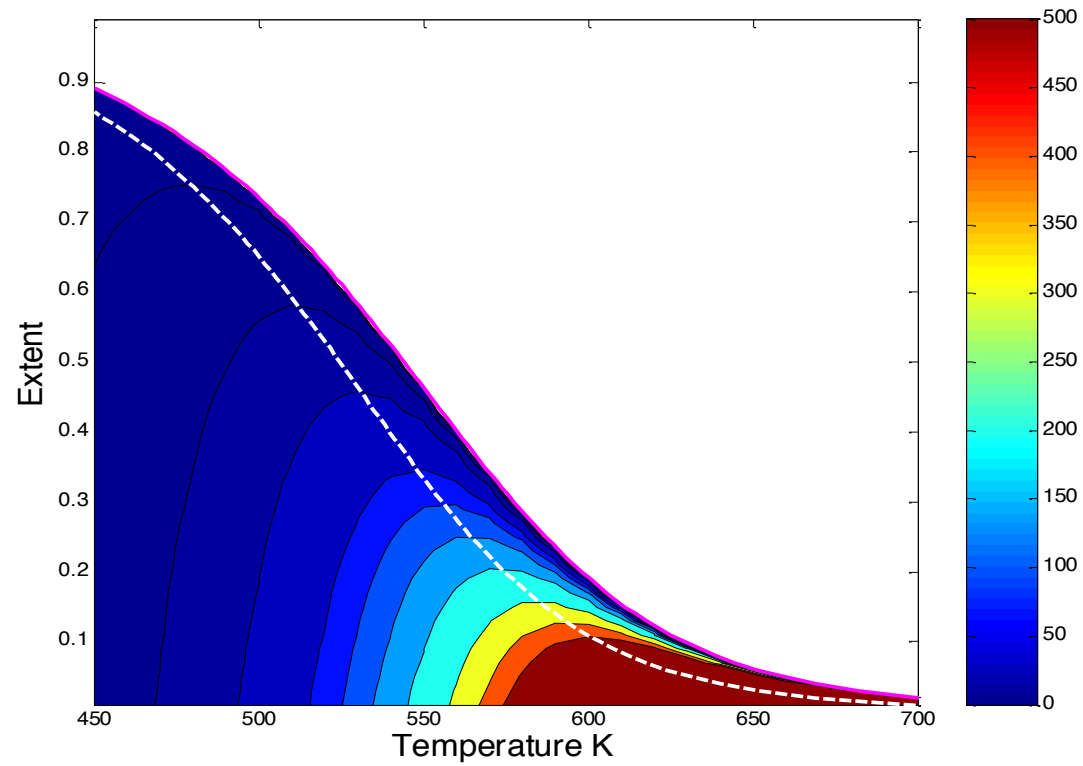


Rate contours – endothermic reaction



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Rate contours – exothermic reaction



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Summary

- Rate of reaction
- Power law kinetics
- Law of mass action kinetics
- Exothermic and endothermic reactions

