

Stochastic Structural Dynamics

Lecture-16

Random vibration analysis of MDOF systems-4

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VIBRATION ANALYSIS OF CONTINUOUS SYSTEMS

$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \varepsilon(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = f(x, t)$$

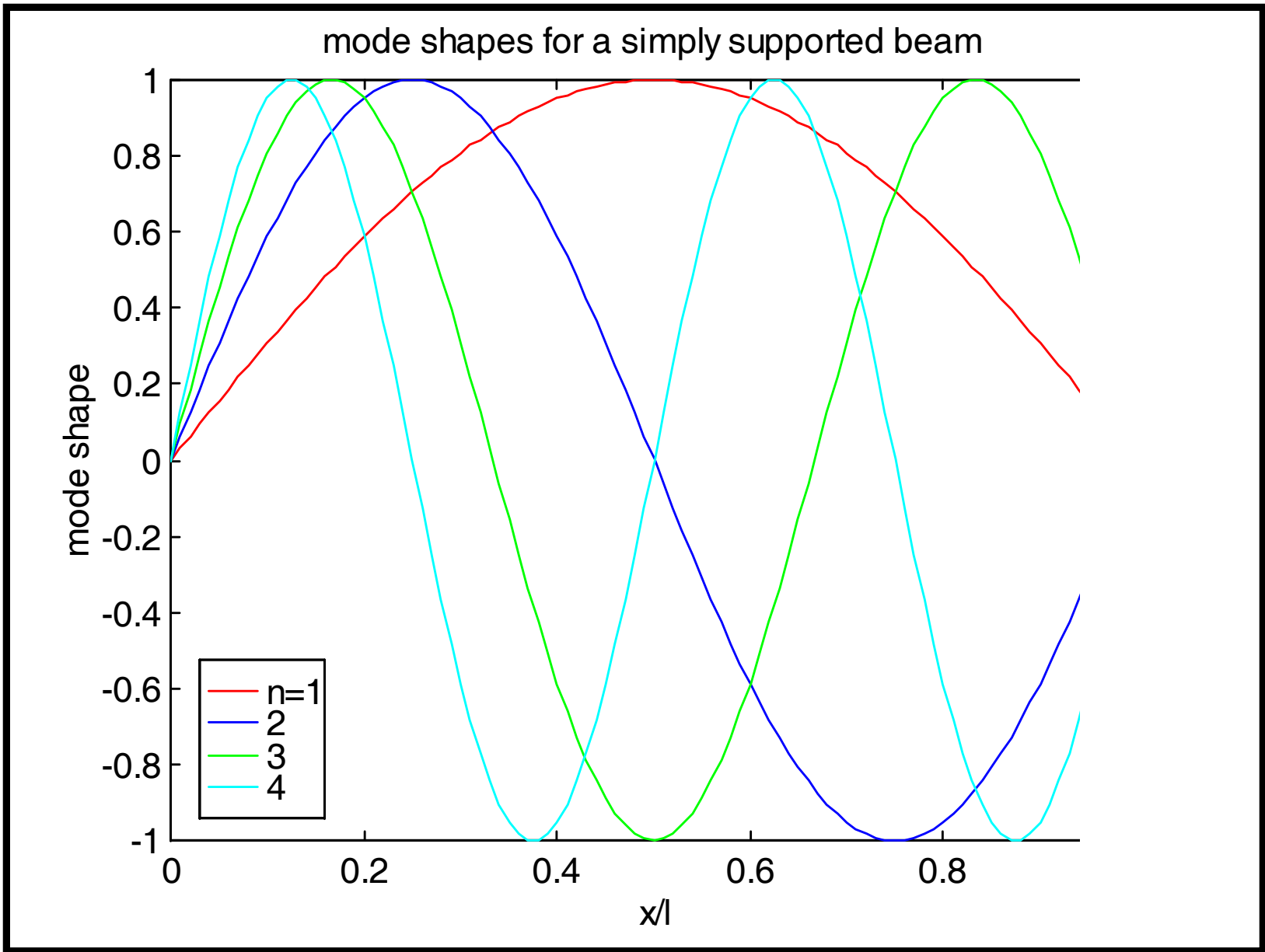
ICS: $y_0(x) = y(x, 0)$ $\dot{y}_0(x) = \dot{y}(x, 0)$ & BCS as appropriate.

$$\varepsilon(x) = \nu EI(x)$$

$$y(x, t) = \sum_{n=1}^{\infty} a_n(t) \varphi_n(x)$$

$$\left[EI \varphi_n'' \right]'' = m \omega_n^2 \varphi_n(x)$$

$$\int_0^L EI \varphi_n'' \varphi_k'' dx = 0 \quad n \neq k \quad \int_0^L m \varphi_n \varphi_k dx = 0 \quad n \neq k$$



$$\ddot{a}_n + 2\eta_n \omega_n \dot{a}_n + \omega_n^2 a_n = p_n(t);$$

$$2\eta_n \omega_n = (\alpha + \nu \omega_n^2);$$

$$p_n(t) = \frac{\int_0^L \varphi_n(x) f(x,t) dx}{\int_0^L \varphi_n^2(x) m(x) dx} \quad n = 1, 2, \dots, \infty$$

$$y(x,t) = \sum_{n=1}^{\infty} \varphi_n(x) \left\{ \exp(-\eta_n \omega_n t) [A_n \cos \omega_{dn} t + B_n \sin \omega_{dn} t] + \int_0^t h_n(t-\tau) p_n(\tau) d\tau \right\}$$

- Displacement: $y(x, t) = \sum_{n=1}^{N \rightarrow \infty} a_n(t) \phi_n(x)$

- Slope: $y'(x, t) = \sum_{n=1}^{N \rightarrow \infty} a_n(t) \phi'_n(x)$

- Bending moment: $EI(x) y''(x, t) = \sum_{n=1}^{N \rightarrow \infty} a_n(t) EI(x) \phi''_n(x)$

- Shear force: $\left[EI(x) y''(x, t) \right]' = \sum_{n=1}^{N \rightarrow \infty} a_n(t) \left[EI(x) \phi''_n(x) \right]'$

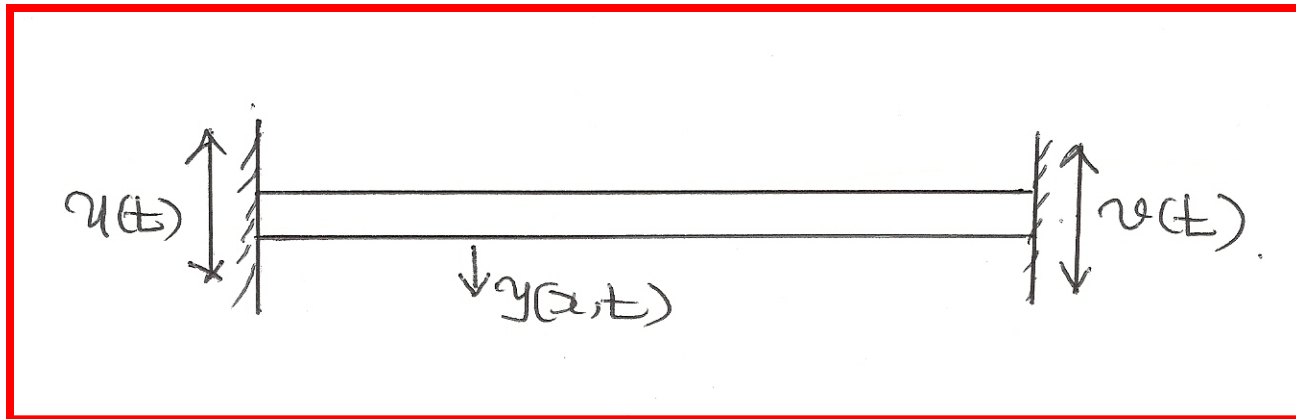
Other quantities

- Bending stress

- Shear stress

- Principal stresses

A clamped beam under differential support displacements



$$EIy^{iv} + m\ddot{y} + c\dot{y} = 0$$

$$y(0, t) = u(t); y'(0, t) = 0$$

$$y(l, t) = v(t); y'(l, t) = 0$$

$$y(x, 0) = 0; \dot{y}(x, 0) = 0$$

The BCS are time dependent.

Modal expansion method cannot be used directly.

Introduce a new dependent variable

$$y(x, t) = w(x, t) + h_1(x)u(t) + h_2(x)v(t)$$

$$y(0, t) = w(0, t) + h_1(0)u(t) + h_2(0)v(t) = u(t)$$

Select $w(0, t) = 0$; $h_1(0) = 1$; & $h_2(0) = 0$

$$y'(0, t) = w'(0, t) + h_1'(0)u(t) + h_2'(0)v(t) = 0$$

Select $w'(0, t) = 0$; $h_1'(0) = 0$; & $h_2'(0) = 0$

$$y(l, t) = w(l, t) + h_1(l)u(t) + h_2(l)v(t) = v(t)$$

Select $w(l, t) = 0$; $h_1(l) = 0$; & $h_2(l) = 1$

$$y'(l, t) = w'(l, t) + h_1'(l)u(t) + h_2'(l)v(t) = 0$$

Select $w'(l, t) = 0$; $h_1'(l) = 0$; & $h_2'(l) = 0$

$$EI \left[w^{iv} + \underline{h_1^{iv}} u + \underline{h_2^{iv}} v \right] + m \left[\ddot{w} + h_1 \ddot{u} + h_2 \ddot{v} \right] + c \left[\dot{w} + h_1 \dot{u} + h_2 \dot{v} \right] = 0$$

Select

$$h_1^{iv} = 0$$

$$h_2^{iv} = 0$$

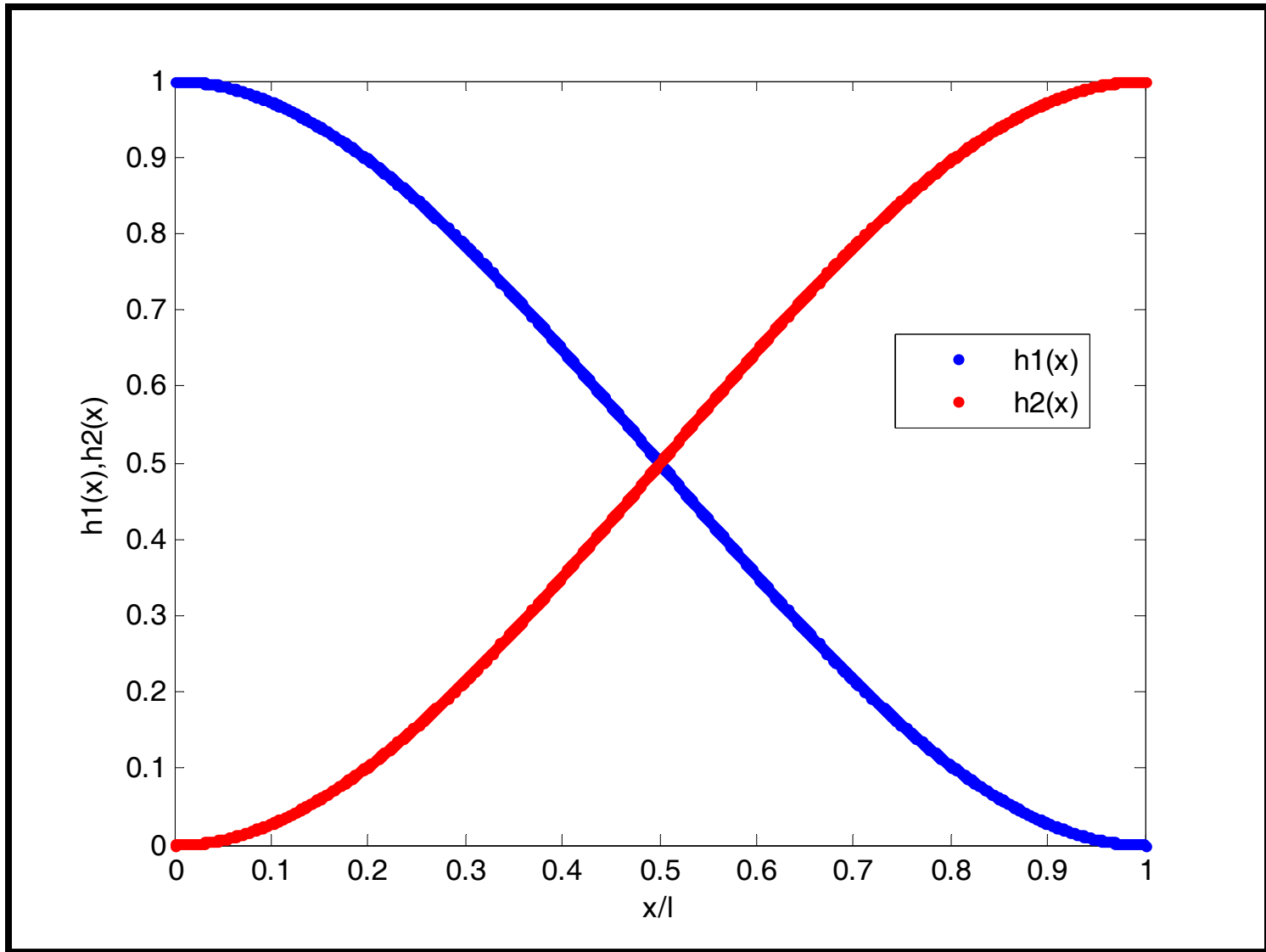
$$h_1(x) = ax^3 + bx^2 + cx + d$$

$$h_1(0) = 1; h_1(l) = 0; h_1'(0) = 0; h_1'(l) = 0;$$

$$h_1(x) = 1 - \frac{3x^2}{L^2} + \frac{2x^3}{L^3} //$$

Similarly

$$h_2(x) = \frac{3x^2}{L^2} - \frac{2x^3}{L^3}$$



$$EI \left[w^{iv} + h_1^{iv} u + h_2^{iv} v \right] + m \left[\ddot{w} + h_1 \ddot{u} + h_2 \ddot{v} \right] + c \left[\dot{w} + h_1 \dot{u} + h_2 \dot{v} \right] = 0$$

$$\Rightarrow EI w^{iv} + m \ddot{w} + c \dot{w} =$$

$$-m \left[\ddot{u} \left(1 - \frac{3x^2}{L^2} + \frac{2x^3}{L^3} \right) + \ddot{v} \left(\frac{3x^2}{L^2} - \frac{2x^3}{L^3} \right) \right]$$

$$-c \left[\dot{u} \left(1 - \frac{3x^2}{L^2} + \frac{2x^3}{L^3} \right) + \dot{v} \left(\frac{3x^2}{L^2} - \frac{2x^3}{L^3} \right) \right] = f(x, t)$$

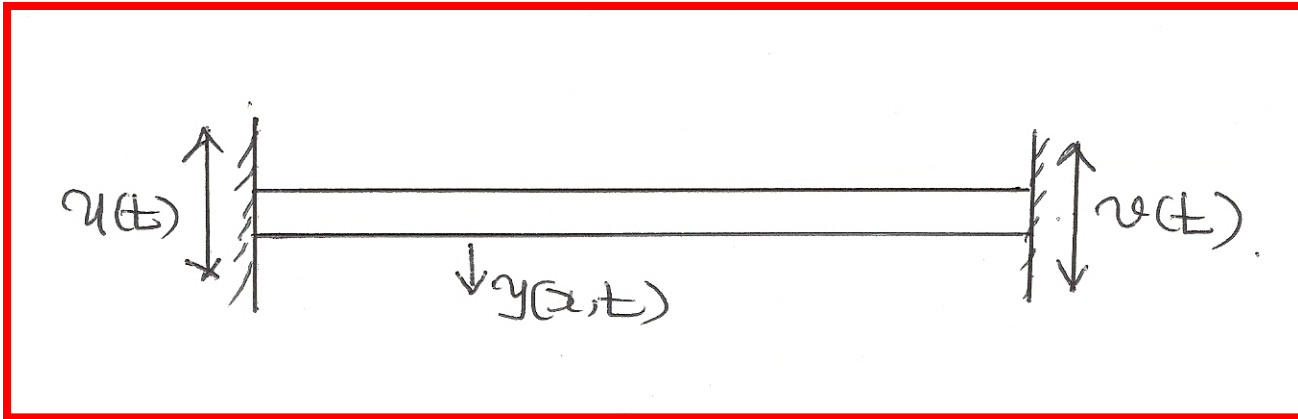
$$w(0, t) = 0; w'(0, t) = 0$$

$$w(l, t) = 0; w'(l, t) = 0$$

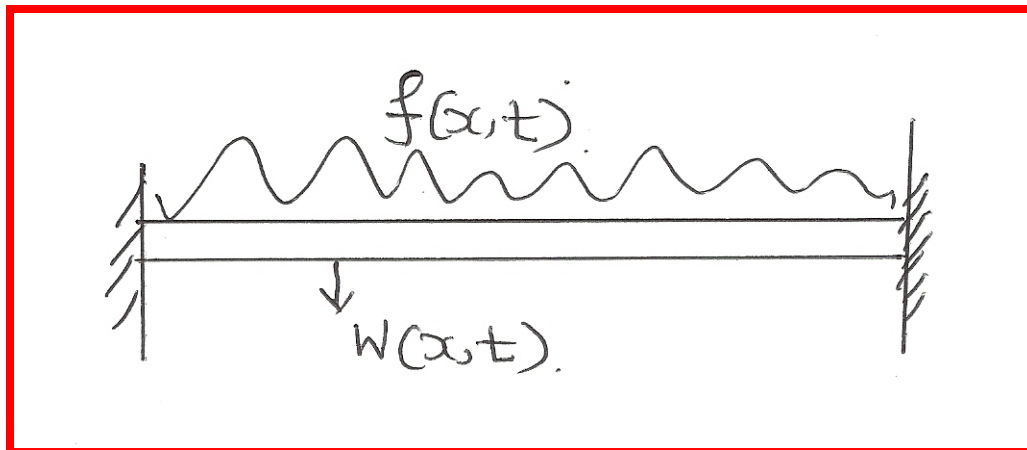
$$w(x, 0) = -h_1(x)u(0) - h_2(x)v(0)$$

$$\dot{w}(x, 0) = -h_1(x)\dot{u}(0) - h_2(x)\dot{v}(0)$$

Eigenfunction expansion method can now be used.



$$y(x,t) = w(x,t) + [h_1(x)u(t) + h_2(x)v(t)]$$



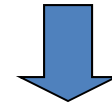
$$y(x, t) = w(x, t) + [h_1(x)u(t) + h_2(x)v(t)]$$



**Total
response**



**Dynamic
response**

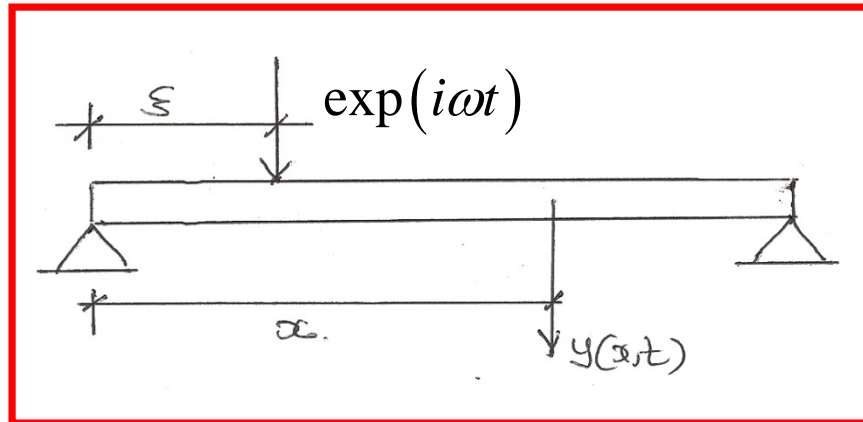


**Pseudo-dynamic
response**



$$\begin{Bmatrix} u^T \\ u_g \end{Bmatrix} = \begin{Bmatrix} u(t) \\ 0 \end{Bmatrix} + \begin{Bmatrix} u^p(t) \\ u_g(t) \end{Bmatrix}$$

Harmonically driven beam: Green's functions in frequency domain



$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = \exp(i\omega t) \delta(x - \xi)$$

$$\text{ICS: } y_0(x) = y(x, 0) \quad \dot{y}_0(x) = \dot{y}(x, 0)$$

$$\text{BCS: } y(0, t) = 0; EIy''(0, t) = 0; y(L, t) = 0; EIy''(L, t) = 0$$

$$\lim_{t \rightarrow \infty} y(x, t) = ?$$

$$y(x, t) = \sum_{n=1}^{\infty} a_n(t) \varphi_n(x)$$

$$\left[EI \varphi_n'' \right]'' = m \omega_n^2 \varphi_n(x)$$

$$\int_0^L EI \varphi_n'' \varphi_k'' dx = 0 \quad n \neq k \quad \int_0^L m \varphi_n \varphi_k dx = 0 \quad n \neq k$$

$$\begin{aligned} \ddot{a}_n + 2\eta_n \omega_n \dot{a}_n + \omega_n^2 a_n &= \int_0^L \exp(i\omega t) \phi_n(x) \delta(x - \xi) dx \\ &= \phi_n(\xi) \exp(i\omega t); \\ n &= 1, 2, \dots, \infty \end{aligned}$$

$$\lim_{t \rightarrow \infty} a_n(t) \rightarrow \frac{\phi_n(\xi) \exp(i\omega t)}{\omega_n^2 - \omega^2 + i2\eta_n \omega \omega_n}$$

\Rightarrow

$$\lim_{t \rightarrow \infty} y(x, t) = \sum_{n=1}^{N \rightarrow \infty} \frac{\phi_n(x) \phi_n(\xi) \exp(i\omega t)}{\omega_n^2 - \omega^2 + i2\eta_n \omega \omega_n}$$

$$= G(x, \xi, \omega) \exp(i\omega t)$$

with

$$G(x, \xi, \omega) = \sum_{n=1}^{N \rightarrow \infty} \frac{\phi_n(x) \phi_n(\xi)}{\omega_n^2 - \omega^2 + i2\eta_n \omega \omega_n}$$

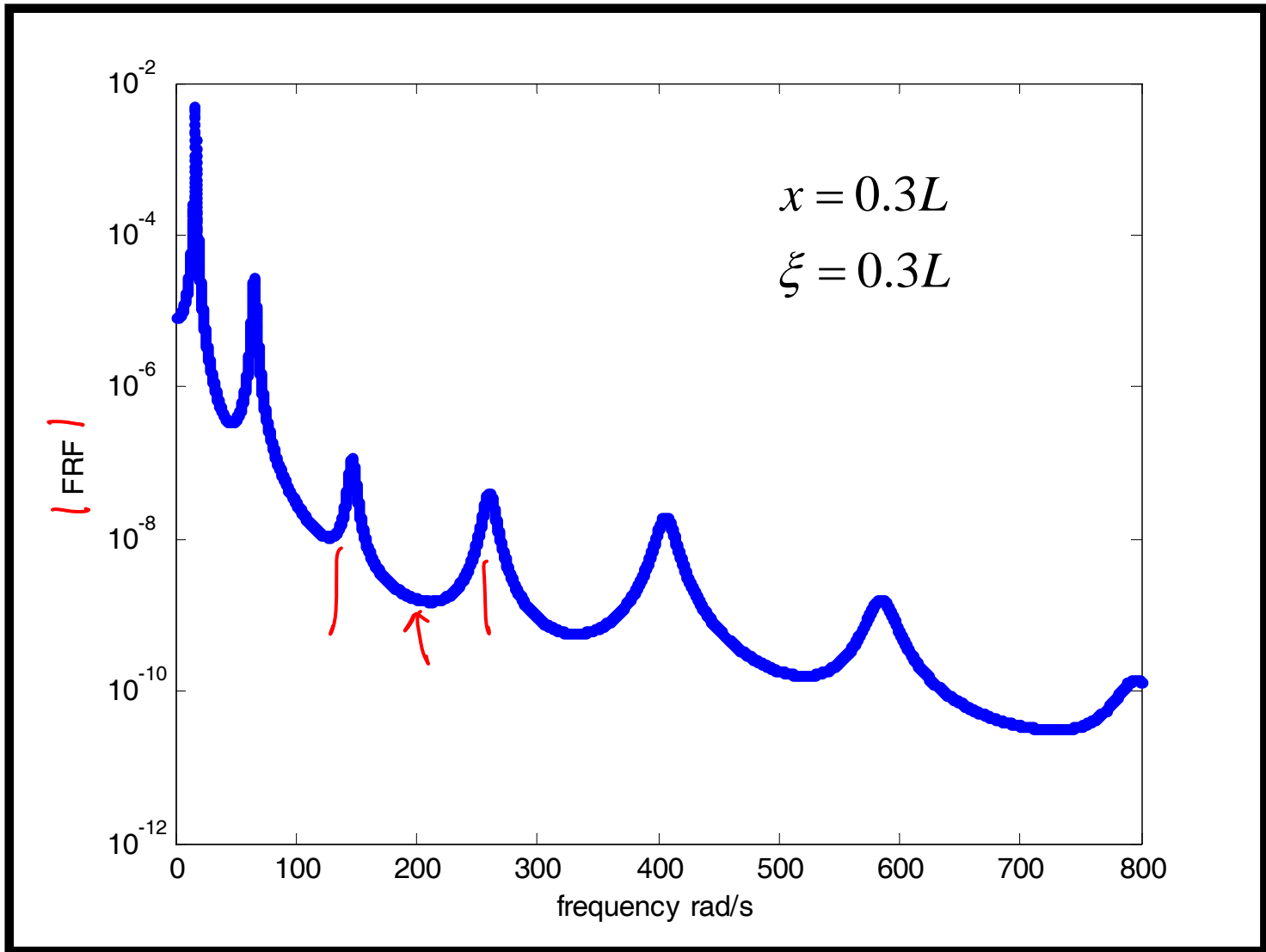
$$G(x, \xi, \omega) = \text{Green's function}$$

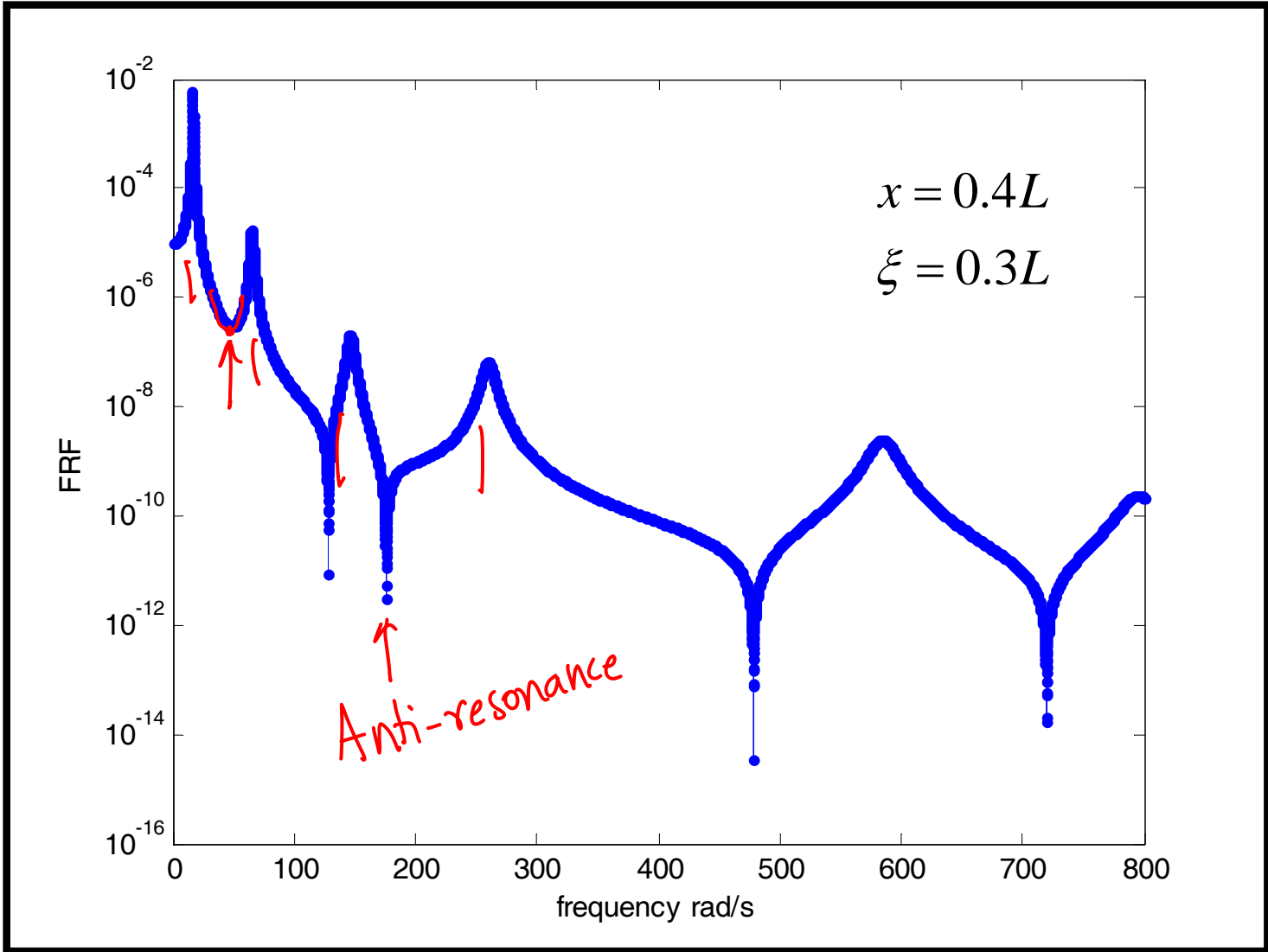
Note

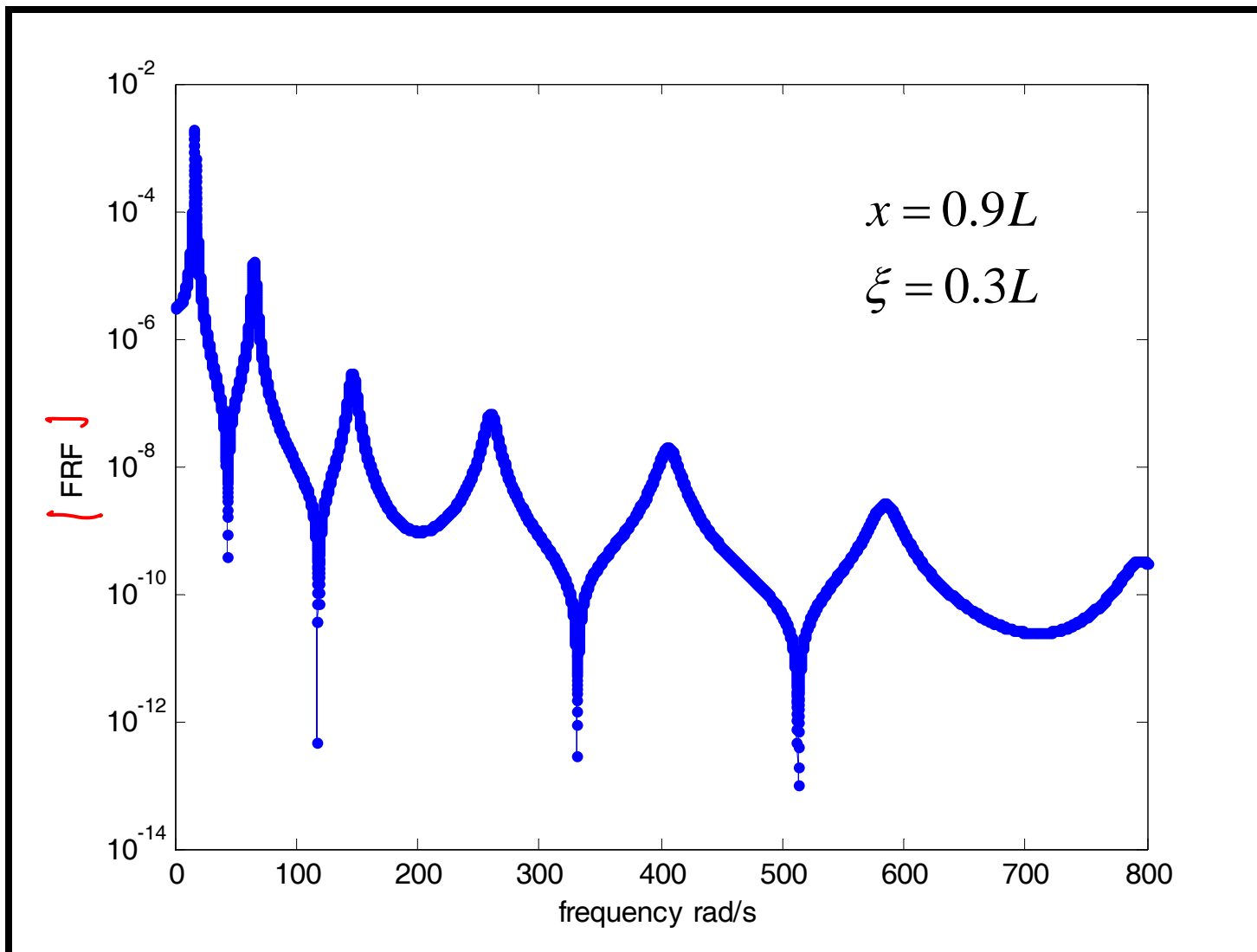
- $G(x, \xi, \omega) = G(\xi, x, \omega)$
- $G(x, \xi, \omega)$ is complex valued
- $G(x, \xi, \omega)$ is the generalization of the FRF discussed earlier

$$H_{ij}(\omega)$$

x, ξ

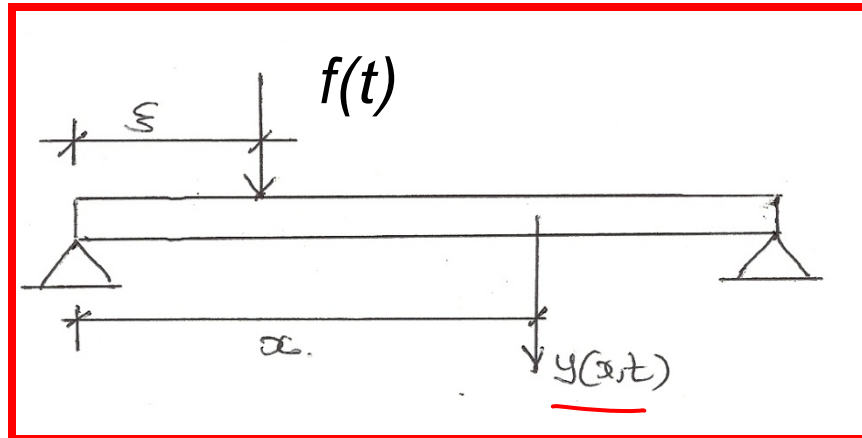






Response of beam to a general load $f(t)$

Note: the Fourier transform of $f(t)$ is taken to exist



$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = f(t) \delta(x - \xi)$$

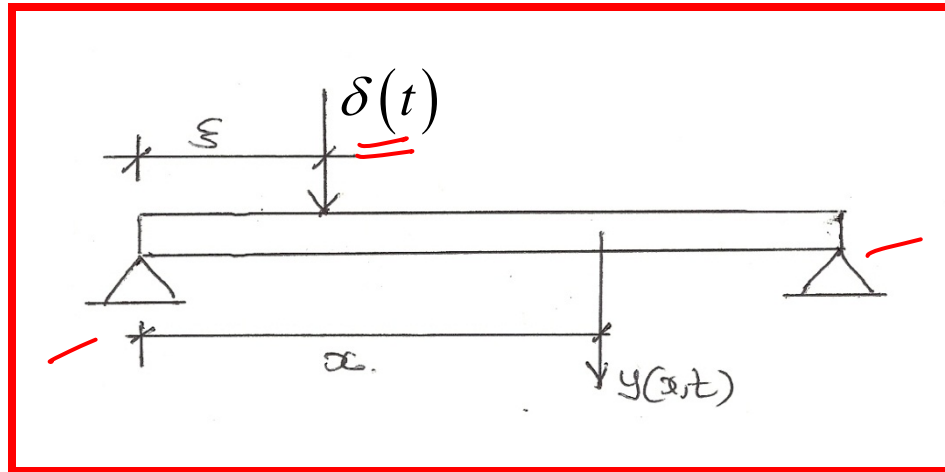
$$\text{ICS: } y_0(x) = y(x, 0) \quad \dot{y}_0(x) = \dot{y}(x, 0)$$

$$\text{BCS: } y(0, t) = 0; EIy''(0, t) = 0; y(L, t) = 0; EIy''(L, t) = 0$$

$$Y(\omega) = H(\omega) F(\omega)$$

$$Y(x, \omega) = G(x, \xi, \omega) F(\omega)$$

Beam driven by impulse excitation: Green's functions in time domain



$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = \underline{\underline{\delta(t-0) \delta(x-\xi)}}$$


$$\text{ICS: } y_0(x) = y(x, 0) = 0 \quad \dot{y}_0(x) = \dot{y}(x, 0) = 0$$

$$\text{BCS: } y(0, t) = 0; EIy''(0, t) = 0; y(L, t) = 0; EIy''(L, t) = 0$$

$$y(x, t) = \sum_{n=1}^{\infty} a_n(t) \varphi_n(x)$$

$$\left[EI \varphi_n'' \right]'' = m \omega_n^2 \varphi_n(x)$$

$$\int_0^L EI \varphi_n'' \varphi_k'' dx = 0 \quad n \neq k \quad \int_0^L m \varphi_n \varphi_k dx = 0 \quad n \neq k$$


$$\begin{aligned} \ddot{a}_n + 2\eta_n \omega_n \dot{a}_n + \omega_n^2 a_n &= \int_0^L \phi_n(x) \delta(t) \delta(x - \xi) dx \\ &= \phi_n(\xi) \delta(t); \\ n &= 1, 2, \dots, \infty \end{aligned}$$

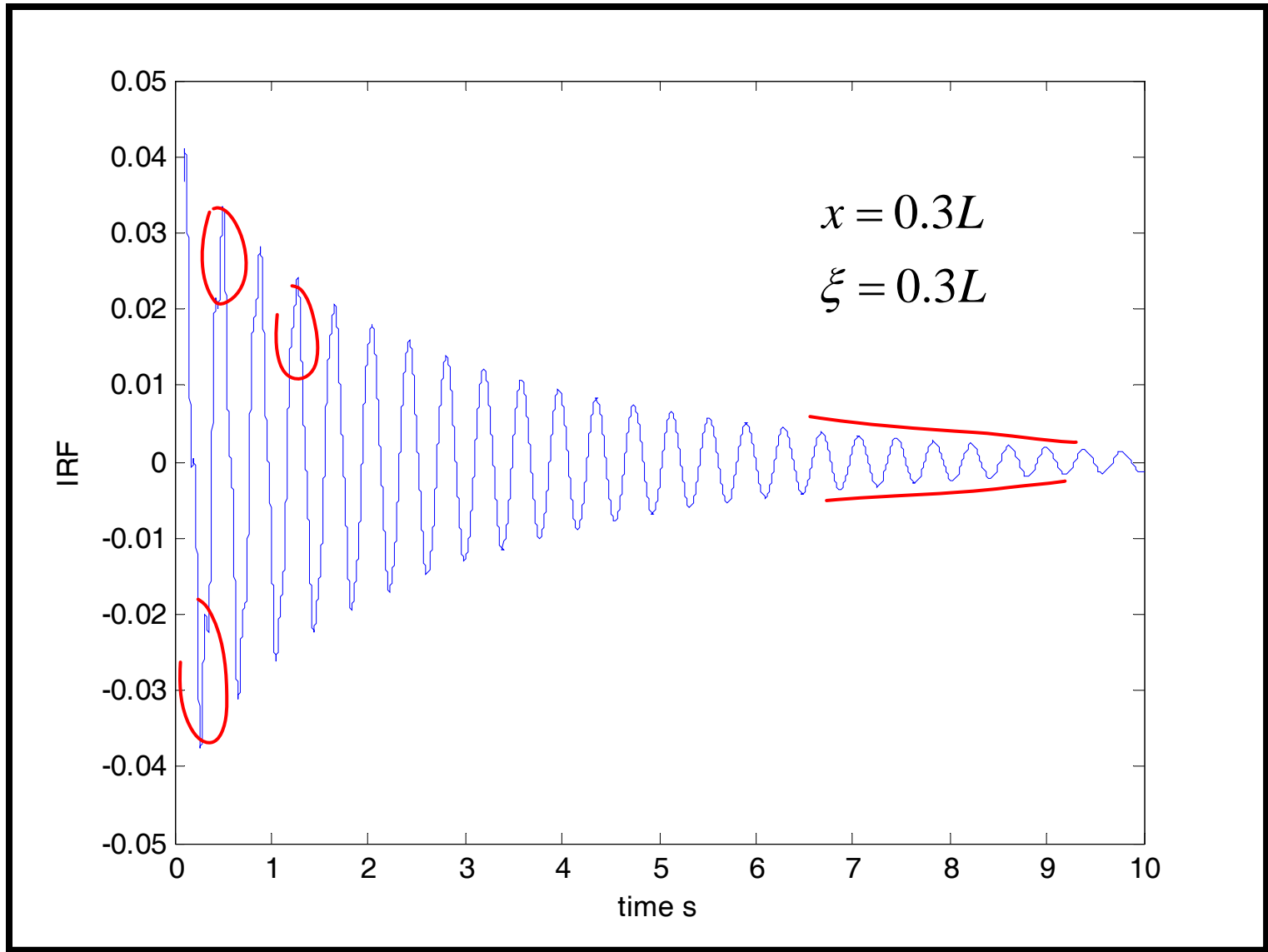
$$a_n(t) = \phi_n(\xi) h_n(t)$$

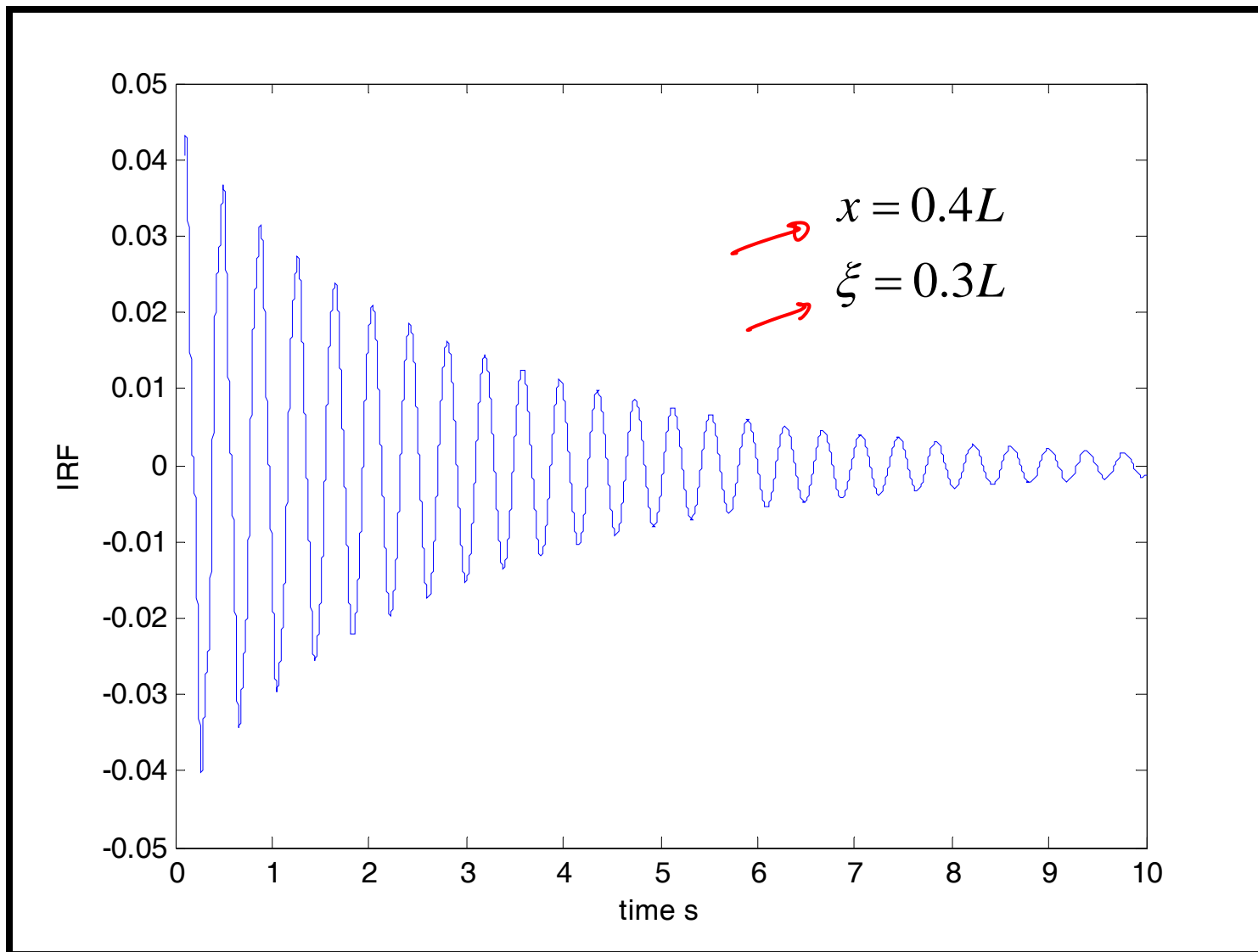
$$M_n = 1 \int_0^L m \phi_n^2(x) dx = 1$$

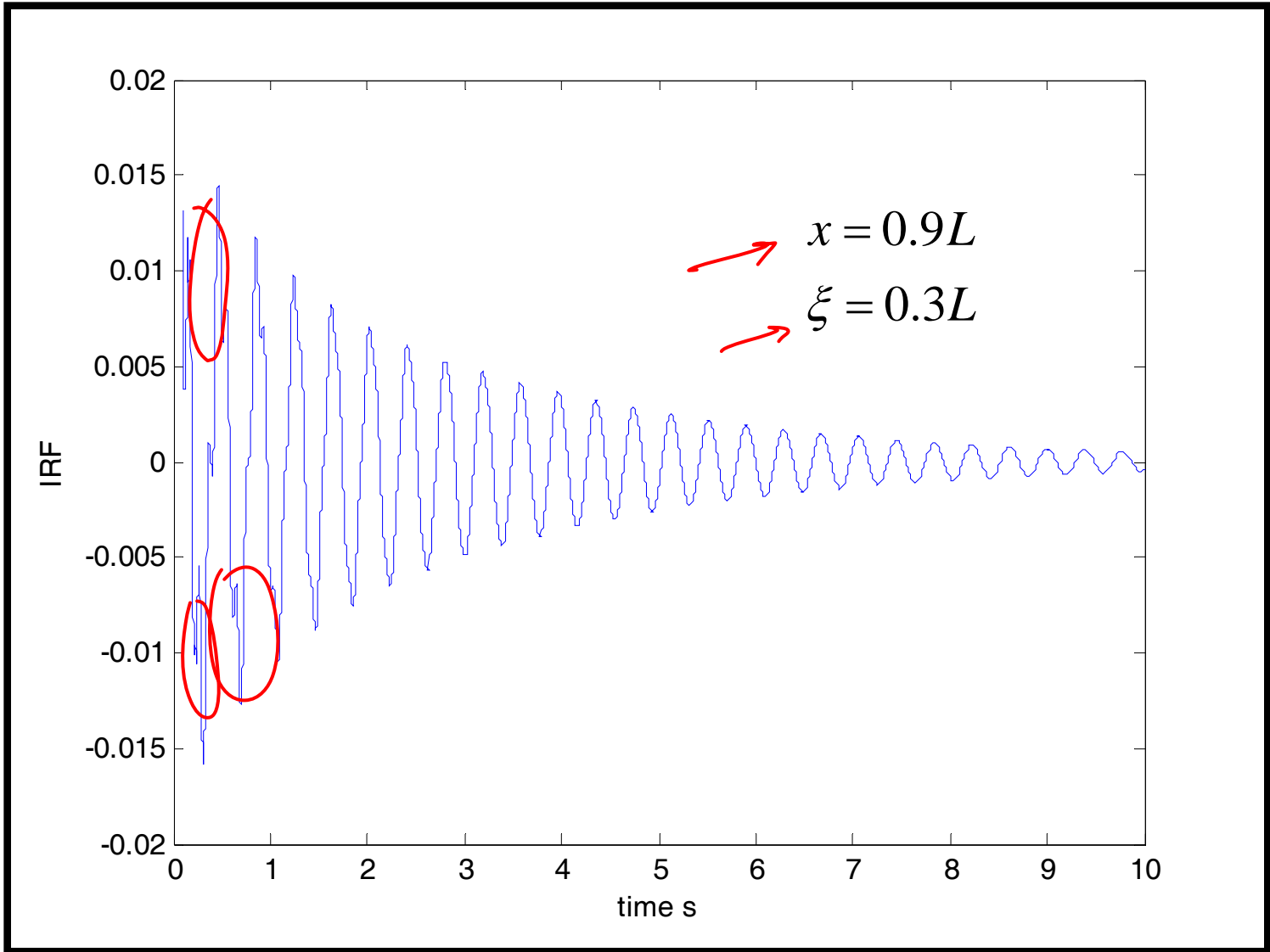
$$= \frac{\phi_n(\xi)}{m_n \omega_{dn}} \exp(-\eta_n \omega_n t) \sin(\omega_{dn} t) \quad \checkmark$$

$$y(x, t) = \sum_{n=1}^{N \rightarrow \infty} \frac{\phi_n(\xi) \phi_n(x)}{\omega_{dn}} \exp(-\eta_n \omega_n t) \sin(\omega_{dn} t)$$
$$= g(x, \xi, t)$$

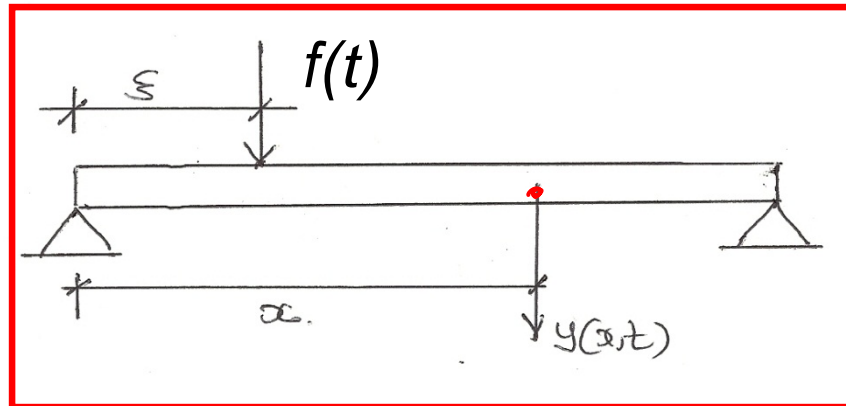
$$g(x, \xi, t) = g(\xi, x, t)$$







Response of beam to a concentrated load $f(t)$



$$y(x,t) = \int_0^t h(x,\xi,t-\tau) f(\tau) d\tau$$

$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = f(t) \delta(x - \xi)$$

ICS: $y_0(x) = y(x, 0) = 0$ $\dot{y}_0(x) = \dot{y}(x, 0) = 0$

BCS: $y(0, t) = 0; EIy''(0, t) = 0; y(L, t) = 0; EIy''(L, t) = 0$

hij

$$y(x, t) = \int_0^t g(x, \xi, t - \tau) f(\tau) d\tau$$

Exercise

Show that

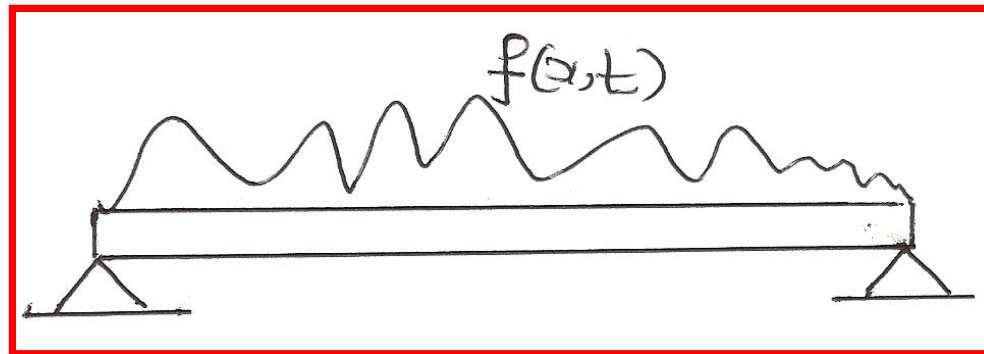
$$\underline{g}(x, \xi, t) \Leftrightarrow \underline{G}(x, \xi, \omega) \quad h(t) \Leftrightarrow H(\omega)$$

That is

$$G(x, \xi, \omega) = \int_{-\infty}^{\infty} g(x, \xi, t) \exp(i\omega t) dt$$

$$g(x, \xi, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} G(x, \xi, \omega) \exp(-i\omega t) d\omega$$


Response of beam to a general load $f(x,t)$




$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = \underline{\underline{f(x,t)}}$$

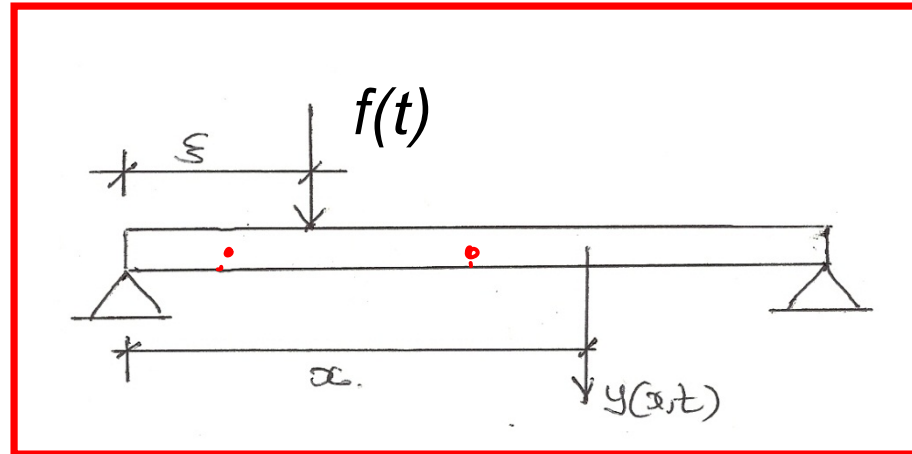
$$\text{ICS: } y_0(x) = y(x,0) = 0 \quad \dot{y}_0(x) = \dot{y}(x,0) = 0 \quad \leftarrow$$

$$\text{BCS: } y(0,t) = 0; EIy''(0,t) = 0; y(L,t) = 0; EIy''(L,t) = 0$$


$$y(x, t) = \int_0^L \int_0^t \underline{g(x, \xi, t - \tau)} \underline{f(\xi, \tau)} d\xi d\tau$$


$$Y(x, \omega) = \int_0^L \underline{G(x, \xi, \omega)} \underline{F(\xi, \omega)} d\xi$$

Response of beam to a concentrated random load $f(t)$



$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = \underline{\underline{f(t) \delta(x - \xi)}}$$

$$\underline{\langle f(t) \rangle} = 0; \underline{\langle f(t) f(t + \tau) \rangle} = \underline{R_{ff}(\tau)} \iff S_{ff}(\omega)$$

$$\text{ICS: } y_0(x) = y(x, 0) = 0 \quad \dot{y}_0(x) = \dot{y}(x, 0) = 0$$

$$\text{BCS: } y(0, t) = 0; EIy''(0, t) = 0; y(L, t) = 0; EIy''(L, t) = 0$$

$$y(x, t) = \int_0^t g(x, \xi, t - \tau) f(\tau) d\tau$$

$$\langle y(x, t) \rangle = \int_0^t g(x, \xi, t - \tau) \langle f(\tau) \rangle d\tau = 0 \quad \checkmark$$

$$\langle y(\underline{x}_1, t_1) y(\underline{x}_2, t_2) \rangle = \int_0^{t_1} \int_0^{t_2} g(x_1, \xi, t_1 - \tau_1) g(x_2, \xi, t_2 - \tau_2) \langle \underline{f}(\tau_1) \underline{f}(\tau_2) \rangle d\tau_1 d\tau_2$$

$$= \int_0^{t_1} \int_0^{t_2} g(x_1, \xi, t_1 - \tau_1) g(x_2, \xi, t_2 - \tau_2) R_{ff}(\tau_1, \tau_2) d\tau_1 d\tau_2$$

$$= \int_0^{t_1} \int_0^{t_2} g(x_1, \xi, t_1 - \tau_1) g(x_2, \xi, t_2 - \tau_2) R_{ff}(\tau_1 - \tau_2) d\tau_1 d\tau_2$$

$$\begin{aligned}
\langle y(x_1, t_1) y(x_2, t_2) \rangle &= \int_0^{t_1} \int_0^{t_2} g(x_1, \xi, t_1 - \tau_1) g(x_2, \xi, t_2 - \tau_2) \underline{R_{ff}(\tau_1 - \tau_2)} d\tau_1 d\tau_2 \\
&= \int_0^{t_1} \int_0^{t_2} g(x_1, \xi, t_1 - \tau_1) g(x_2, \xi, t_2 - \tau_2) \left[\frac{1}{\pi} \int_0^{\infty} S_{ff}(\omega) \cos \omega(\tau_1 - \tau_2) d\omega \right] d\tau_1 d\tau_2 \\
&= \int_0^{\infty} S_{ff}(\omega) \mathbf{H}(x_1, x_2, \xi, t_1, t_2, \omega) d\omega // \\
\mathbf{H}(x_1, x_2, \xi, t_1, t_2, \omega) &= \int_0^{t_1} \int_0^{t_2} \underline{g(x_1, \xi, t_1 - \tau_1)} \underline{g(x_2, \xi, t_2 - \tau_2)} \underline{\cos \omega(\tau_1 - \tau_2)} d\tau_1 d\tau_2 \\
\langle y^2(x, t) \rangle &= \int_0^{\infty} S_{ff}(\omega) \mathbf{H}(x, x, \xi, t, t, \omega) d\omega
\end{aligned}$$

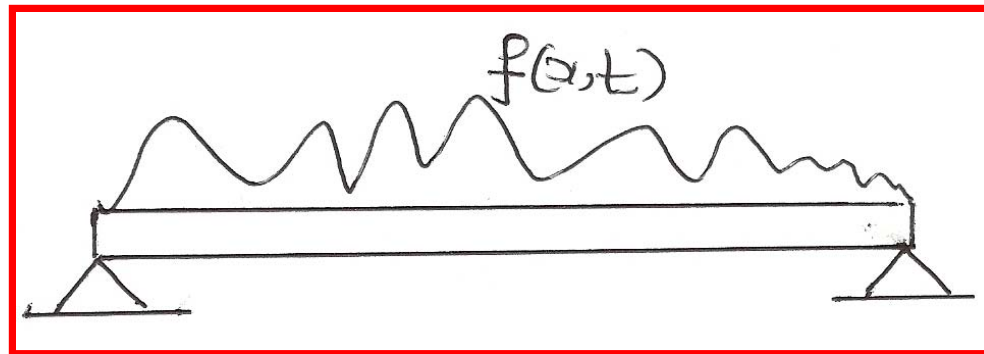
Steady state response

$$\rightarrow Y_T(x, \xi, \omega) = G(x, \xi, \omega) \underline{F_T(\omega)}$$

$$\underline{S_{YY}(x, \xi, \omega)} = \lim_{T \rightarrow \infty} \frac{1}{T} \left\langle |Y_T(x, \xi, \omega)|^2 \right\rangle$$

$$= |G(x, \xi, \omega)|^2 S_{FF}(\omega)$$

Beam excited by space-time white noise forcing
(Rain on the roof excitation)



$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \nu EI(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + \underline{m(x) \ddot{y}} + \underline{c(x) \dot{y}} = \underline{f(x,t)}$$

$$\langle \underline{f(x,t)} \rangle = 0; \langle \underline{f(x,t) f(x+\xi, t+\tau)} \rangle = I_0 \underline{m(x)} \delta(\xi) \delta(\tau)$$

$$\text{ICS: } y_0(x) = y(x, 0) = 0 \quad \dot{y}_0(x) = \dot{y}(x, 0) = 0$$

$$\text{BCS: } y(0, t) = 0; EIy''(0, t) = 0; y(L, t) = 0; EIy''(L, t) = 0$$

$$y(x, t) = \sum_{n=1}^{\infty} \underline{a_n(t)} \underline{\phi_n(x)}$$

$$[EI \phi_n'']'' = m \omega_n^2 \phi_n(x) \quad \rightarrow$$

$$\int_0^L EI \phi_n'' \phi_k'' dx = 0 \quad n \neq k \quad \int_0^L m \phi_n \phi_k dx = 0 \quad n \neq k$$

$$\underline{\ddot{a}_n + 2\eta_n \omega_n \dot{a}_n + \omega_n^2 a_n} = \int_0^L \underline{\phi_n(x) f(x, t)} dx; n = 1, 2, \dots, \infty$$

$$a_n(t) = \int_0^t \int_0^L h_n(t - \tau) \phi_n(x) f(x, \tau) dx d\tau$$

$$a_n(t) = \int_0^t \int_0^L h_n(t-\tau) \phi_n(x) \underline{f(x, \tau)} dx d\tau$$

$$\langle \underline{a_n(t)} \rangle = \int_0^t \int_0^L h_n(t-\tau) \phi_n(x) \langle \underline{f(x, \tau)} \rangle dx d\tau = \underline{0}$$

$$\langle \underline{a_n(t_1)} a_k(t_2) \rangle = \int_0^{t_1} \int_0^{t_2} \int_0^L \int_0^L h_n(t_1-\tau_1) \phi_n(x_1) h_k(t_2-\tau_2) \phi_k(x_2)$$

$$\langle \underline{f(x_1, \tau_1)} f(x_2, \tau_2) \rangle dx_1 dx_2 d\tau_1 d\tau_2$$

$$= \int_0^{t_1} \int_0^{t_2} \int_0^L \int_0^L h_n(t_1-\tau_1) \phi_n(x_1) h_k(t_2-\tau_2) \phi_k(x_2)$$

$$I_0 m(x_1) \delta(\tau_1 - \tau_2) \delta(x_1 - x_2) dx_1 dx_2 d\tau_1 d\tau_2$$

$$\langle a_n(t_1) a_k(t_2) \rangle = \int_0^{t_1} \int_0^{t_2} \int_0^L \int_0^L h_n(t_1 - \tau_1) \phi_n(x_1) h_k(t_2 - \tau_2) \phi_k(x_2)$$

$$I_0 m(x_1) \delta(\tau_1 - \tau_2) \delta(x_1 - x_2) dx_1 dx_2 d\tau_1 d\tau_2$$

$$= \int_0^{t_2} \int_0^L h_n(t_1 - \tau_2) h_k(t_2 - \tau_2) I_0 m(x_2) \phi_n(x_2) \phi_k(x_2) dx_2 d\tau_2$$

$$= 0 \text{ for } n \neq k$$

$$\int_0^L m(x) \phi_n(x) \phi_k(x) dx$$

Generalized
coordinates
are uncorrelated

$$= \int_0^{t_2} h_n^2(t_1 - \tau) I_0 d\tau \text{ for } n = k$$

⇒

$$\langle a_n^2(t) \rangle = \int_0^t h_n^2(t - \tau) I_0 d\tau //$$

$$y(x, t) = \sum_{n=1}^{N \rightarrow \infty} a_n(t) \phi_n(x)$$

\Rightarrow

$$\langle y(x, t) \rangle = \sum_{n=1}^{N \rightarrow \infty} \phi_n(x) \langle \underline{a_n(t)} \rangle = 0$$

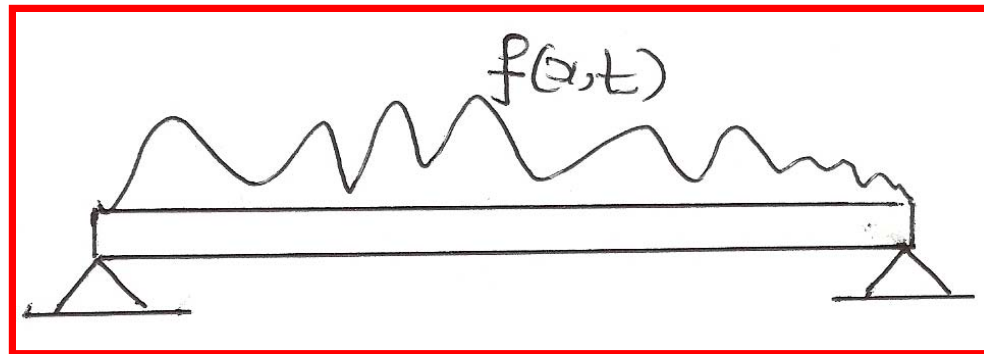
$$\langle y(x_1, t_1) y(x_2, t_2) \rangle = \sum_{n=1}^{N \rightarrow \infty} \sum_{k=1}^{N \rightarrow \infty} \phi_n(x_1) \phi_k(x_2) \langle \underline{a_n(t_1) a_k(t_2)} \rangle$$

$$= \sum_{n=1}^{N \rightarrow \infty} \phi_n(x_1) \phi_n(x_2) \langle a_n(t_1) a_n(t_2) \rangle$$

\Rightarrow

$$\langle y^2(x, t) \rangle = \sum_{n=1}^{N \rightarrow \infty} \langle \underline{a_n^2(t)} \rangle \phi_n^2(x)$$

Beam excited by a space-time random process



$$\underline{EI} \frac{\partial^4 y}{\partial x^4} + \underline{m}\ddot{y} + \underline{c}\dot{y} = f(x,t)$$

$$\langle \underline{f(x,t)} \rangle = 0; \langle \underline{f(x,t) f(x+\xi, t+\tau)} \rangle = \underline{I_0} \underline{\delta(\xi)} \underline{R(\tau)}$$

$$\text{ICS: } y_0(x) = y(x,0) = 0 \quad \dot{y}_0(x) = \dot{y}(x,0) = 0$$

$$\text{BCS: } y(0,t) = 0; EIy''(0,t) = 0; y(L,t) = 0; EIy''(L,t) = 0$$

$$y(x, t) = \sum_{n=1}^{\infty} a_n(t) \phi_n(x)$$

$$= \sum_{n=1}^{\infty} \phi_n(x) \int_0^t \int_0^L h_n(t-\tau) \phi_n(s) f(s, \tau) ds d\tau$$

$$\Rightarrow \langle y(x, t) \rangle = \sum_{n=1}^{\infty} \phi_n(x) \int_0^t \int_0^L h_n(t-\tau) \phi_n(s) \langle f(s, \tau) \rangle ds d\tau = \underline{\underline{0}}$$

$$\langle y(x_1, t_1) y(x_2, t_2) \rangle = \sum_{n=1}^{\infty} \sum_{k=1}^{\infty} \phi_n(x_1) \phi_k(x_2) \int_0^{t_1} \int_0^{t_2} \int_0^L \int_0^L h_n(t_1 - \tau_1) h_k(t_2 - \tau_2)$$

$$\phi_n(s_1) \phi_k(s_2) \langle f(s_1, \tau_1) f(s_2, \tau_2) \rangle ds_1 ds_2 d\tau_1 d\tau_2$$

$$= \sum_{n=1}^{\infty} \sum_{k=1}^{\infty} \phi_n(x_1) \phi_k(x_2) \int_0^{t_1} \int_0^{t_2} \int_0^L \int_0^L h_n(t_1 - \tau_1) h_k(t_2 - \tau_2)$$

$$\phi_n(s_1) \phi_k(s_2) \delta(s_1 - s_2) R(\tau_1 - \tau_2) ds_1 ds_2 d\tau_1 d\tau_2$$

$$\langle y(x_1, t_1) y(x_2, t_2) \rangle = \sum_{n=1}^{\infty} \sum_{k=1}^{\infty} \phi_n(x_1) \phi_k(x_2) \int_0^{t_1} \int_0^{t_2} \int_0^L \int_0^L h_n(t_1 - \tau_1) h_k(t_2 - \tau_2)$$

$$\phi_n(s_1) \phi_k(s_2) \delta(s_1 - s_2) R(\tau_1 - \tau_2) ds_1 ds_2 d\tau_1 d\tau_2$$

$$= \sum_{n=1}^{\infty} \sum_{k=1}^{\infty} \phi_n(x_1) \phi_k(x_2) \int_0^{t_1} \int_0^{t_2} \int_0^L h_n(t_1 - \tau_1) h_k(t_2 - \tau_2) \underbrace{\phi_n(s_2)} \underbrace{\phi_k(s_2)} R(\tau_1 - \tau_2) ds_2 d\tau_1 d\tau_2$$

Recall

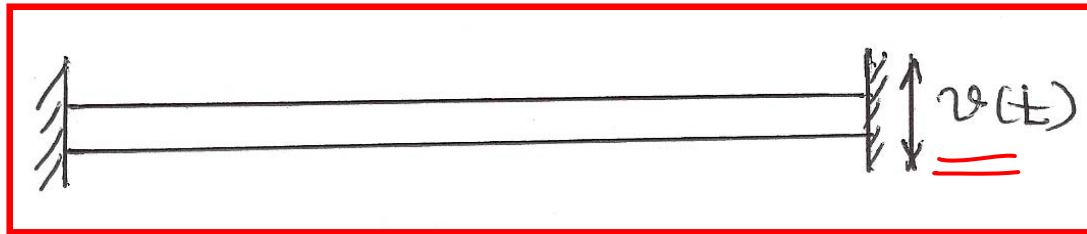
$$\int_0^L m \phi_n \phi_k dx = \delta_{nk} \Rightarrow //$$

m constant

c constant

$$\langle y(x_1, t_1) y(x_2, t_2) \rangle = \sum_{n=1}^{\infty} \phi_n(x_1) \phi_n(x_2) (1/m) \int_0^{t_1} \int_0^{t_2} h_n(t_1 - \tau_1) h_n(t_2 - \tau_2) R(\tau_1 - \tau_2) d\tau_1 d\tau_2$$

Beam under random support motions



$$EIy^{iv} + m\ddot{y} + c\dot{y} = 0$$

$$y(0, t) = 0; y'(0, t) = 0$$

$$y(l, t) = \underline{v(t)}; y'(l, t) = 0$$

$$y(x, 0) = 0; \dot{y}(x, 0) = 0$$

$$\langle v(t) \rangle = 0$$

$$\langle v(t)v(t+\tau) \rangle = R_{vv}(\tau) \Leftrightarrow S_{vv}(\omega)$$

Introduce a new dependent variable

$$y(x, t) = \underline{w(x, t)} + \underline{h(x)v(t)}$$

$$y(0, t) = w(0, t) + h(0)v(t) = 0$$

$$\text{Select } w(0, t) = 0; h(0) = 0$$

$$y'(0, t) = w'(0, t) + h'(0)v(t) = 0$$

$$\text{Select } w'(0, t) = 0; h'(0) = 0$$

$$y(l, t) = w(l, t) + h(l)v(t) = v(t)$$

$$\text{Select } w(l, t) = 0; h(l) = 1$$

$$y'(l, t) = w'(l, t) + h'(l)v(t) = 0$$

$$\text{Select } w'(l, t) = 0; h'(l) = 0$$

$$EI \left[w^{iv} + h^{iv} v \right] + m \left[\ddot{w} + h \ddot{v} \right] + c \left[\dot{w} + h \dot{v} \right] = 0$$

Select

$$h^{iv} = 0$$

$$h(x) = ax^3 + bx^2 + cx + d$$

$$h(0) = 0; h(l) = 1; h'(0) = 0; h'(l) = 0;$$

$$h(x) = \frac{3x^2}{L^2} - \frac{2x^3}{L^3}$$

$$EI \left[w^{iv} + h^{iv} v \right] + m \left[\ddot{w} + h\ddot{v} \right] + c \left[\dot{w} + h\dot{v} \right] = 0$$

$$\Rightarrow EI w^{iv} + m \ddot{w} + c \dot{w} =$$
$$-m \left[\ddot{v} \left(\frac{3x^2}{L^2} - \frac{2x^3}{L^3} \right) \right] - c \left[\dot{v} \left(\frac{3x^2}{L^2} - \frac{2x^3}{L^3} \right) \right] = \underline{\underline{f(x,t)}}$$

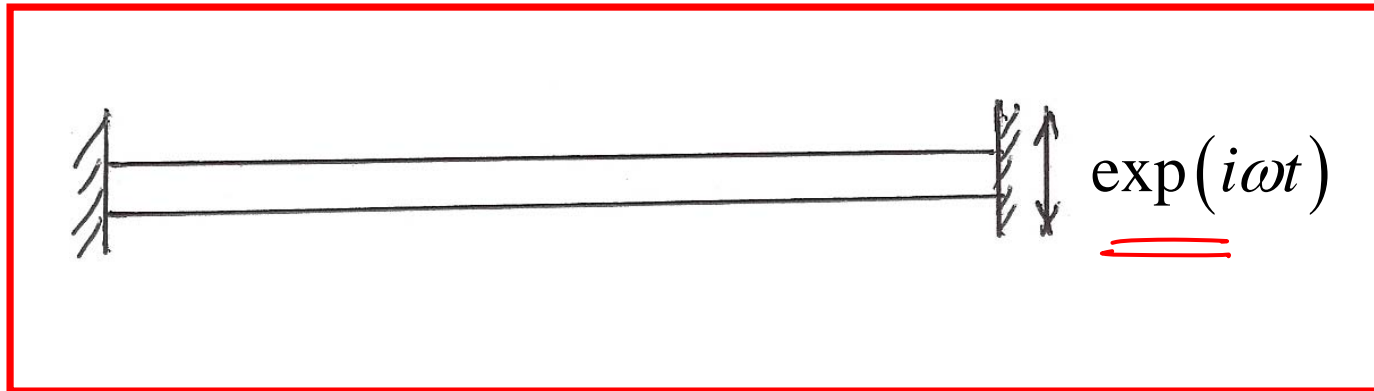
$$w(0,t) = 0; w'(0,t) = 0$$

$$w(l,t) = 0; w'(l,t) = 0$$

$$w(x,0) = -h(x)v(0)$$

$$w(x,0) = -h(x)\dot{v}(0)$$

Alternative approach for steady state response analysis



$$EIy^{iv} + m\ddot{y} + c\dot{y} = 0$$

$$y(0, t) = 0; y'(0, t) = 0$$

$$y(l, t) = \underline{\exp(i\omega t)}; y'(l, t) = 0$$

$$y(x, 0) = 0; \dot{y}(x, 0) = 0$$

$$EIy^{iv} + m\ddot{y} + c\dot{y} = 0$$

$$y(x, t) = \phi(x) \exp(i\omega t) \checkmark$$

$$y(x, t) = \phi(x) e^{i\omega t}$$

$$= e^{i\omega t}$$

$$Q(x) = 1$$

\Rightarrow

$$EI\phi^{iv} - m\omega^2\phi + i\omega c\phi = 0$$

$$\phi(0) = 0; \phi'(0) = 0; \phi(l) = 1; \phi'(l) = 0$$

\Rightarrow

$$\phi^{iv} - \lambda^4\phi = 0; \lambda^4 = \frac{m\omega^2 - i\omega c}{EI}$$

$$\phi(x) = a(\cos \lambda x + \cosh \lambda x) + b(\cos \lambda x - \cosh \lambda x)$$

$$+ c(\sin \lambda x + \sinh \lambda x) + d(\sin \lambda x - \sinh \lambda x)$$

$$\phi'(x) = a\lambda(-\sin \lambda x + \sinh \lambda x) + b\lambda(-\sin \lambda x - \sinh \lambda x)$$

$$+ c\lambda(\cos \lambda x + \cosh \lambda x) + d\lambda(\cos \lambda x - \cosh \lambda x)$$

$$\phi(0) = 0; \phi'(0) = 0; \phi(l) = 1; \phi'(l) = 0$$

$$\phi(x) = \underline{a}(\cos \lambda x + \cosh \lambda x) + b(\cos \lambda x - \cosh \lambda x)$$

$$+ \underline{c}(\sin \lambda x + \sinh \lambda x) + d(\sin \lambda x - \sinh \lambda x)$$

$$\phi'(x) = a\lambda(-\sin \lambda x + \sinh \lambda x) + b\lambda(-\sin \lambda x - \sinh \lambda x)$$

$$+ c\lambda(\cos \lambda x + \cosh \lambda x) + d\lambda(\cos \lambda x - \cosh \lambda x)$$

$$\phi(0) = 0 \Rightarrow a = 0 \quad \checkmark$$

$$\phi'(0) = 0 \Rightarrow c = 0 \quad \checkmark$$

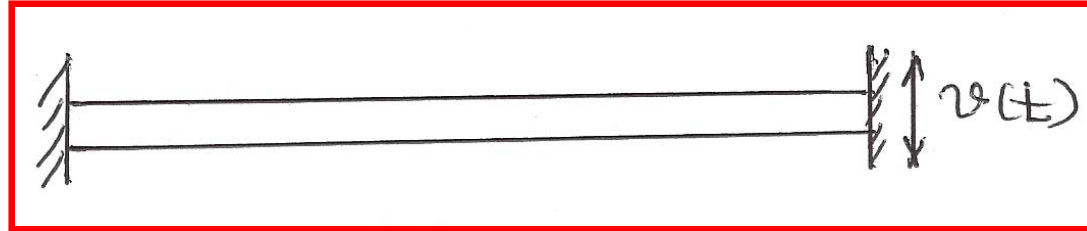
$$\phi(l) = 1 \Rightarrow b(\cos \lambda l - \cosh \lambda l) + d(\sin \lambda l - \sinh \lambda l) \quad \checkmark$$

$$\phi'(l) = 0 \Rightarrow b\lambda(-\sin \lambda l - \sinh \lambda l) + d\lambda(\cos \lambda l - \cosh \lambda l) = 0 \quad \checkmark$$

b & d can thus be determined.

$$\Rightarrow y(x, t) = \left\{ \left[b(\cos \lambda x - \cosh \lambda x) + d(\sin \lambda x - \sinh \lambda x) \right] \right\} \exp(i\omega t)$$

Random support motions



PSD function of $y(x, t)$

$$S_{YY}(x, \omega) = \lim_{T \rightarrow \infty} \frac{1}{T} \langle \underline{Y_T(x, \omega) Y_T^*(x, \omega)} \rangle$$

$$Y_T(x, \omega) = \underline{\phi(x, \omega) V_T(\omega)}$$

\Rightarrow

$$S_{YY}(x, \omega) = |\phi(x, \omega)|^2 S_{VV}(\omega)$$

Merits of studying continuous systems

- **Means of first cut models for tall buildings, soil layers and line like structures such as chimneys and towers.**
- **For certain problems, continuous models may simplify the problem: for example, continuous models for lattice structures such as towers.**
- **If loads are rapidly fluctuating or when high frequency vibration is of interest it may be preferable to use continuous models.**
- **Exact solutions are possible for a class of problems. This is of educational value and also helps in assessing approximate methods of analysis.**

Limitations

- For each structural type, we need to develop a separate theory (axially vibrating bar, beam, arch, plate, shell...).
- Built-up structures (like building structures or water tanks) are difficult (if not impossible) to study using continuous system models.