

# **Two Machine System pu Model**

# Differential Equations: Network Transients Neglected

$$\frac{d\psi_G}{dt} = \frac{1}{T'_q}(-\psi_G + \psi_q)$$

$$\frac{d\psi_K}{dt} = \frac{1}{T''_q}(-\psi_K + \psi_q)$$

$$\frac{d\psi_H}{dt} = \frac{1}{T''_d}(-\psi_H + \psi_d)$$

$$\frac{d\psi_F}{dt} = \frac{1}{T'_d}(-\psi_F + \psi_d + \frac{x'_d}{(x_d - x'_d)} E_{fd})$$

## Simple Static Exciter + AVR Model

$$\frac{dX_E}{dt} = \frac{1}{T_A} (-X_E + k_A (V_{ref} - V) )$$

$$V = \sqrt{v_d^2 + v_q^2} = \sqrt{v_D^2 + v_Q^2}$$

$E_{fd} = X_E$  except that it is clipped if limits are exceeded

## Simple Turbine- Governor Model

$$\frac{\Delta P_m(s)}{\Delta \omega(s)} = K \frac{1 + 2s}{1 + 6s}$$

$$P_m = P_{m0} + \Delta P_m$$

$$\Delta \omega = \omega_{REF} - \omega$$

$P_m$  is limited.

## Mechanical Equations in per-unit

$$\frac{d\delta}{dt} = \omega - \omega_0$$

$$\frac{2H}{\omega_B} \frac{d\omega}{dt} = T_m - (\psi_{d^i q} - \psi_{q^i d})$$

$$\approx P_m - (\psi_{d^i q} - \psi_{q^i d})$$

## Mechanical Equations in per-unit

$\omega$  is the electrical angular speed in rad/s.

$\omega_B$  is the base electrical angular speed in rad/s.

$\theta = \omega_o t + \delta$ , is the rotor position.

In this study, let us take,  $\omega_o = \omega_B$

## Algebraic Equations (Both Machines)

$$\psi_d = x_d'' i_d + \frac{(x_d' - x_d'')}{x_d'} \psi_H + \frac{(x_d - x_d') x_d''}{x_d x_d'} \psi_F$$

$$0 = -\omega_B \psi_q - \omega_B R_a i_d - \omega_B v_d$$

$$\psi_q = x_q'' i_q + \frac{(x_q' - x_q'')}{x_q'} \psi_K + \frac{(x_q - x_q') x_q''}{x_q x_q'} \psi_G$$

$$0 = \omega_B \psi_d - \omega_B R_a i_q - \omega_B v_q$$

## D-Q variables

$$[C_K] = \sqrt{\frac{2}{3}} \begin{bmatrix} \cos \omega_{ot} & \sin \omega_{ot} & \sqrt{\frac{1}{2}} \\ \cos(\omega_{ot} - 2\pi/3) & \sin(\omega_{ot} - 2\pi/3) & \sqrt{\frac{1}{2}} \\ \cos(\omega_{ot} + 2\pi/3) & \sin(\omega_{ot} + 2\pi/3) & \sqrt{\frac{1}{2}} \end{bmatrix}$$



## D-Q variables

$$\begin{bmatrix} f_a \\ f_b \\ f_c \end{bmatrix} = [C_{P1}] \begin{bmatrix} f_{d1} \\ f_{q1} \\ f_o \end{bmatrix} = [C_K] \begin{bmatrix} f_{D1} \\ f_{Q1} \\ f_o \end{bmatrix}$$

## D-Q variables

$$\begin{bmatrix} \cos \delta_1 & \sin \delta_1 \\ -\sin \delta_1 & \cos \delta_1 \end{bmatrix} \begin{bmatrix} f_{d1} \\ f_{q1} \end{bmatrix} = \begin{bmatrix} f_{D1} \\ f_{Q1} \end{bmatrix}$$

$$(f_{Q1} + j f_{D1}) = (f_{q1} + j f_{d1}) e^{j\delta_1}$$

For Machine 2:

$$(f_{Q2} + j f_{D2}) = (f_{q2} + j f_{d2}) e^{j\delta_2}$$

**Algebraic Equations (Both Machines): Assume  $x''_d = x''_q$**

$$\psi_D = x''_d i_D + \mathcal{F}_1(\psi_H, \psi_G, \psi_K, \psi_F, \delta)$$

$$0 = -\omega_B \psi_Q - \omega_B R_{ai} i_D - \omega_B v_D$$

$$\psi_Q = x''_d i_Q + \mathcal{F}_2(\psi_H, \psi_G, \psi_K, \psi_F, \delta)$$

$$0 = \omega_B \psi_D - \omega_B R_{ai} i_Q - \omega_B v_Q$$

## Algebraic Equations: Network + Load: Transients Neglected

$$\begin{bmatrix} 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -\frac{r\omega_B}{x} & -\omega_B \\ \omega_B & -\frac{r\omega_B}{x} \end{bmatrix} \begin{bmatrix} i_{lD} \\ i_{lQ} \end{bmatrix} + \frac{\omega_B}{x} \left( \begin{bmatrix} v_{D1} \\ v_{Q1} \end{bmatrix} - \begin{bmatrix} v_{D2} \\ v_{Q2} \end{bmatrix} \right)$$

## Algebraic Equations: Network + Load: Transients Neglected

$$v_{Q1} = R_{L1}(i_{Q1} - i_{lQ1})$$

$$v_{D1} = R_{L1}(i_{D1} - i_{lD1})$$

$$v_{Q2} = R_{L2}(i_{Q2} + i_{lQ2})$$

$$v_{D2} = R_{L2}(i_{D2} + i_{lD2})$$

Differential Equations / States: 16

$$\delta_1, \omega_1, \psi_{G1}, \psi_{H1}, \psi_{K1}, \psi_{F1}, X_{E1}, X_{G1}$$

$$\delta_2, \omega_2, \psi_{G2}, \psi_{H2}, \psi_{K2}, \psi_{F2}, X_{E2}, X_{G2}$$

Algebraic Equations / Variables: 14

$$\psi_{D1}, \psi_{Q1}, \psi_{D2}, \psi_{Q2}, i_{D1}, i_{Q1}, i_{D2},$$

$$i_{Q2}, v_{D1}, v_{Q1}, v_{D2}, v_{Q2}, i_{lD}, i_{lQ}$$