

CRYOGENIC ENGINEERING



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Lecture No - 25

Earlier Lecture

- In the earlier lecture, we have seen the importance of equilibrium curve, OP lines and q line in calculation of number of plates using graphical **McCabe – Thiele** method.
- A tutorial problem was solved using an excel sheet to understand the stair casing method and the concept of equilibrium of liquid – vapor mixture.

Earlier Lecture

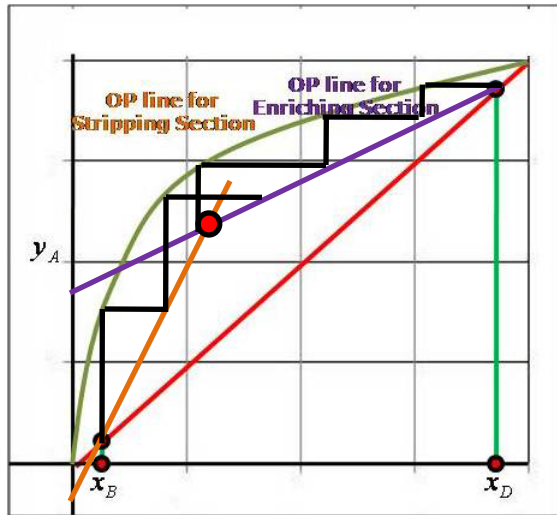
- The total number of theoretical plates is given by the number of vertical lines between the equilibrium and the operating lines.

Outline of the Lecture

Topic : Gas Separation (contd)

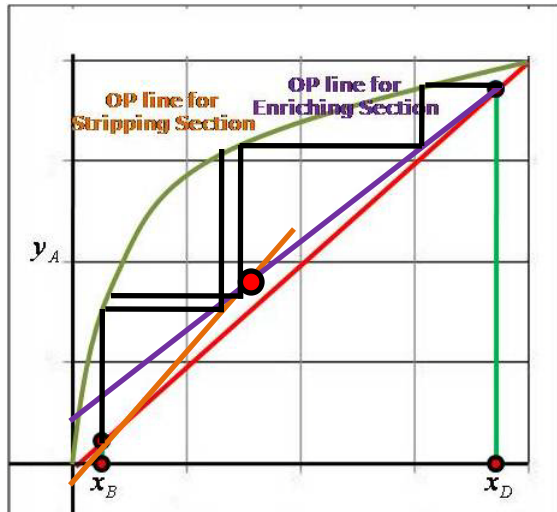
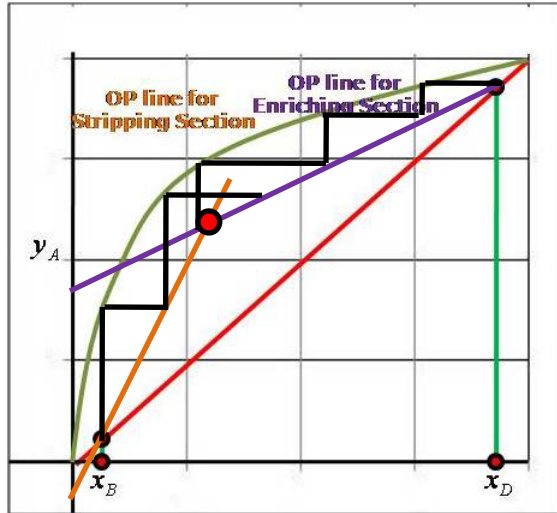
- Concept of Reflux
- Parametric study – Tutorial
- Summary of the topic
- Assignments

McCabe – Thiele Method



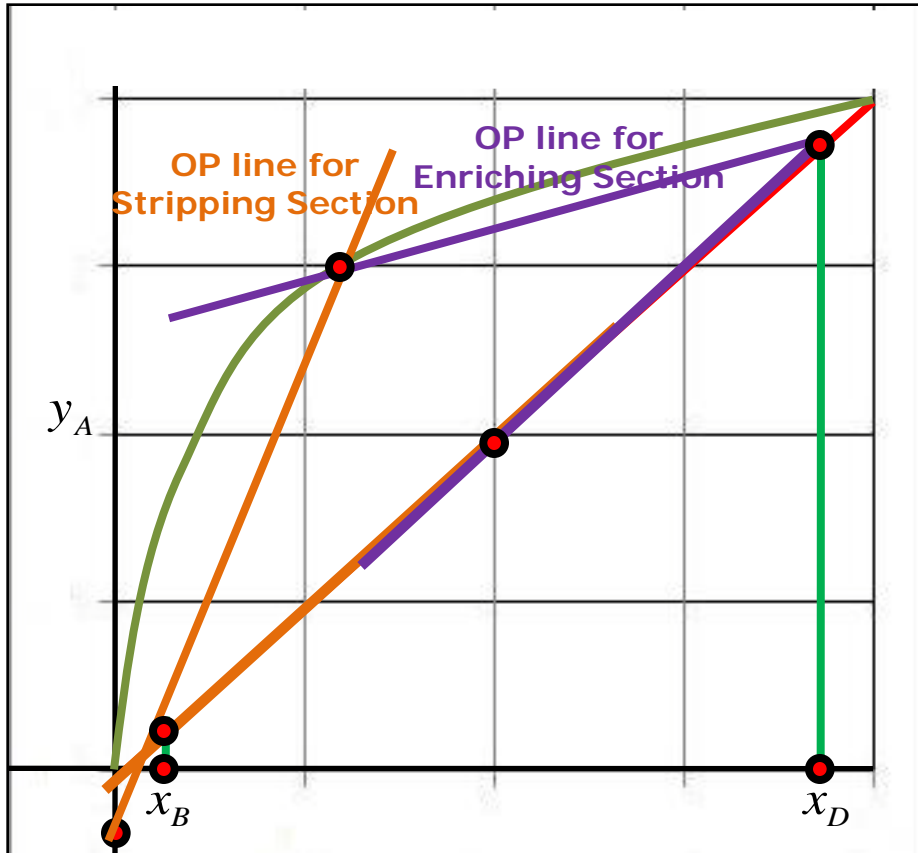
- Consider the OP lines for a column as shown in the figure.
- The number of theoretical plates in this case are **5**.

McCabe – Thiele Method



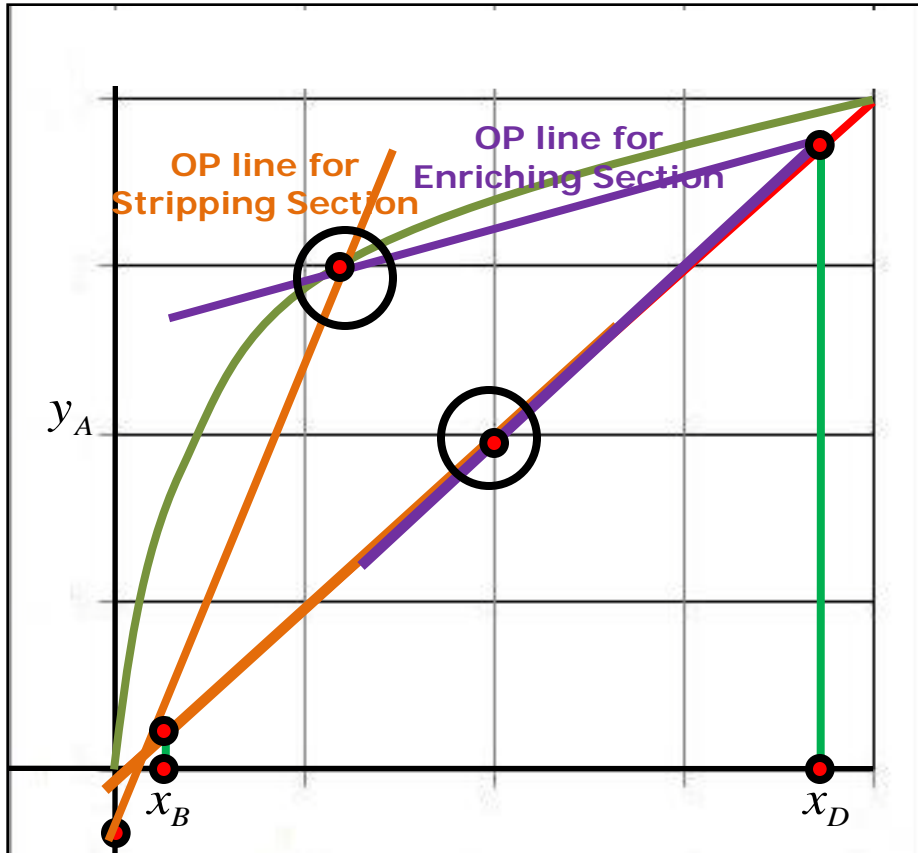
- If the OP lines approach closer to the diagonal, as shown in the figure,
- The number of theoretical plates are reduced to **4**.

McCabe – Thiele Method



- The extreme cases of point of intersection of OP lines are on
 - Equilibrium curve
 - **45°** diagonal
- The point of intersection cannot be above equilibrium and below diagonal lines because, the law of conservation of mass gets violated.

McCabe – Thiele Method



- Therefore, it is clear that the number of theoretical plates are
 - Maximum, when the point of intersection is on equilibrium line.
 - Minimum, when the point of intersection is on diagonal line.

Reflux Ratio

- In the earlier lecture, we have seen the equation for an operating line (for enriching section) as

$$y_n = \left(\frac{L_{n+1}}{V_n} \right) x_{n+1} + \left(\frac{D}{V_n} \right) x_D$$

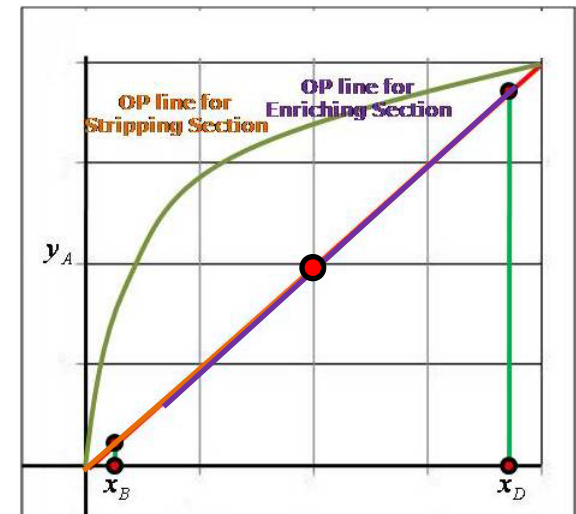
- In the above equation,
 - L_{n+1}/V_n is called as internal reflux ratio (**IR**).
 - D/V_n is called as external reflux ratio (**ER**).

- From the earlier lecture, we have
- Therefore, **IR = 1 - ER**.

$$\frac{L_{n+1}}{V_n} = 1 - \frac{D}{V_n}$$

Reflux Ratio

- The column has two limiting reflux conditions. They are
- **Condition of Total Reflux**
 - In this condition, all the vapor of top plate is condensed and is returned as liquid to column.
 - Hence, $L/V = 1$ (for enriching section) making the OP lines to match with diagonal. The column has minimum number of plates.

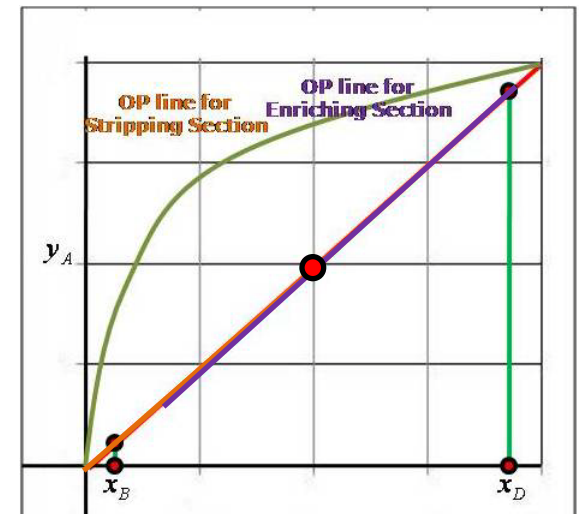


Reflux Ratio

- For $IR=1$, from the equation $IR=1 - ER$, we get $ER=0$.

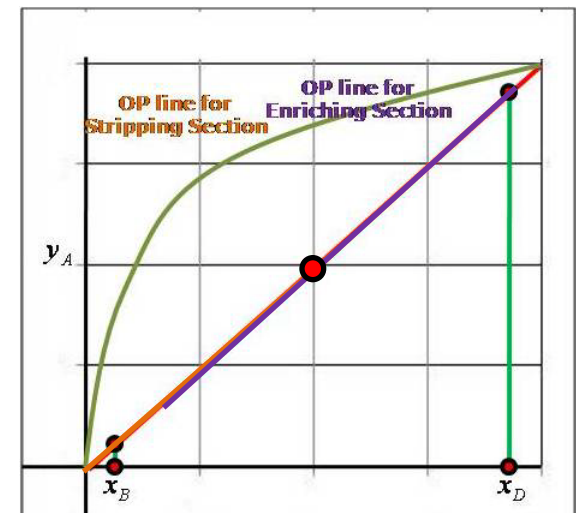
$$ER = \frac{D}{V_n} = 0$$

- Hence, in this condition, the product output of column is **zero**.
- Continuing further, it is clear that L_{n+1} is directly dependent on Q_D . That is, as the value of Q_D increases, IR approaches **1**.



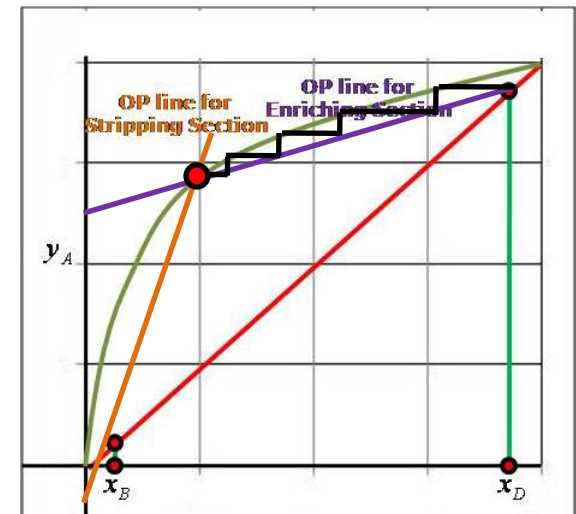
Reflux Ratio

- Summarizing, at high **IR** values (approaching **1**), we have
 - Reduced number of plates.
 - For a given **D**, high condenser loads.
- If **IR=1**, the product output of the column is **zero** (condition of total reflux).



Reflux Ratio

- **Condition of Minimum Reflux**
 - In this condition, the amount of liquid to the column is decreased with a decrease in vapor condensed and returned to the top of the column.
 - Here, $L/V < 1$ (for enriching section) makes the OP lines to move closer to the equilibrium curve. The column has maximum number of plates.

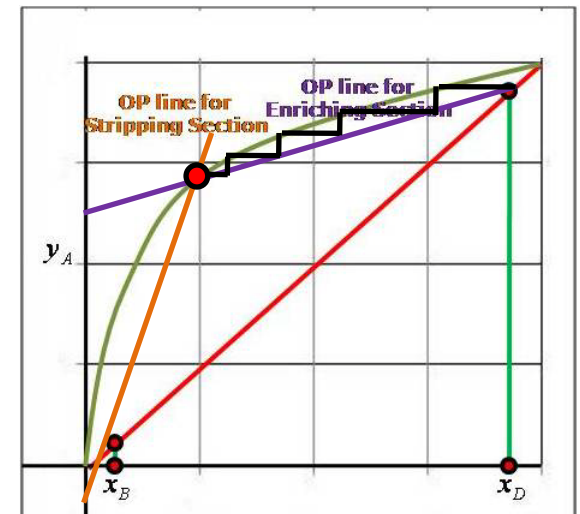


Reflux Ratio

- Again, for $IR < 1$, from the equation $IR = 1 - ER$, we get $ER > 0$.

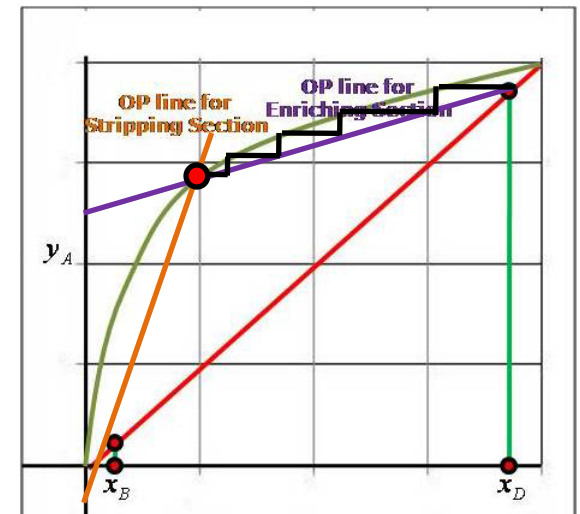
$$ER = \frac{D}{V_n} > 0$$

- Hence, in this condition, unlike the earlier case, there is a finite quantity of product output.
- We know that L_{n+1} is directly dependent on Q_D , therefore as Q_D decreases, IR also decreases.



Reflux Ratio

- Summarizing, at low **IR** values (less than **1**), we have
 - Increased number of plates.
 - Low condenser loads.
 - A finite quantity of product output from the column.



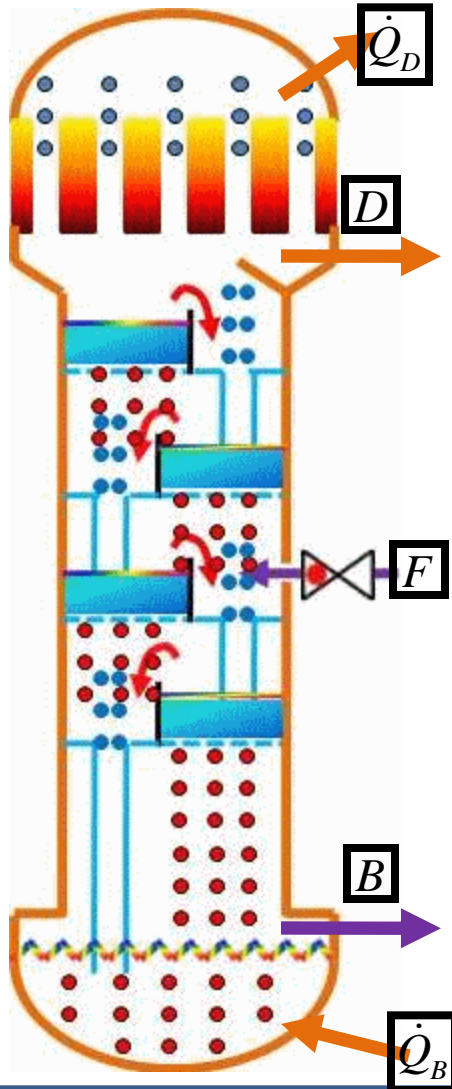
Reflux Ratio

- For the extreme cases of high and low reflux ratios,
 - Plates – minimum, high refrigeration costs.
 - Plates – maximum, low refrigeration costs.
- But in practical cases, the design of column is a compromise between the number of plates and refrigeration costs.

Reflux Ratio

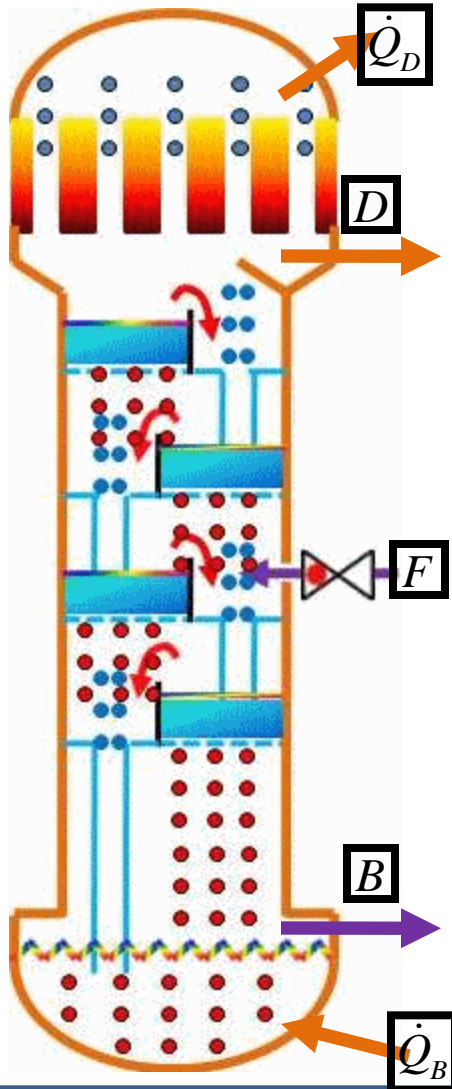
- The typical values of Reflux ratio for a distillation column are **1.15** to **1.35** times the minimum reflux ratio.
- Similarly, for a cryogenic column, we have typical values as **1.05** to **1.15** times the minimum reflux ratio.
- It is important to note that the minimum reflux ratio is dependent on equilibrium curve.

Parametric Study



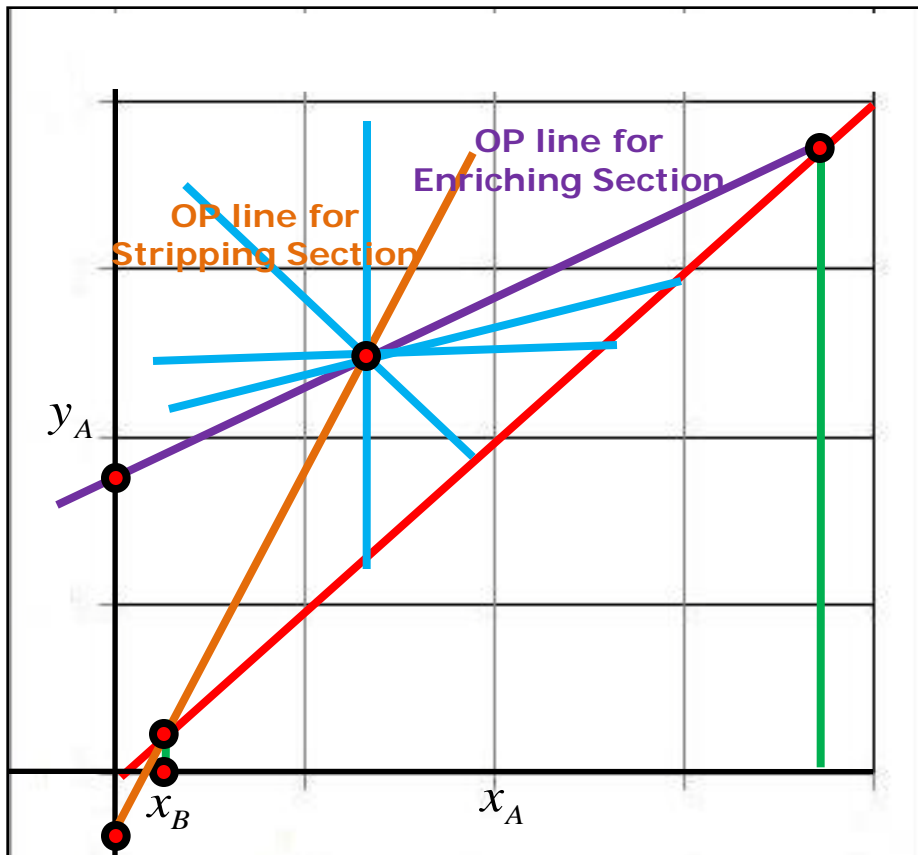
- The slope of an OP line is a function of both L and V , which are in turn dependent on D , \dot{Q}_D , B , \dot{Q}_B .
- It is important to note that, any change in D , alters other parameters as well and vice versa.
- This is to conform with the laws of conservation of mass and energy for the column as a whole.

Parametric Study



- We know that the impurity of component **A** in the bottom product is given by x_B .
- Reducing x_B implies more purity of the bottom product, hence, more number of plates in lower section.
- Similarly, the purity of component **A** in the top product is given by x_D .
- Again, increasing x_D would increase the number of plates in top section.

Parametric Study



- The parameter q is very important in determining
 - The slope of q line.
 - An approximate feed inlet position.
 - The theoretical number of plates.

McCabe – Thiele Method

- In the earlier lecture, we have solved the following tutorial.
- Consider a rectification column for N_2 and O_2 separation operating at 1 atm. Determine the number of theoretical plates required to yield **97% N_2** at top and **95% O_2** at bottom. Feed stream is **50% N_2** and **50% O_2** . Molar fraction of liquid in feed stream is **0.7** mole liquid/mole mixture. The desired flow rate at the bottom product is **20** mole/sec and the heat removed in the condenser at top of the column is **500** kW.

McCabe – Thiele Method

Given

Working Pressure : 1 atm

Mixture : $N_2 + O_2$

Feed stream : 50% $N_2 + 50\%$ O_2

Bottom flow rate : 20 mole/sec = **B**

Feed liq. : 0.7 = **q**

For above mixture

Reqt. of N_2 (top) : 97% = **x_D**

Reqt. of O_2 (bottom) : 95% = **$x_B = 0.05$**

- For the above problem, calculate the number of theoretical plates for changes in **Q_D , q , x_B and x_D** .

McCabe – Thiele Method

- From the earlier lecture, we have the following.
- OP line for enriching section : $y_n = 0.773x_{n+1} + 0.22$
- OP line for stripping section : $y_m = 1.274x_{m+1} - 0.013$
- q line : $y = -2.34x + 1.67$
- In the earlier lecture, we have seen the stair casing procedure on an excel sheet.

McCabe – Thiele Method

- From the excel sheet, it was clear that the total number of vertical lines are **9**.
- Therefore, the total number of theoretical plates for the column are tabulated as shown below.

McCabe – Thiele Method	
Enriching Section	3 + 1 (Condenser)
Stripping Section	6 + 1 (Boiler)

Parametric Study – Tutorial

- Let us see the effect of Q_D , holding all other parameters as constant.

	I	II	III	IV	V
Q_D (kW)	500	350	900	9000	300
Q_B (kW)	430.6	280.6	830.6	8930	930.6
$(L/V)_{ES}$	0.77	0.68	0.87	0.99	0.89
$(L/V)_{SS}$	1.27	1.42	1.14	1.01	1.13
Plates	3 + 6	4 + 8	3 + 5	3 + 5	4 + 9

Parametric Study – Tutorial

- Let us see the effect of x_D and x_B , holding all other parameters as constant.

x_D	Plates
0.97	3 + 6
0.99	4 + 6

x_B	Plates
0.05	3 + 6
0.02	3 + 8

Parametric Study – Tutorial

- Let us see the effect of q , holding all other parameters as constant.

q	Slope	Plates
$q=0.7$	-2.3	3 + 6
$q=1$	∞	2 + 6
$q=0$	0	4 + 6

Parametric Study – Summary

- Summarizing the parametric study, we have the following inferences.
- The number of theoretical plates decrease, as the OP lines approach close to the diagonal.
- The slope of the OP line of enriching section decreases by increasing D or reducing Q_D .

Parametric Study – Summary

- Decreasing x_B (more purity of bottom product) or increasing x_D (more purity of top product), increases the number of plates in the column.
- The value of q is vital in determining the q line, an approximate feed inlet position and number of theoretical plates.

Summary

- In an Ideal Gas Separation system, all the processes are reversible and the work requirement is called as an Ideal Work.
- The equation for work requirement per mole of mixture to separate a mixture with **N** constituents is

$$\frac{-W_i}{n_m} = \mathfrak{R}T_m \sum_{j=1}^N y_j \ln \left(\frac{1}{y_j} \right)$$

- The work/mole of mixture is always less than work/mole of its constituents for any mixture. Also, $\mathbf{W}_{i,m}/\mathbf{n}_m$ is maximum when the percentage compositions of all its ingredients are equal.

Summary

- If number of components, number of phases and degrees of freedom for a mixture in thermal equilibrium are denoted by C , P and F respectively, then the Gibbs Phase Rule

$$F = C - P + 2$$

- Dalton's Law relates partial pressures of non – reacting ideal gases.
- Raoult's Law relates the vapor pressure with the liquid mole fraction of a component in a mixture.
- Gibbs – Dalton's Law is an application of Dalton's law to the vapor above the liquid phase.

Summary

- **Murphree efficiency** of a plate is defined as the ratio of actual change in mole fraction to the maximum possible change that can occur.
- **McCabe – Thiele** method is less general and is widely used for binary mixtures at cryogenic temperatures.
- The major assumption in this method is that the liquid and vapor enthalpies are independent of mole fraction.

Summary

- The equations of operating lines for enriching and stripping sections are

$$y_n = \left(\frac{L_{n+1}}{V_n} \right) x_{n+1} + \left(\frac{D}{V_n} \right) x_D$$

$$y_m = \left(\frac{L_{m+1}}{V_m} \right) x_{m+1} - \left(\frac{B}{V_m} \right) x_B$$

- The locus of intersection of these operating lines denotes the feed condition. It is given as

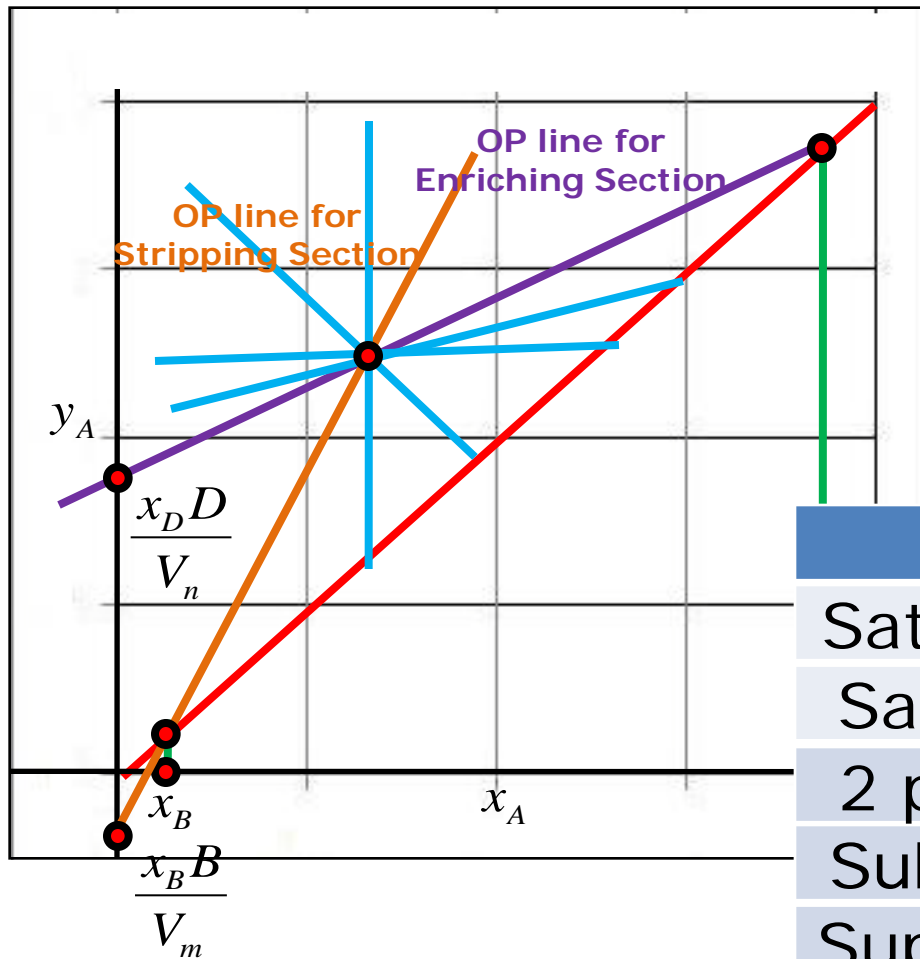
$$y = \left(\frac{q}{q-1} \right) x + \frac{x_F}{1-q}$$

- The point of intersection of feed line or q line and $y=x$ gives the content of a component in the feed, x_F .

McCabe – Thiele Method

- The equation of feed line is

$$y = \left(\frac{q}{q-1} \right) x + \frac{x_F}{1-q}$$



Condition	q	Slp
Sat. Vap. ($h_F = H$)	$q = 0$	0
Sat. Liq. ($h_F = h$)	$q = 1$	∞
2 ph. ($H < h_F < h$)	$0 < q < 1$	-ve
Sub. Liq. ($h_F < h$)	$q > 1$	+ve
Sup. Vap. ($h_F > h$)	$q < 0$	+ve

Summary

- Equilibrium curve gives the relation between liquid composition (x_n) and vapor composition (y_n) on the same plate.
- The OP lines relate the variation of liquid (x_{n+1}) and vapor (y_n) mole fractions of a particular component across the length of the column.
- The plate calculation is a stair casing method which involves locating equilibrium conditions on equilibrium line and OP line.

Summary

- In a McCabe – Thiele diagram
 - Each horizontal line gives the condition of liquid – vapor on the same plate which are in thermal equilibrium.
 - Each vertical line gives the vapor condition for the plate with respect to liquid that leaves the earlier plate on the top.
- The total number of vertical lines in top and bottom section, together with boiler and condenser surfaces is the total number of theoretical plates required.

Summary

- At high **IR** values, we have
 - Reduced number of plates.
 - High condenser loads.
 - Product output is zero (**IR=1**).
- At low **IR** values, we have
 - Increased number of plates.
 - Low condenser loads.
 - Finite quantity of product output.
- The number of theoretical plates decrease, as the OP lines approach close to the diagonal.

Summary

- Decreasing x_B (more purity of bottom product) or increasing x_D (more purity of top product), increases the number of plates in the column.

Assignment - 1

- Determine the number of theoretical plates required to yield **95% N₂** at top and **96% O₂** at bottom. Feed stream is **70% N₂** and **30% O₂**. the operating pressure is 1 atm. Molar fraction of liquid in feed stream is **0.5** mole liquid/mole mixture. The desired flow rate at the bottom product is **30** mole/sec and the heat removed in the condenser at top of the column is **2000** kW.
- Also, calculate the maximum and minimum number of plates for the extreme cases of **Q_D**.

Answers

- OP line for enriching section : $y_n = 0.77x_{n+1} + 0.22$
- OP line for stripping section : $y_m = 1.11x_{m+1} - 0.001$
- q line : $y = -1.0x + 1.4$
- The total number of vertical lines are **8**.

McCabe – Thiele Method

Enriching Section	2 + 1 (Condenser)
Stripping Section	6 + 1 (Boiler)

Thank You!